

**UOP RUSSELL LLC**  
Tulsa, Oklahoma

JOB NO: <b>J-447</b>	TAG NO: <b>V-402</b>	DATE: <b>7/14/2011</b>
CLIENT: <b>UOP Russell</b>	S.O./P.O. NO:	BY: <b>JRG</b>
SUBJECT: <b>60MM Cryo Plant</b>	SERVICE: <b>Cold Separator</b>	

**PRESSURE VESSELS**

MECHANICAL DESIGN	PROCESS DESIGN
Type (vertical, horizontal, tower) <b>Vertical</b>	Operating Pressure (psia) <b>768</b>
Diameter: (inch) <b>78" ID</b>	Operating Temperature (°F) <b>-30 / -5</b>
S/S Length (ft-inch) <b>12' - 0"</b>	Vapor Flow (Lb/Hr) <b>77,881 / 87,818</b>
Skirt Length(ft-inch) <b>3' - 0"</b>	Vapor Density (Lb/cf) <b>4.381 / 4.073</b>
Design Pressure (psig) <b>1100</b>	Liquid Flow (Lb/Hr) <b>32,842 / 22,912</b>
Design Temperature (°F) <b>150</b>	Liquid Density (Lb/cf) <b>29.13 / 30.25</b>
MDMT (°F) @ Pressure (psig) <b>-50 @ 1100</b>	Liquid Residence Time (Min) <b>&gt; 5 min @ NLL</b>
Corrosion Allowance (inch) <b>0.0625</b>	
Radiography <b>RT-1</b>	<b>MIST PAD</b>
PWHT Req'd? <b>Yes</b>	Req'd : <b>Yes</b> Diameter: <b>40"</b>
Wind / Seismic Code <b>ASCE 7-10 / ASCE 7-10</b>	Overall Thk: <b>11"</b> Pad Thk: <b>9"</b>
Wind Code <b>Cf=0.7, V=120 mph, Exp. C, Cat. III</b>	Removable: <b>No</b> Grid Matl: <b>316SS</b>
Seismic Code <b>Site D, I=1.25, S<sub>s</sub>=100% , S<sub>1</sub>=40%</b>	Wire Diameter: <b>0.006</b> Mesh Matl: <b>316SS</b>
Insulation <b>2°C</b>	<b>MATERIAL SPECIFICATIONS</b>
Fireproof <b>No</b>	Shell SA- <b>516-70N</b>
Code <b>ASME VIII, Div I</b>	Head SA- <b>516-70N</b>
Code Stamp Req'd <b>Yes</b>	Nozzle Necks SA- <b>333 Gr. 6</b>
Sandblast / Paint <b>SSPC-SP6 / TRCo Std ENG-36c</b>	Flanges SA- <b>350-LF2</b>
Ladder / Platform Clips Req'd? <b>No</b>	Couplings SA- <b>350-LF2</b>
Pipe Supports Req'd? <b>No</b>	Studs SA- <b>193-B7</b>
	Nuts SA- <b>194-2H</b>
	Skirt / Baseplate SA- <b>516-70</b>

**NOZZLES**

SERVICE	MK	QTY	SIZE	RATING	FACE & TYPE	NOZZLE APPURTENANCES
Inlet	A	1	8."	600	RF FLG	w/ Diverter
Vapor Outlet	B	1	8."	600	RF FLG	
Liquid Outlet	C	1	▲ 4."	600	RF FLG	Syphon
LSHH	D	2	1."	6000	CPLG	
TI	E	1	.75"	6000	CPLG	
LT	F	2	1."	6000	CPLG	
LG	G	4	.75"	6000	CPLG	
Manway	H	1	18."	600	RF FLG	
TE	J	1	.75"	6000	CPLG	

**INTERNALS AND APPURTENANCES**

PACKING	Size (in.)	Type	Bed Height (ft.)	PLATFORMS	Quantity	Angle / Area				
Top				Access:		(deg)	Diameter (in):			
Middle				Stepoff:		(deg)	Length (in):			
Bottom				Other:		(Sq.Ft.)	with flanges			
<b>TRAYS</b>	Quantity	No. of Passes	Weldins by:	Platepack Length (inch):			Qty Break Flg Pairs:			
				Total Ladder Length (ft):			Qty of Hat Trays:			
<b>NOTES:</b>							Weir Plate:	<b>No</b>		
1) See scope of supply for oversizing mist pads.							Wave Baffle:	<b>No</b>		
2) 5 minutes residence time at the NLL 60" (Recovery). Disengaging height 53".							Nat'l Board Req'd:	<b>Yes</b>		
3) Use TRCo Painting System 3(CS only).							Charcoal Bed Height (ft):			
REVISION	3		▲ 4	1	2		Qty Catalyst bed Supports:			
ENGINEER/DATE	TKF	7/11/13	JRG	8/13/13	BH	11/21/11	TKF	29-Oct		
ISSUED FOR	Revised		Revised	Revised	Revised					

**UOP RUSSELL, LLC**  
Tulsa, Oklahoma

FORM # MST-ELM

**MIST ELIMINATOR SPECIFICATION**

Job Number J-447

Spec. No.: ME-402

Vessel Tag V-402

Spec. By: SHP

Date: 07/09/13

Mistpad Installed Diameter: 40 in

Mesh Thickness: 9 in

Mesh Material: 316SS

Density Required: 12 lbs/cf

Wire Diameter: 0.006 in

Grid Material: 316SS

Grid Diameter: Note 2

Grid Thickness (Top & Bottom) 1 in

Oversized Diameter: Note 1

Manway I.D.: 17 in

Number of Segments: Per Mfr

Removeable (Yes / No): No

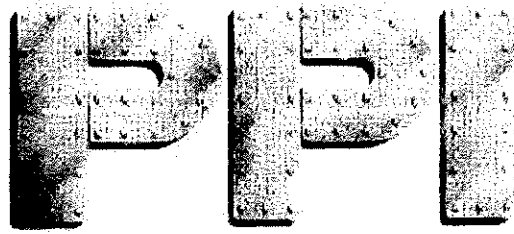
**Note 1: Oversized diameter of Mist Extractor shall allow the vessel to be shipped horizontally with the extractor installed and shall be at least:**

<u>No. of segments</u>	<u>Oversize (all sides of each sections)</u>
1 or 2	1/2"
3 or 4	3/8"
More than 4	1/4"

**Note 2: Grid diameter shall be 1-1/2" less than the installed diameter shown above.**

**Note 3: OD of each grid section shall be banded.**

REVISION	0			
ENGINEER/DATE	SHP	7/9/13		
ISSUED FOR	AFC			



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

**5654-1 Databook  
Manufacturer's Databook**

**P.P.I. Job Number: 5654**

**P.P.I. Shop Order: 5654-1**

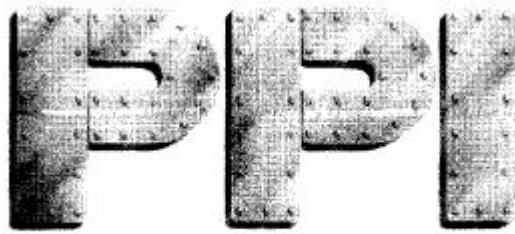
**Customer: UOP RUSSELL**

**Item: V-402,**

**COLD SEPARATOR**

**Customer P.O. No. # 4500754097**

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**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

### **List of Contents**

# **Item: V-402, COLD SEPARATOR**

#### **Cover Sheet**

#### **Table of Contents**

##### **1) Quality Documents**

Pg. 1	Manufacturer Data Report (U-1A)
Pg. 2	Inspection Traveler
Pg. 3-5	Quality Inspection Plan
Pg. 6	Certificate of Compliance

##### **2) Design Documentations**

Pg. 1-3	Certified 'As-Built' Drawings
Pg. 4-92	Calculations

##### **3) Materials**

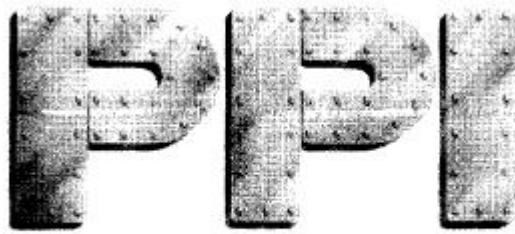
Pg. 1&2	Heat Number Map
Pg. 3-42	Material Test Reports (MTR'S)

##### **4) Non-Destructive Testing (NDE)**

Pg. 1-5	Radiography Reports
Pg. 6	Magnetic Particle Test Report
Pg. 7	Ultrasonic Test Reports

##### **5) Welding**

Pg. 1	Approved Weld Map
Pg. 2-6	WPS 149DCP Rev.2
Pg. 7-11	WPS 151DCP Rev.1
Pg. 12&13	(DOT.T)
Pg. 14&15	(E)
Pg. 16&17	(I)
Pg. 18&19	(K)
Pg. 20&21	(Q)



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

**List of Contents**

### **Item: V-402, COLD SEPARATOR**

#### **6) Pressure Testing**

Pg. 1            Hydrostatic Pressure Chart  
Pg. 2-4        Gauge Calibration Sheets (PPI GAUGES: PPI-38, PPI-39 & RECORDER: R-37)

#### **7) Miscellaneous Certificates/Reports/Drawings/Parts List(s)**

Pg. 1            Nameplate Photocopy  
Pg. 2&3        PWHT Heat Charts & Calibration Sheet  
Pg. 4            Paint Sheet



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## **5654-1 Databook**

List of Contents

Item: V-402, COLD SEPARATOR

# **Quality Documents**

<b>Pg. 1</b>	<b>Manufacturer Data Report (U-1A)</b>
<b>Pg. 2</b>	<b>Inspection Traveler</b>
<b>Pg. 3-5</b>	<b>Quality Inspection Plan</b>
<b>Pg. 6</b>	<b>Certificate of Compliance</b>

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**FORM U-1A MANUFACTURER'S DATA REPORT FOR PRESSURE VESSELS**  
 (Alternative Form for Single Chamber, Completely Shop or Field Fabricated Vessels Only)  
 As Required by the Provisions of the ASME Boiler and Pressure Vessel Code Rules, Section VIII, Division 1

1. Manufactured and certified by Professional Projects Inc. 18115 Telge Rd. Cypress, Tx 77429  
 (Name and address of Manufacturer)  
 2. Manufactured for UOP Russell  
 (Name and address of Purchaser)  
 3. Location of installation Unknown  
 (Name and address)  
 4. Type Vertical Tank 5654-1 5654-1 Rev. 1 3170 2017  
 (Horizontal or vertical tank) (Manufacturer's serial No.) (CRN) (Drawing number) (National Board number) (Year built)  
 5. ASME Code, Section VIII, Division 1 2013  
 [Edition and Addenda, if applicable (date)] (Code Case Numbers) [Special Service per UG 120(d)]

6. Shell: SA-516-70N 2.50" .0625" 78" 12'-0"  
 (Material spec. number, grade) (Nominal thickness, in.) (Corrosion allowance, in.) (Inner diameter in.) (Length (overall))

Body Flanges on Shells								Bolting				
No.	Type	ID	OD	Flange Thk	Min Hub Thk	Material	How Attached	Location	Num & Size	Bolting Material	Washer (OD, ID, th)	Washer Material
---	---	---	---	---	---	---	---	---	---	---	---	---
---	---	---	---	---	---	---	---	---	---	---	---	---

7. Seams: Welded Dbl Butt Full 1.0 1150 1.49 Welded Dbl Butt Full 1.0 1  
 (Long. (welded, dbl, snlg, lap, butt) R.T. (Spot or Full) (Eff. %) (H.T. Temp.) (Time hr) Girth (welded, dbl, snlg, lap, butt) R.T. (spot or full) (Eff. %) (No. of courses)

8. Heads: (a) Material SA-516-70N (b) Material SA-516-70N  
 (Spec no., grade) (Spec no., grade)

	Location (Top, Bottom, Ends)	Minimum Thickness	Corrosion Allowance	Crown Radius	Knuckle Radius	Elliptical Ratio	Conical Apex Angle	Hemispherical Radius	Flat Diameter	Side to Pressure (Convex or Concave)
(a)	Top	2.2262"	.0625"	---	---	2:1	---	---	---	Concave
(b)	Bottom	2.2262"	.0625"	---	---	2:1	---	---	---	Concave

Body Flanges on Heads								Bolting				
	Type	ID	OD	Flange Thk	Min Hub Thk	Material	How Attached	Location	Num & Size	Bolting Material	Washer (OD, ID, th)	Washer Material
(a)	---	---	---	---	---	---	---	---	---	---	---	---
(b)	---	---	---	---	---	---	---	---	---	---	---	---

9. MAWP 1100 --- 150 --- °F  
 (Internal) (External) psi at max. temp. (Internal) (External)  
 Min. design metal temp. -50 °F at 1100 psi. Hydro., pneu., or comb. test pressure Hydro. 1430 psi.

10. Nozzles, inspection and safety valve openings: Proof test ---

Purpose (inlet, Outlet, Drain, etc.)	No.	Diameter or Size	Type	Material		Nozzle Thickness		Reinforcement Material	Attachment Details		Location (Insp. Open.)
				Nozzle	Flange	Nom.	Corr.		Nozzle	Flange	
Manway	1	18"	600 RFHB	SA-350-LF2	---	2.00"	.0625"	---	Type 7	---	Shell
Inlet w/ Diverter	1	8"	600 RFHB	SA-350-LF2	---	1.375"	.0625"	---	Type 7	---	Shell
Vapor Outlet	1	8"	600 RFHB	SA-350-LF2	---	1.375"	.0625"	---	Type 7	---	Top Head
Liquid Outlet w/Syphon	1	4"	600 RFHB	SA-350-LF2	---	1.00"	.0625"	---	Type 7	---	Shell
LSHH	2	1"	6000# CLPG	SA-350-LF2	---	.4675"	.0625"	---	Type 7	---	Shell
LT	2	1"	6000# CLPG	SA-350-LF2	---	.4675"	.0625"	---	Type 7	---	Shell
TI, LG, TE	6	3/4"	6000# CPLG	SA-350-LF2	---	.4675"	.0625"	---	Type 7	---	Shell

11. Supports: Skirt Yes Lugs 0 Legs 0 Other --- Attached Bottom Head/Welded  
 (Yes or no) (Number) (Number) (Describe) (Where and how)

12. Remarks: Manufacturer's Partial Data Reports properly identified and signed by Commissioned Inspectors have been furnished for the following items of the report: \_\_\_\_\_  
 (Name of part, item number, Manufacturer's name and identifying stamp)

MDMT per UG-20(f).

ITEM: V-402, Cold Separator P.O.: 4500754097

<b>CERTIFICATE OF SHOP/FIELD COMPLIANCE</b>	
We certify that the statements made in this report are correct and that all details of design, material, construction, and workmanship of this vessel conform to the ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. "U" Certificate of Authorization No. <u>17,507</u> expires <u>April 21, 2015</u>	
Date <u>8/17/2017</u>	Co. name <u>Professional Projects Inc.</u> Signed _____ (Representative)
<b>CERTIFICATE OF SHOP/FIELD INSPECTION</b>	
Vessel constructed by <u>Professional Projects Inc.</u> at <u>18115 Telge Rd. Cypress, TX 77429</u> . I, the undersigned, holding a valid commission issued by The National Board of Boiler and Pressure Vessel Inspectors and employed by <u>James Walsh</u> have inspected the component described in this Manufacturer's Data Report on <u>8/17/2017</u> , and state that, to the best of my knowledge and belief, the Manufacturer has constructed this pressure vessel in accordance with ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. By signing this certificate neither the Inspector nor his/her employer makes any warranty, expressed or implied, concerning the pressure vessel described in this Manufacturer's Data Report. Furthermore, neither the Inspector nor his/her employer shall be liable in any manner for any personal injury or property damage or a loss of any kind arising from or connected with this inspection.	
Date <u>8/17/2017</u> Signed <u>[Signature]</u> Commissions <u>107582</u> [National Board (incl. endorsements)]	

DESCRIPTION 78" ID X 12'-0" S/S  
 ITEM NO. V-402, COLD SEPARATOR  
 SERIAL NO. 5654-1  
 DATE 1/17/2017  
 CUSTOMER UOP RUSSELL

INSPECTION TRAVELER

S/O #: 5654-1

INSPECTION, EXAMINATION PERFORMED	CODE	A.I.	Q.C.	REMARKS
1. SPECS., DESIGN CALCULATIONS, DRAWINGS & MTRS:			1-17-17 SW	
2. MATERIALS:				
a. Heads checked form forming specs. thk.			3/28/17 RC	
b. Shell specs. & thk. out-of-roundness.			3/28/17 RC	
c. CPLGS, Nozzles, Flg. specs.			4/11/17 RC	
3. WELDING:				
a. Procedures Specifications.			1-17-17 SW	
b. Procedure & Performance Qualification.			1-17-17 SW	
4. FABRICATION:				
a. Examine plate surface.			3/28/17 RC	
b. Examine cut edges.			4/4/17 RC	
c. Check weld groove preparation.			4/20/17 RC	
d. Cutting, fitting alignment.			4/20/17 RC	
e. Back-Chip.				
f. Welders symbols (See Heat Chart or Dwg).			4/11/17 RC	
g. Record Mill stamping & transfers (See Heat Chart or Dwg.).				
(1) HEAD (BTM)			3/28/17 RC	
(2) HEAD (TOP)			3/28/17 RC	
(3) SHELL			3/28/17 RC	
(4) SHELL			3/28/17 RC	
h. Verify nozzle thickness & flange ratings			4/11/17 RC	
5. FINAL INSPECTION:				
a. Weld appearance & reinforcement.			3/12/17 RC	
b. Check fillet weld sizes.			3/12/17 RC	
c. Workmanship.			3/14/17 RC	
d. Out-of-roundness. <i>TRAP</i>			3/14/17 RC	
e. Internal.				
f. Vacuum.				
6. POST WELD HEAT TREATMENT:			3/15/17 RC	
a. Type.				
b. Charts reviewed.			3/16/17 RC	
c. Verify up, hold & down periods.			3/15/17 RC	
7. NON-DESTRUCTIVE EXAMINATION:				
a. Hydrostatic PSIG (1430) Gauge #: (R-37)			3/17/17 RC	
b. Radiograph Examination.			4/15/17 RC	
c. MT-Magnetic Particle Examination.			7/19/17 RC	
d. UT-Ultrasonic Examination.			6/14/17 RC	
e. PT-Liquid Penetrant Examination.				
f. Other.				
g. Soap & Air Test reinforcing pads.				
8. NON-CONFORMITY REPORT:				
9. PREPARATION FOR SHIPMENT:				
a. Nameplate attached.				
b. Check stamping on nameplate.				
c. Data report checked and signed.				
d. Customer Inspection & Release.				

P.P.I. CODE LEGEND

x in Code box indicates inspection points

P.O. # 4500754097

ITEMS: V-402

Cold Separator

P.O. #	REVIEW POINTS: I= INSPECT N/A= NOT APPLICATE	REFERENCE DOCUMENTS	Q.C.DEPARTMENT REVIEW		CLIENT REVIEW		COMMENTS
			R.P.	DATE	INITIAL	R.P.	
1.00	PRE-INSPECTION MEETING						
2.00	DOCUMENTS						
2.01	CUSTOMER P.O.	CUST. P.O.	R			R	
2.02	CUSTOMER SPECIFICATIONS	CUST. SPECS.	R			R	
2.03	P.P.I. DRAWINGS	S/O #	R	1-17-17	SD	R	
2.04	P.P.I. CALCULATIONS	S/O #	R			R	
2.05	WPS/PQR & WELD MAP	SECTION IX	R	5-3-17	SD	R	
2.06	WELDER QUALIFICATION	SECTION IX	R	1-17-17	SD	R	
3.00	MATERIALS						
3.01	MATERIAL TEST REPORTS/CERTS	ASME SECT II	R	3/28/17	RC	R	
3.02	THICKNESS REQUIREMENTS	CALCS / DWG	R	3/28/17	RC	R	
3.03	SURFACE CONDITIONS		I	4/14/17	RC	R	
3.04	HEAT NUMBER TRACEABILITY		I	3/28/17	RC	R	
4.00	HEADS						
4.01	FORMING SPECIFICATIONS	UCS-79 & UG-81	R	3/28/17	RC	R	
4.02	EDGE PREPARATIONS	QC-VT	I	4/14/17	RC	R	
5.00	SHELLS						
5.01	OUT-OF-ROUNDNESS	UG-80	I	3/28/17	RC	I	
5.02	EDGE PREPARATIONS	QC-VT	I	4/14/17	RC	I	
6.00	NOZZLES & FITTINGS						
6.01	FLANGE RATING	DWG.	I	4/14/17	RC	I	
6.02	NOZZLE NECK REQUIREMENTS	CALCS. / DWGS.	I	4/14/17	RC	I	
6.03	EDGE PREPARATIONS	QC-VT	I	4/14/17	RC	I	
7.00	LAYOUT & FIT-UP						
7.01	SHELL LONG SEAMS	UW-33	I	4/18/17	RC	R	
7.02	SHELL GIRTH SEAMS	UW-33	I	4/18/17	RC	R	
7.03	HEAD TO SHELL SEAMS	UW-33	I	4/28/17	RC	R	
7.04	FLANGE TO NECK SEAMS	UW-33	I	5/3/17	RC	R	
7.05	NOZZLE TO SHELL/HEAD	UW-33	I	5/5/17	RC	R	
7.06	ATTACHMENTS	UW-33	I			R	

P.O. # 4500754097

ITEMS: V-402

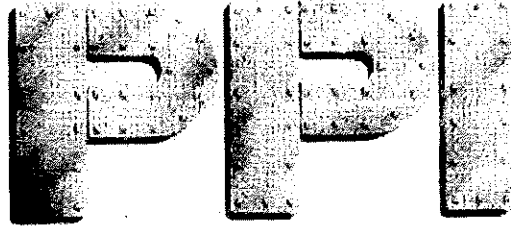
Cold Separator

H= HOLD R= REVIEW	REVIEW POINTS: I= INSPECT N/A= NOT APPLICATE	REFERENCE DOCUMENTS	Q.C. DEPARTMENT		CLIENT		COMMENTS
			R.P.	DATE	R.P.	DATE	
8.00	WELD OUT						
8.01	LONG SEAMS SHELL	UW-35	I	8/15/17 RC	R		
8.02	GIRTH SEAMS SHELLS / HEADS	UW-35	I	8/15/17 RC	R		
8.03	NOZZLE GIRTH SEAMS	UW-35	I	8/15/17 RC	R		
8.04	NOZZLE TO SHELLS / HEADS	UW-35	I	8/15/17 RC	R		
8.05	ATTACHMENTS	UW-35	I		R		
9.00	NDE						
9.01	RT (RADIOGRAPHY)	UW11a	I	8/15/17 RC	I		
9.02	UT (ULTRASONIC)	TGRUT-1	N/A	8/15/17 RC	N/A		
9.03	MT (MAGNETIC PARTICLE)	QC-MT	I	7/19/17 RC	I		
9.04	PT (LIQUID PENETRANT)	QC-PT	N/A		N/A		
9.05	VT (VISUAL)	QC-VT	I		I		
9.06	PMI (POSITIVE MATERIAL IDENTIFICATION)	PMI-100A	N/A		N/A		
10.00	POST WELD HEAT TREATMENT			8/15/17 RC			
10.01	VERIFY TEMP. & HOLD TIMES	UCS-56	R	8/15/17 RC	R		
10.02	REVIEW CHARTS		R	8/15/17 RC	R		
11.00	NDE AFTER P.W.H.T.						
11.01	RT (RADIOGRAPHY)	UW11a	N/A		N/A		
11.02	UT (ULTRASONIC)	TGRUT-1	N/A		N/A		
11.03	MT (MAGNETIC PARTICLE)	QC-MT	N/A	8/15/17 RC	N/A		
11.04	PT (LIQUID PENETRANT)	QC-PT	N/A		N/A		
11.05	VT (VISUAL)	QC-VT	N/A		N/A		
11.06	BRINNELL HARDNESS TESTING	PP-1TP	N/A		N/A		
12.00	PRE-HYDRO INSPECTION						
12.01	FINAL DIMENSIONAL	DWGS.	I	8/15/17 RC	H		
12.02	AIR TEST REINFORCING PADS		I		R		
12.03	INTERNAL INSPECTION/OVERALL APPEARANCE		I		I		

P.O. # 4500754097

ITEMS: V-402  
 Cold Separator

R-REVIEW	H- HOLD	REVIEW POINTS: I=INSPECT NA=NOT APPLICABLE	REFERENCE DOCUMENTS	O.C. DEPARTMENT REVIEW			CLIENT REVIEW			COMMENTS
				R.P.	DATE	INITIAL	R.P.	DATE	INITIAL	
13.00		HYDROSTATIC TEST								
13.01		VERIFY PRESSURE & HOLD TIME	UG-99	W	8/24/17	RC	H			8/24/17 RC
13.02		VERIFY GAUGE CALIBRATION		W	8/24/17	RC	H			
13.03		REVIEW CHARTS		W	8/24/17	RC	H			
14.00		COATING								
14.01		VERIFY REQUIREMENTS	DWG.	W	8/24/17	RC	R			
14.02		ANCHOR PROFILE / SANDBLAST		W	8/24/17	RC	R			
14.03		PRIMER		W	8/24/17	RC	R			
14.04		MIDDLE COAT		W	8/24/17	RC	R			
14.05		FINISH		W	8/24/17	RC	R			
14.06		DRY FILM THICKNESS		H	9/18/17	RC	H			
14.07		OVERALL APPEARANCE		H	9/18/17	RC	H			
15.00		PRE-SHIPMENT								
15.01		FINAL INTERNAL CLEANING		W			H			
15.02		ATTACH BLINDS & COVERS		W			H			
15.03		MARKING		W			H			
15.04		NAMEPLATE REVIEW & ATTACHED		W			H			
15.00		DATA PACKAGE REVIEW		R			H			



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **CERTIFICATE OF COMPLIANCE**

**MANUFACTURED FOR:** UOP RUSSELL

**P.O. NUMBER:** 4500754097 **ITEM #:** V-402

**P.P.I. JOB NO.:** 5654 **P.P.I. SERIAL NO.:** 5654-1

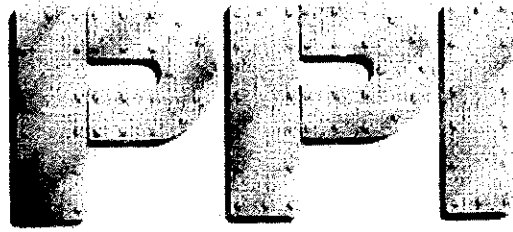
**DESCRIPTION:** COLD SEPARATOR

**HYDROSTATIC TESTED @** 1430 **PSIG.**

**PROFESSIONAL PROJECTS, INC. HEREBY CERTIFIES THAT THE CHEMICAL & PHYSICAL PROPERTIES OF ALL PARTS ON THE ABOVE PRESSURE VESSEL MEETS OR EXCEEDS THE MATERIAL SPECIFICATIONS OF THE ASME CODE. THE CONSTRUCTION & WORKMANSHIP HAVE BEEN DONE IN ACCORDANCE TO SECTION VIII DIVISION 1 OF THE ASME CODE.**

8/17/2017  
**DATE:** 8/11/2017

  
**Seth B. Westbrook**  
**QUALITY CONTROL MANAGER**



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

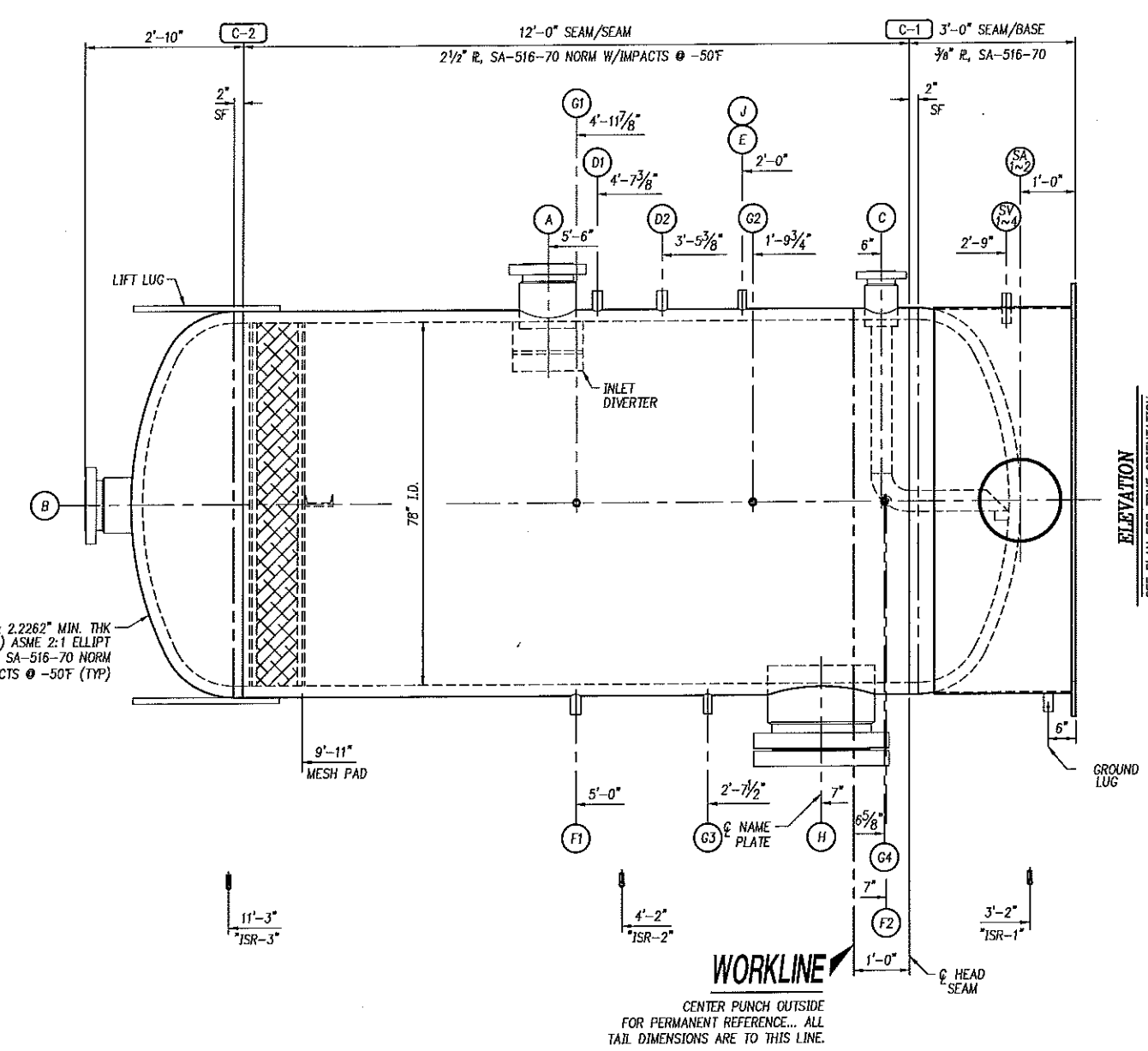
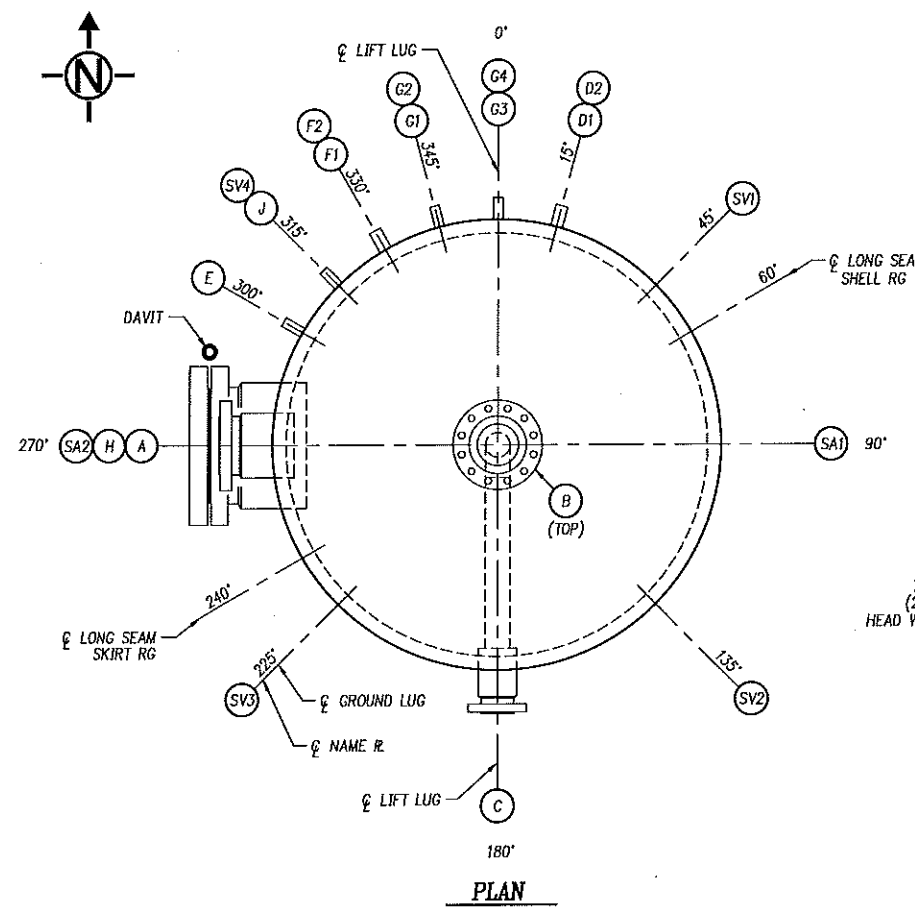
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Item: V-402, COLD SEPARATOR

# **Design Documentation**

**Pg. 1-3**      **Certified 'As-Built' Drawings**  
**Pg. 4-92**     **Calculations**

A handwritten signature in black ink, appearing to read 'J. G. [unclear]', is located in the lower right quadrant of the page.



**DESIGN DATA**  
 VESSEL DESIGNED PER THE 2015 EDITION OF THE ASME CODE SECTION VIII DIVISION 1, N/A APPENDIX A  
 CODE STAMP: REQ'D SERIAL NO: 5654-1 NATIONAL BOARD NO: 3170  
 DESIGN PRESSURE INTERNAL: 1100 PSI @ 150 DEG F  
 DESIGN PRESSURE EXTERNAL: N/A  
 HYDRO TEST: SHOP 1430 PSI @ MINIMUM -25F  
 MAMP: 1100 PSI @ 150 DEG F  
 MAP: 1100 PSI @ 70 DEG F  
 MWMT: -50 DEG F PWMT: REQ'D, HOLD AT 1150F ±25F FOR 120 MINUTES.  
 CORROSION ALLOWANCE: HEAD/SHELL: 1/16" NOZZLES: 1/16"  
 RADIOGRAPH: HEAD/SHELL: FULL UW-11(O) (BEFORE PWMT ONLY)  
 SHELL LONG: FULL UW-11(O)  
 SHELL CIRC: FULL UW-11(O)  
 ESTIMATED WEIGHT: FABRICATION: 36,003 LBS (BARE VESSEL WT.)  
 EMPTY: 49,867 LBS (FAB. WT. + INSULATION)  
 TEST: 70,757 LBS  
 OPERATING: 56,771 LBS  
 INSULATION: 2" THK. FIRE PROOFING: N/A INSPECTION BY: ONESIC

**MATERIAL SPECIFICATIONS**  
 SHELL SA-516-70 NORM W/IMPACTS @ -50F FLANGES SA-350-LF2 CL. 1 125-250 RMS  
 HEADS SA-516-70 NORM W/IMPACTS @ -50F SUPPORTS SA-516-70  
 CPLGS SA-350-LF2 CL. 1 INTERIORS AS NOTED  
 STUDS SA-193-B7 CAD PLTD REINF. PADS N/A  
 NUTS SA-194-2H CAD PLTD NOZZLE NECKS SA-106B / SA-350-LF2 CL. 1  
 GASKETS 1/8" THK, 316 SS SPIRAL WOUND, FLEXIBLE GRAPHITE FILLED, C.S. OUTER RING

**WELDING PROCEDURES**

WPS No.	POR No.	PROCESS	JOINT	COMMENTS
151 DCP	151-1 DCP	GMAW/FCAW/SAW	ROUND & LONG SEAMS	
149 DCP	149-1 DCP	GMAW/FCAW	ALL ATTACHMENTS NOZZLE TO HEAD & SHELL	

**COATING REQUIREMENTS**  
 EXTERNAL SURFACES OF VESSEL PER SYSTEM 3  
 1) SANDBLAST PER SSPC-SP6  
 2) PRIMER: SHERWIN WILLIAMS MACROPOXY 646 FAST CURE EPOXY B58-600, 4.0-6.0 MILS D.F.T.  
 3) INTERMEDIATE PRIMER: SHERWIN WILLIAMS MACROPOXY 646 FAST CURE EPOXY B58-600, 4.0-6.0 MILS D.F.T.  
 I.S. & O.S. OF SKIRT & PROTRUSIONS OUTSIDE INSULATION:  
 4) FINISH: SHERWIN WILLIAMS HI-SOLIDUS POLYURETHANE B65 SERIES B60-V30, 3.0-4.0 MILS D.F.T.  
 FINISH COLOR: SHERWIN WILLIAMS STRUCTURAL GRAY SW4031.

- GENERAL NOTES**
- ALL BOLT HOLES SHALL EVENLY STRADDLE NORMAL VESSEL CENTERLINES.
  - VESSELS SHALL BE THOROUGHLY DRAINED OF TEST MEDIUM AND CLEANED INSIDE AND OUT AND SHALL BE FREE OF ALL DIRT AND REFUSE.
  - ALL MACHINED SURFACES AND THREADS SHALL BE PROTECTED WITH A RUST PREVENTATIVE.
  - ALL OPEN FLANGES SHALL BE SUPPLIED WITH WOODEN SHIPPING COVERS.
  - THREADED TEST HOLES SHALL BE LEFT UNPLUGGED, BUT GREASED.
  - VESSEL ITEM NUMBER SHALL BE PROMINENTLY PAINTED ON TWO SIDES OF THE VESSEL IN 3" HIGH LETTERS.
  - ALL ITEMS SHIPPED LOOSE SHALL BE TAGGED WITH THE VESSEL ITEM NUMBER, PURCHASE ORDER NUMBER, AND NAME OF THE PARTS AND SHALL BE PROPERLY PROTECTED FOR SHIPMENT.
  - MINIMUM PRODUCTION IMPACT TEST VALUES = 16ftlbs/11ftlbs @ -50F

UOP JOB NO.: J-447

FILE NAME: 5654-1  
 PLOT DATE: 1/17/17  
 PLOT TIME: 3:00  
 BY: MLR

**PPI Professional Projects, Inc.**  
 P.O. BOX 618 (18115 TELGE RD.) CYPRESS, TEXAS 77429

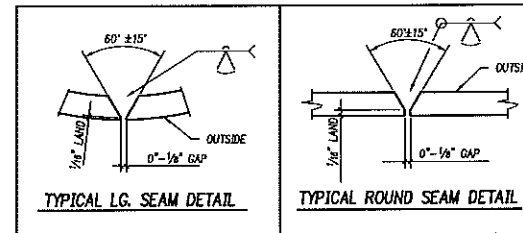
TITLE  
 78" ID x 12'-0" SEAM/SEAM  
 ITEM: V-402, COLD SEPARATOR  
 PLAN, ELEVATION & GENERAL NOTES

CUSTOMER: UOP RUSSELL

CUSTOMER P.O. NO.	PPI NO.	DATE	DATE
4500754097	5654	1/17/17	1/17/17

DRAWN: MLR CHECKED: MUD  
 SHEET NUMBER: 1 REVISION NO.: 1

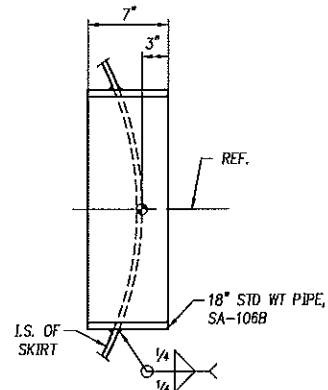
MARK	SIZE	TYPE	CLASS	IDENTIFIER	O.S. PROJ.	I.S. PROJ.
SV1~4	1.5			SKIRT VENT (4)		
SA1~2	18			SKIRT ACCESS (2)		
J	0.75	CPLG	6000#	TE	3 3/4"	-
H	18	HB	600#	MANWAY	11 3/4"	3 3/4"
G4	0.75	CPLG	6000#	LG	3 3/4"	-
G3	0.75	CPLG	6000#	LG	3 3/4"	-
G2	0.75	CPLG	6000#	LG	3 3/4"	-
G1	0.75	CPLG	6000#	LG	3 3/4"	-
F2	1	CPLG	6000#	LT	3 3/4"	-
F1	1	CPLG	6000#	LT	3 3/4"	-
E	0.75	CPLG	6000#	TI	3 3/4"	-
D2	1	CPLG	6000#	LSHH	3 3/4"	-
D1	1	CPLG	6000#	LSHH	3 3/4"	-
C	4	HB	600#	LIQUID OUTLET W/SYPHON	8"	1 1/2"
B	8	HB	600#	VAPOR OUTLET	10 1/4"	-
A	8	HB	600#	INLET W/DIVERTER	10"	1 1/2"



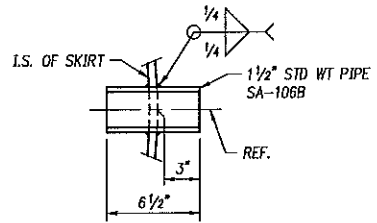
**NAME PLATE FACSIMILE & BRACKET DETAILS**  
 ONE (1) REQUIRED

HEAD MAT'L	SA-516-70M	THK	2.2262"
SHELL MAT'L	SA-516-70M	THK	2.5"
HYDRO TEST	1430	PSI	COR. ALLOW. 1/16"
EST. WT. EMPTY	40,667	LBS	
ITEM:	V-402, COLD SEPARATOR		
P.O.:	4500754097		

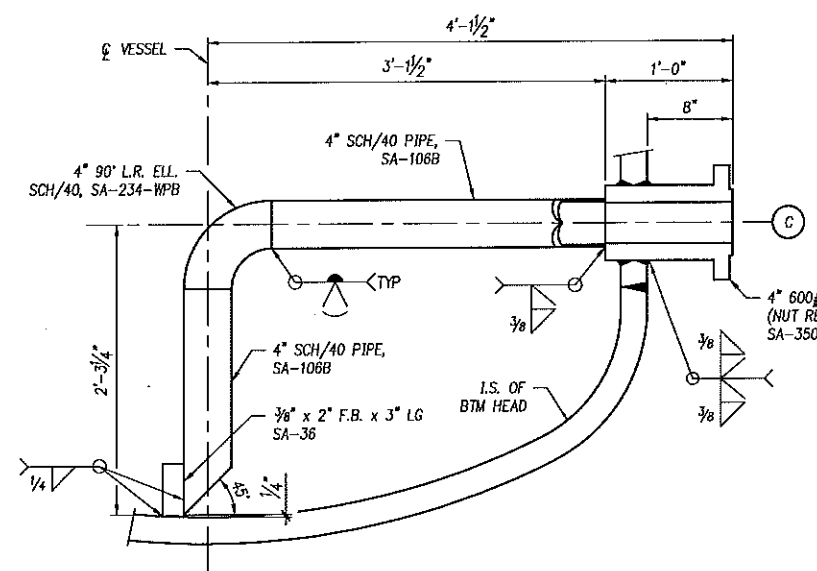
CERTIFIED AS-BUILT



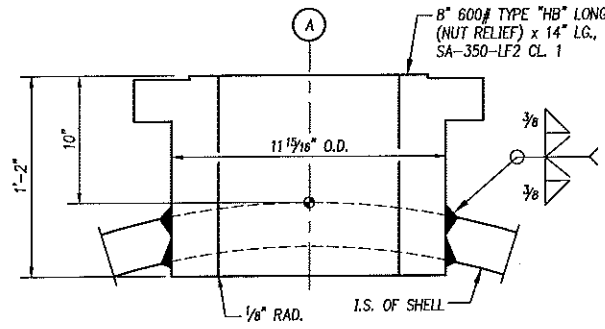
**DETAIL OF 18" SKIRT ACCESS**  
TWO (2) REQ'D MK "SA1-2"



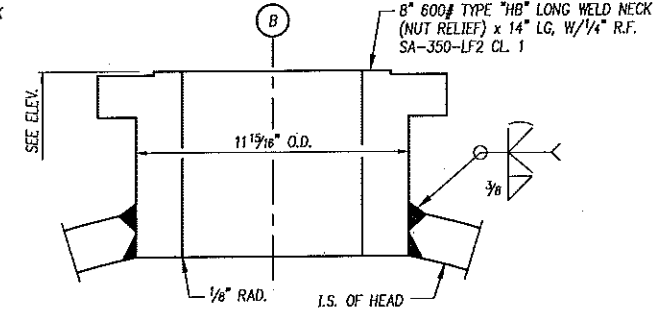
**DETAIL OF 1 1/2" SKIRT VENT**  
FOUR (4) REQ'D MK "SV1-4"



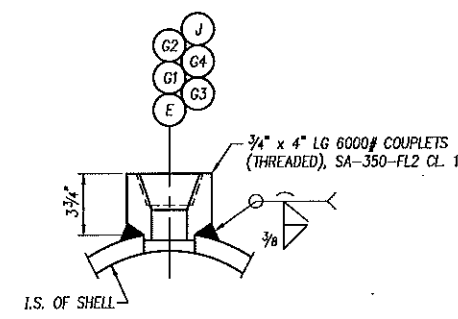
**DETAIL OF 4" 600# NOZZLE MK "C" W/ SYPHON**  
ONE (1) REQ'D



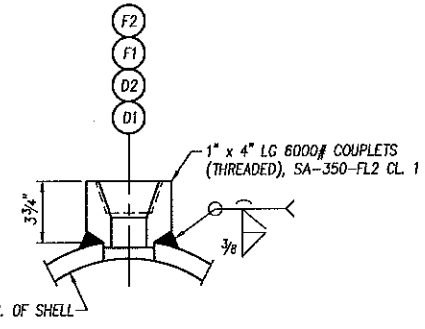
**DETAIL OF 8" 600# NOZZLE MK "A"**  
ONE (1) REQ'D



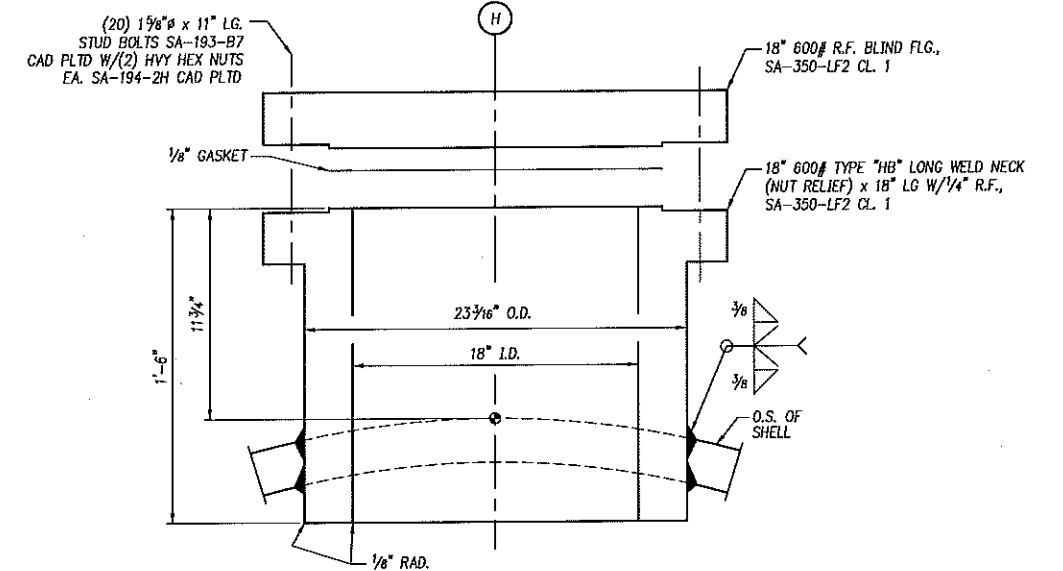
**DETAIL OF 8" 600# NOZZLE MK "B"**  
ONE (1) REQ'D



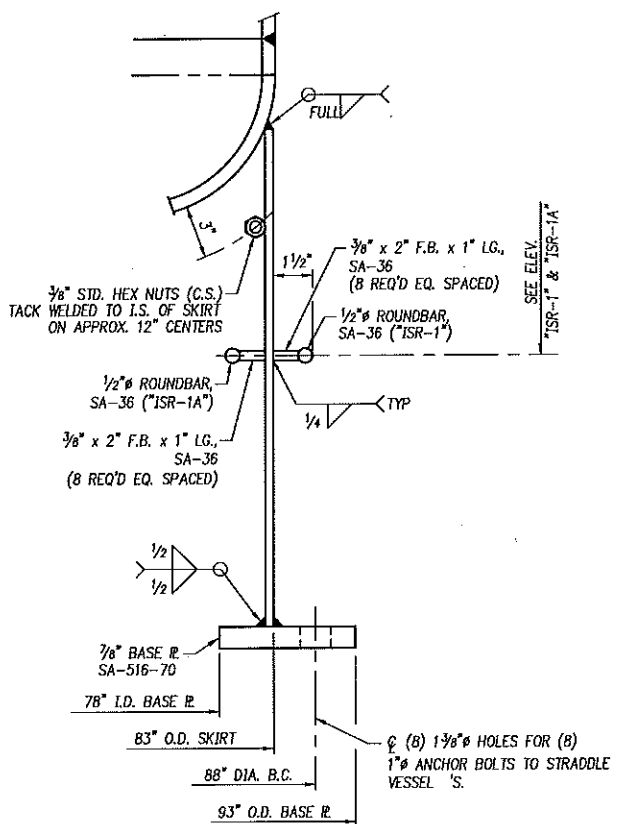
**DETAIL OF 3/4" 6000# COUPLINGS**  
MK "E, G1, G2, G3 G4, & J"  
SIX (6) REQ'D



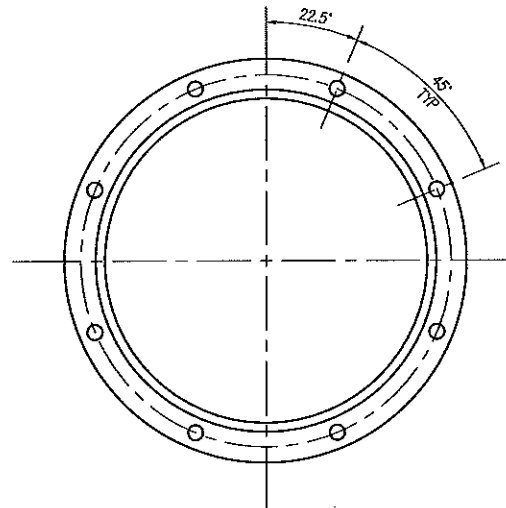
**DETAIL OF 1" 6000# COUPLINGS**  
MK "D1, D2, F1, & F2"  
FOUR (4) REQ'D



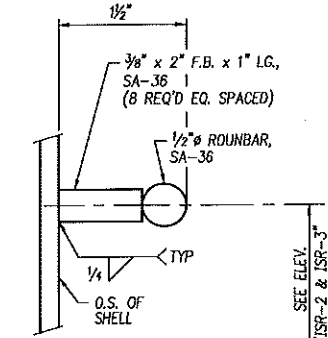
**DETAIL OF 18" 600# MANWAY MK "H"**  
ONE (1) REQ'D



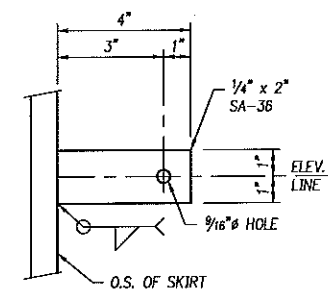
**BASEPLATE DETAIL**



**BASE PLAN**



**INSULATION SUPPORT RING**  
ONE (1) REQ'D EA. MK "ISR-2 & ISR-3"  
TWO (2) TOTAL REQ'D



**GROUNDING LUG DETAIL**  
ONE (1) REQ'D

NO.	REVISION	BY	DATE
1	ADDED P.O. NUMBER	MLR	9/11/17
0	ISSUED FOR CUSTOMER APPROVAL	MLR	1/17/17

FILE NAME: 5654-1  
PLOT DATE: 1/17/17  
PLOT TIME: 3:00  
BY: MLR

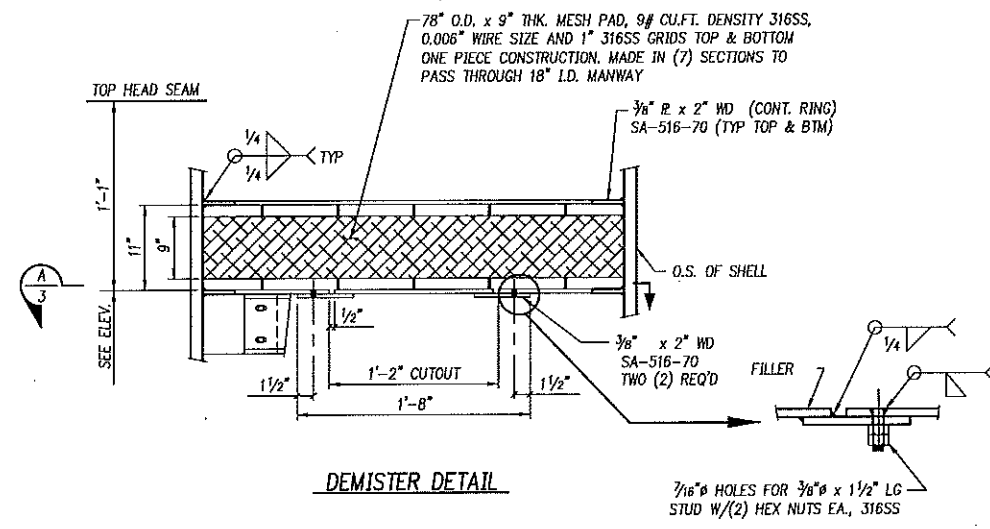
**PPI Professional Projects, Inc.**  
P.O. BOX 818 (18115 TELGE RD.) CYPRESS, TEXAS 77429

TITLE: 78" ID x 12'-0" SEAM/SEAM  
ITEM: V-402, COLD SEPARATOR  
DETAILS

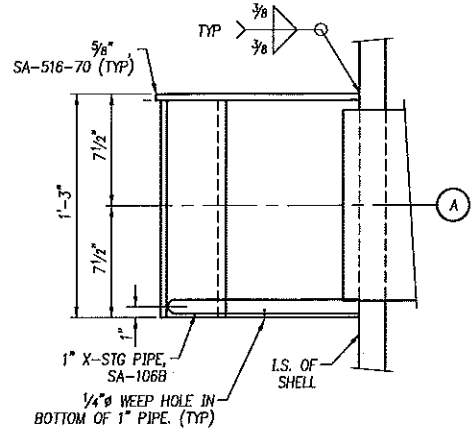
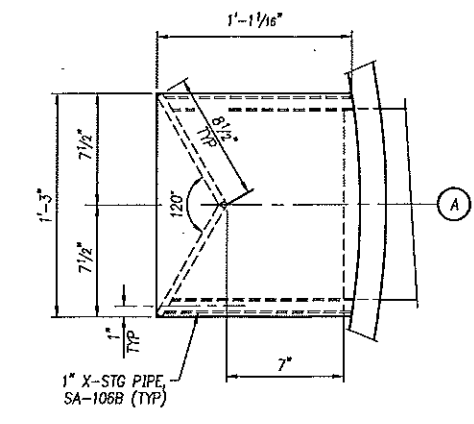
CUSTOMER: UOP RUSSELL

CUSTOMER P.O. NO. 4500754097	PPI NO. 5654
DRAWN MLR	CHECKED MUD
DATE 1/17/17	DATE 1/17/17
DRAWING NO. S/O 5654-1	SHEET NUMBER 2
	REVISION NO. 1

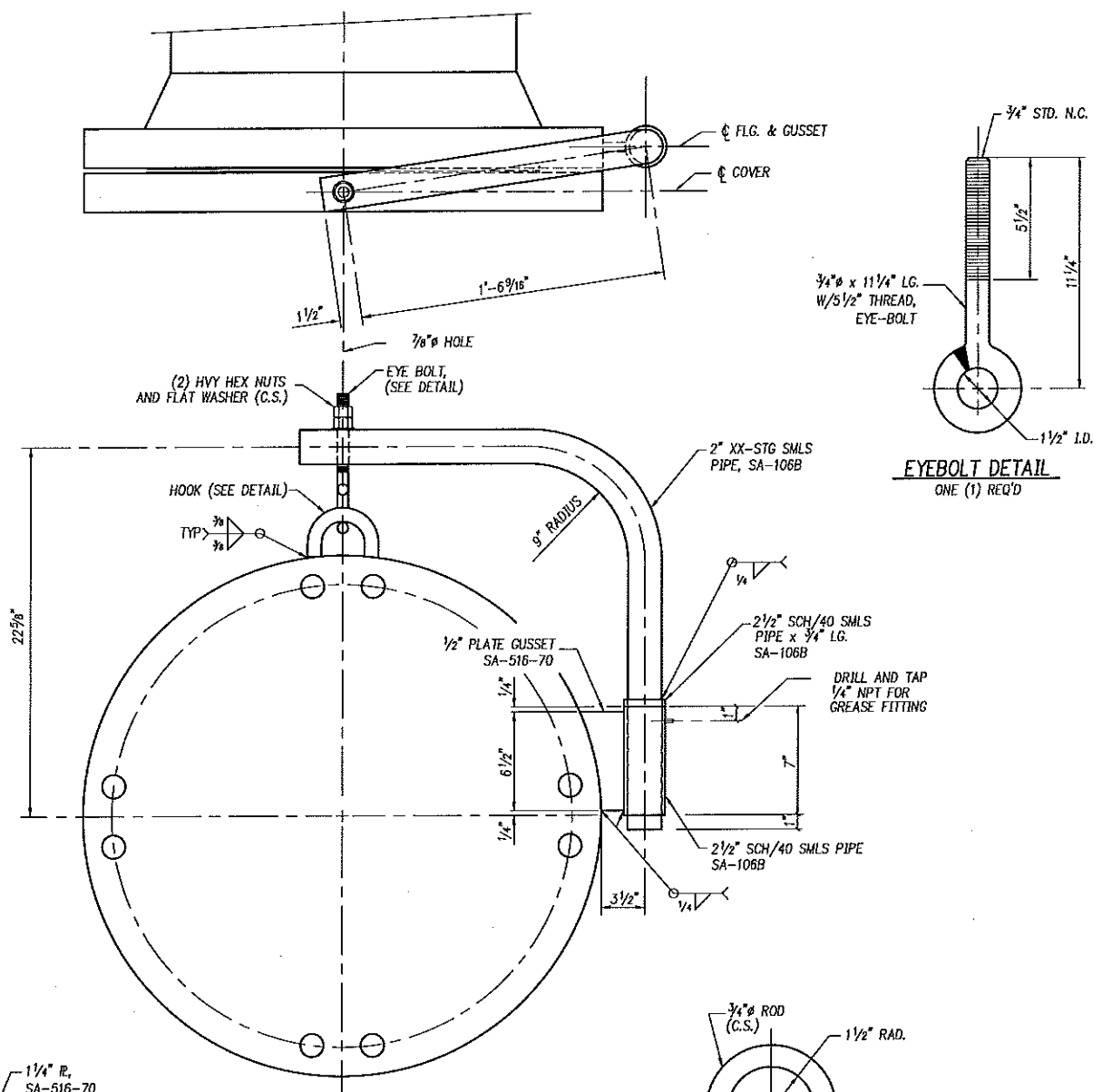
CERTIFIED AS-BUILT



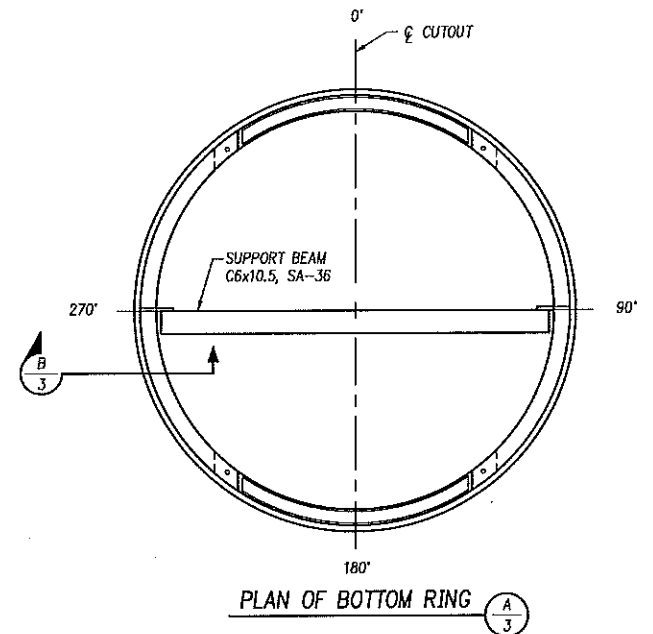
**DEMISTER DETAIL**



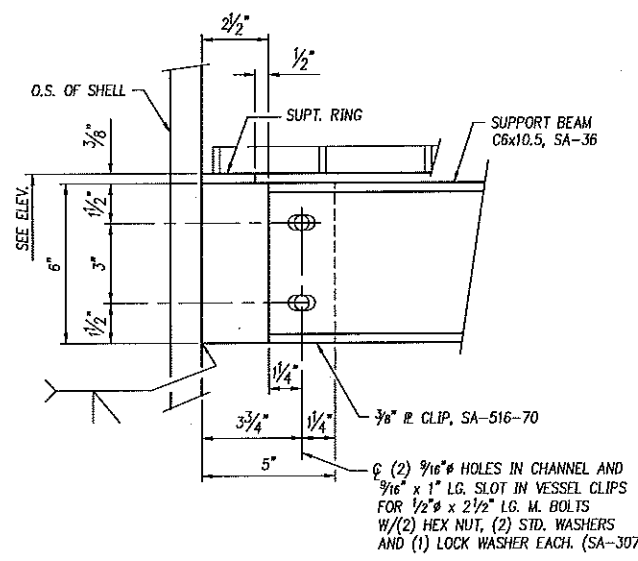
**DETAIL OF INLET DIVERTER**  
ONE (1) REQ'D NOZZLE MK "A"



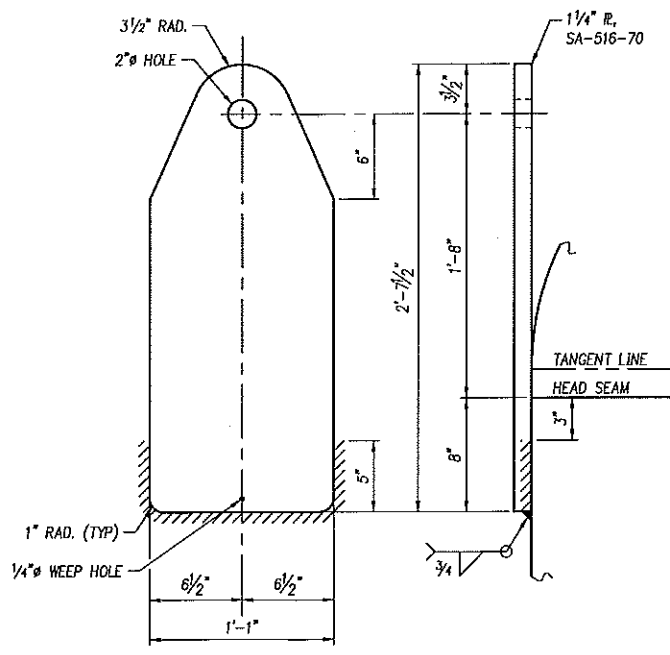
**DETAIL OF 18" 600# MANHOLE DAVIT**  
ONE (1) REQ'D FOR MK "H"  
SEE PLAN FOR TRUE ORIENTATION



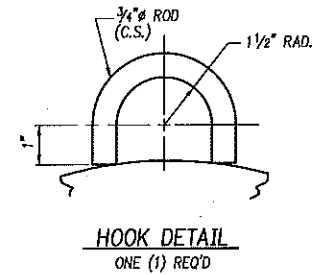
**PLAN OF BOTTOM RING**



**BEAM SUPPORT CLIP DETAIL**



**DETAIL OF LIFTING LUG**  
TWO (2) REQ'D



**HOOK DETAIL**  
ONE (1) REQ'D

NO.	REVISION	BY	DATE
1	ADDED P.O. NUMBER	MLR	9/11/17
0	ISSUED FOR CUSTOMER APPROVAL	MLR	1/17/17

**PPI Professional Projects, Inc.**  
P.O. BOX 618 (1815 TELGE RD.) CYPRESS, TEXAS 77429

FILE NAME: 5654-1  
PLOT DATE: 1/17/17  
PLOT TIME: 3:00  
BY: MLR

**78" ID x 12'-0" SEAM/SEAM**  
**ITEM: V-402, COLD SEPARATOR**  
**DETAILS**

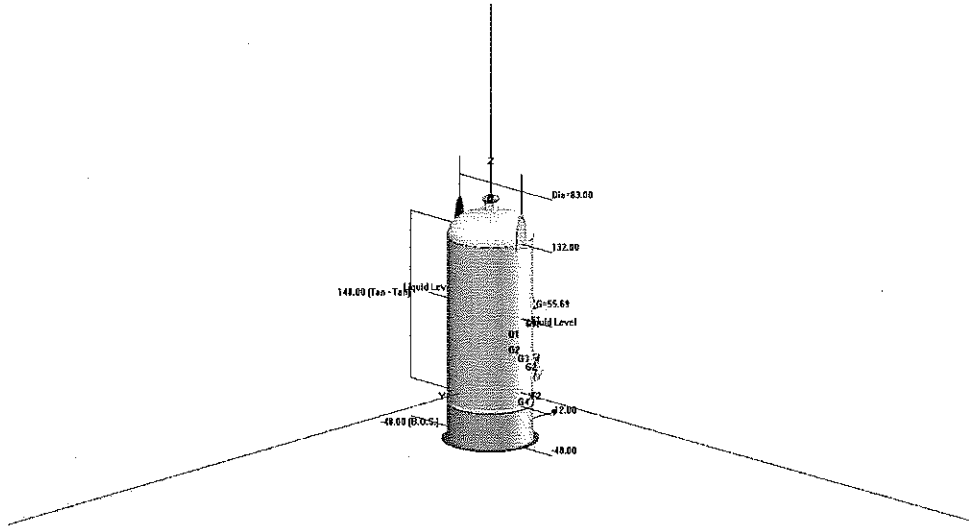
CUSTOMER: UOP RUSSELL

CUSTOMER P.O. NO. 4500754097	PPI NO. 5654
DRAWN MLR	CHECKED MUD
DATE 1/17/17	DATE 1/17/17
DRAWING NO. S/O 5654-1	SHEET NUMBER 3
	REVISION NO. 1

**CERTIFIED AS-BUILT**

# PROFESSIONAL PROJECTS, INC

CYPRESS, TEXAS



## COMPRESS Pressure Vessel Design Calculations

**Item:** V-402, COLD SEPARATOR  
**Shop Order:** 5654-1, Job No. 5654  
**Customer:** UOP RUSSELL LLC, J-447  
**Designer:** Lorraine Rodriguez  
**Date:** January 17, 2017  
**Vessel Name:** 5654-1 CALCS

King Design Group, Inc  
14011 Park Drive #113  
Tomball, Tx 77377  
markkdg@sbcglobal.net

A handwritten signature in black ink, appearing to read 'Lorraine Rodriguez'.

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<u>TI (E)</u> .....	52/86
<u>LT (F1)</u> .....	54/86
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<u>TE (J)</u> .....	69/86
<u>Liquid Level</u> .....	71/86
<u>LIFTING LUG</u> .....	72/86
<u>TAILING LUG</u> .....	80/86

## Revision History

Revisions			
No.	Date	Operator	Notes
0	1/17/2017	KDG3	ISSUED FOR APPROVAL

## Settings Summary

<b>COMPRESS 2016 Build 7600</b>	
<b>ASME Section VIII Division 1, 2015 Edition</b>	
Units	U.S. Customary
Datum Line Location	12.00" from bottom seam
Vessel Design Mode	Get Thickness from Pressure
Minimum thickness	0.0625" per UG-16(b)
Design for cold shut down only	No
Design for lethal service (full radiography required)	No
Design nozzles for	Design P only
Corrosion weight loss	100% of theoretical loss
UG-23 Stress Increase	1.20
Skirt/legs stress increase	1.0
Minimum nozzle projection	4"
Juncture calculations for $\alpha > 30$ only	No
Preheat P-No 1 Materials $> 1.25"$ and $\leq 1.50"$ thick	Yes
UG-37(a) shell tr calculation considers longitudinal stress	No
Cylindrical shells made from pipe are entered as minimum thickness	No
Nozzles made from pipe are entered as minimum thickness	No
ASME B16.9 fittings are entered as minimum thickness	No
Butt welds	Tapered per Figure UCS-66.3(a)
Disallow Appendix 1-5, 1-8 calculations under 15 psi	No
<b>Hydro/Pneumatic Test</b>	
Shop Hydrotest Pressure	1.3 times vessel MAWP
Test liquid specific gravity	1.00
Field Hydrotest Pressure	1.3 times vessel MAWP
Wind load present @ field	33% of design
Maximum stress during test	90% of yield
<b>Required Marking - UG-116</b>	
UG-116(e) Radiography	RT1
UG-116(f) Postweld heat treatment	HT
<b>Code Cases/Interpretations</b>	
Use Code Case 2547	No
Use Code Case 2695	No

Apply interpretation VIII-1-83-66	No
Apply interpretation VIII-1-86-175	Yes
Apply interpretation VIII-1-01-37	Yes
Apply interpretation VIII-1-01-150	No
Apply interpretation VIII-1-07-50	Yes
No UCS-66.1 MDMT reduction	No
No UCS-68(c) MDMT reduction	No
Disallow UG-20(f) exemptions	No
<b>UG-22 Loadings</b>	
UG-22(a) Internal or External Design Pressure	Yes
UG-22(b) Weight of the vessel and normal contents under operating or test conditions	Yes
UG-22(c) Superimposed static reactions from weight of attached equipment (external loads)	No
UG-22(d)(2) Vessel supports such as lugs, rings, skirts, saddles and legs	Yes
UG-22(f) Wind reactions	Yes
UG-22(f) Seismic reactions	Yes
UG-22(j) Test pressure and coincident static head acting during the test:	Yes
Note: UG-22(b),(c) and (f) loads only considered when supports are present.	

<b>License Information</b>	
Company Name	King Design Group
License	Commercial
License Key ID	30395
Support Expires	April 21, 2017

## Pressure Summary

Component Summary					
Identifier	P Design (psi)	T Design (°F)	MDMT (°F)	MDMT Exemption	Impact Tested
<u>TOP HEAD</u>	1,100	150	-58.9	Note 1	Yes
<u>Straight Flange on TOP HEAD</u>	1,100	150	-58.9	Note 2	Yes
<u>SHELL RG</u>	1,100	150	-58.6	Note 3	Yes
<u>Straight Flange on BOTTOM HEAD</u>	1,100	150	-58.6	Note 5	Yes
<u>BOTTOM HEAD</u>	1,100	150	-58.6	Note 4	Yes
<u>INLET W/DIVERTER (A)</u>	1,100	150	-55	Note 6	No
<u>VAPOR OUTLET (B)</u>	1,100	150	-55	Note 6	No
<u>LIQUID OUTLET (C)</u>	1,100	150	-55	Note 7	No
<u>LSHH (D1)</u>	1,100	150	-155	Note 8	No
<u>LSHH (D2)</u>	1,100	150	-155	Note 8	No
<u>TI (E)</u>	1,100	150	-155	Note 9	No
<u>LT (F1)</u>	1,100	150	-155	Note 10	No
<u>LT (F2)</u>	1,100	150	-155	Note 11	No
<u>LG (G1)</u>	1,100	150	-155	Note 12	No
<u>LG (G2)</u>	1,100	150	-155	Note 9	No
<u>LG (G3)</u>	1,100	150	-155	Note 9	No
<u>LG (G4)</u>	1,100	150	-155	Note 13	No
<u>MANWAY (H)</u>	1,100	150	-55	Note 14	No
<u>TE (I)</u>	1,100	150	-155	Note 9	No

Chamber Summary	
Design MDMT	-50 °F
Rated MDMT	-55 °F @ 1,100 psi
MAWP hot & corroded	1,100 psi
(1) This pressure chamber is not designed for external pressure.	

Notes for Maximum Pressure Rating	
Note #	Details
1.	Option to calculate MAP was not selected. See the Calculation->General tab of the Set Mode dialog.
2.	Option to calculate MAWP was not selected. See the Calculation->General tab of the Set Mode dialog.

Notes for MDMT Rating		
Note #	Exemption	Details
1.	<u>Straight Flange</u> governs MDMT	
2.	Material is impact tested per UG-84 to -50°F.	UCS-66(i) reduction of 8.9°F applied (ratio = 0.9115).
3.	Material is impact tested per UG-84 to -50°F.	UCS-66(i) reduction of 8.6°F applied (ratio = 0.9139).
4.	<u>Straight Flange</u> governs MDMT	
5.	Material is impact tested per UG-84 to -50°F.	UCS-66(i) reduction of 8.6°F applied (ratio = 0.914).
6.	Flange rating governs: Flange rated MDMT = -75.7°F Bolts rated MDMT per Fig UCS-66 note (c) = -55°F Flange is impact tested per material specification to -50°F.	UCS-66(i) reduction of 25.7°F applied (ratio = 0.7432).
7.	Flange rating governs: Flange rated MDMT = -75.5°F Bolts rated MDMT per Fig UCS-66 note (c) = -55°F Flange is impact tested per material specification to -50°F.	UCS-66(i) reduction of 25.5°F applied (ratio = 0.745).
8.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1012 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
9.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1164 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
10.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1011 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
11.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1014 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
12.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1163 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
13.	Nozzle is impact tested per material specification to -50°F.	Stress ratio = $0.1165 \leq 0.35$ , MDMT per UCS-66(b)(3) = -155°F..
14.	Flange rating governs: Flange rated MDMT = -75.5°F Bolts rated MDMT per Fig UCS-66 note (c) = -55°F Flange is impact tested per material specification to -50°F.	UCS-66(i) reduction of 25.5°F applied (ratio = 0.7447).

## Nozzle Schedule

Specifications									
Nozzle mark	Identifier	Size	Materials		Impact Tested	Normalized	Fine Grain	Flange	Blind
<u>A</u>	INLET W/DIVERTER	11.94 OD x 2.16	Nozzle	SA-350 LF2 Cl 1	No	No	No	NPS 8 Class 600 HB (or equiv.) A350 LF2 Cl.1	No
<u>B</u>	VAPOR OUTLET	11.94 OD x 2.16	Nozzle	SA-350 LF2 Cl 1	No	No	No	NPS 8 Class 600 HB (or equiv.) A350 LF2 Cl.1	No
<u>C</u>	LIQUID OUTLET	7.06 OD x 1.615	Nozzle	SA-350 LF2 Cl 1	No	No	No	NPS 4 Class 600 HB (or equiv.) A350 LF2 Cl.1	No
<u>D1</u>	LSHH	NPS 1 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>D2</u>	LSHH	NPS 1 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>E</u>	TI	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>E1</u>	LT	NPS 1 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>E2</u>	LT	NPS 1 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>G1</u>	LG	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>G2</u>	LG	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>G3</u>	LG	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>G4</u>	LG	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No
<u>H</u>	MANWAY	23.19 OD x 2.595	Nozzle	SA-350 LF2 Cl 1	No	No	No	NPS 18 Class 600 HB (or equiv.) A350 LF2 Cl.1	NPS 18 Class 600 A350 LF2 Cl.1
<u>J</u>	TE	NPS 0.75 Class 6000 - threaded	Nozzle	SA-350 LF2 Cl 1	No	No	No	N/A	No

## Nozzle Summary

Dimensions												
Nozzle mark	OD (in)	t <sub>n</sub> (in)	Req t <sub>n</sub> (in)	A <sub>1</sub> ?	A <sub>2</sub> ?	Shell			Reinforcement Pad		Corr (in)	A <sub>a</sub> /A <sub>r</sub> (%)
						Nom t (in)	Design t (in)	User t (in)	Width (in)	t <sub>pad</sub> (in)		
A	11.94	2.16	0.3819	Yes	Yes	2.5	2.2845		N/A	N/A	0.0625	161.0
B	11.94	2.16	0.3819	Yes	Yes	2.2262*	2.0038		N/A	N/A	0.0625	144.5
C	7.06	1.615	0.3075	Yes	Yes	2.5	2.2898		N/A	N/A	0.0625	197.1
D1	2.25	0.4675	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
D2	2.25	0.4675	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
E	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
F1	2.25	0.4675	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
F2	2.25	0.4675	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
G1	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
G2	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
G3	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
G4	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt
H	23.19	2.595	0.5791	Yes	Yes	2.5	2.2894		N/A	N/A	0.0625	111.9
J	1.75	0.35	0.125	Yes	Yes	2.5	N/A		N/A	N/A	0.0625	Exempt

\*Head minimum thickness after forming

Definitions	
t <sub>n</sub>	Nozzle thickness
Req t <sub>n</sub>	Nozzle thickness required per UG-45/UG-16
Nom t	Vessel wall thickness
Design t	Required vessel wall thickness due to pressure + corrosion allowance per UG-37
User t	Local vessel wall thickness (near opening)
A <sub>a</sub>	Area available per UG-37, governing condition
A <sub>r</sub>	Area required per UG-37, governing condition
Corr	Corrosion allowance on nozzle wall

## Thickness Summary

Component Data								
Component Identifier	Material	Diameter (In)	Length (in)	Nominal t (in)	Design t (in)	Total Corrosion (in)	Joint E	Load
TOP HEAD	SA-516 70	78 ID	21.7262	2.2262*	2.2183	0.0625	1.00	Internal
Straight Flange on TOP HEAD	SA-516 70	78 ID	2	2.5	2.2843	0.0625	1.00	Internal
SHELL RG	SA-516 70	78 ID	144	2.5	2.2902	0.0625	1.00	Internal
Straight Flange on BOTTOM HEAD	SA-516 70	78 ID	2	2.5	2.2903	0.0625	1.00	Internal
BOTTOM HEAD	SA-516 70	78 ID	21.7262	2.2262*	2.2254	0.0625	1.00	Internal
SKIRT	SA-516 70	82.25 ID	32.47	0.375	0.0588	0	0.55	Seismic

\*Head minimum thickness after forming

Definitions	
Nominal t	Vessel wall nominal thickness
Design t	Required vessel thickness due to governing loading + corrosion
Joint E	Longitudinal seam joint efficiency
Load	
Internal	Circumferential stress due to internal pressure governs
External	External pressure governs
Wind	Combined longitudinal stress of pressure + weight + wind governs
Seismic	Combined longitudinal stress of pressure + weight + seismic governs

## Weight Summary

Weight (lb) Contributed by Vessel Elements											
Component	Metal New*	Metal Corroded	Insulation	Insulation Supports	Lining	Piping + Liquid	Operating Liquid		Test Liquid		Surface Area ft <sup>2</sup>
							New	Corroded	New	Corroded	
TOP HEAD	5,024.9	4,894	115.1	100	0	0	0	0	2,597.3	2,613.2	60
SHELL RG	25,338.1	24,724.1	534.1	100	0	0	13,516.2	13,560.8	24,905	24,986.2	257
BOTTOM HEAD	5,095.4	4,962.5	115.1	100	0	0	2,587.3	2,602.8	2,587.3	2,602.8	61
SKIRT	870.4	870.4	0	0	0	0	0	0	0	0	118
BASE RING	496	496	0	0	0	0	0	0	0	0	30
<b>TOTAL:</b>	<b>36,824.7</b>	<b>35,946.9</b>	<b>764.3</b>	<b>300</b>	<b>0</b>	<b>0</b>	<b>16,103.5</b>	<b>16,163.5</b>	<b>30,089.6</b>	<b>30,202.2</b>	<b>525</b>

\*Shells with attached nozzles have weight reduced by material cut out for opening.

Weight (lb) Contributed by Attachments											
Component	Body Flanges		Nozzles & Flanges		Packed Beds	Ladders & Platforms	Trays	Tray Supports	Rings & Clips	Vertical Loads	Surface Area ft <sup>2</sup>
	New	Corroded	New	Corroded							
TOP HEAD	0	0	296.8	291	0	0	0	0	0	0	4
SHELL RG	0	0	2,220.7	2,188.3	0	0	0	0	248.2	0	29
BOTTOM HEAD	0	0	0	0	0	0	0	0	0	0	0
SKIRT	0	0	0	0	0	0	0	0	12.6	0	1
<b>TOTAL:</b>	<b>0</b>	<b>0</b>	<b>2,517.4</b>	<b>2,479.4</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>260.7</b>	<b>0</b>	<b>35</b>

Vessel Totals		
	New	Corroded
Operating Weight (lb)	56,771	55,915
Empty Weight (lb)	40,667	39,751
Test Weight (lb)	70,757	69,954
Surface Area (ft <sup>2</sup> )	559	-
Capacity** (US gal)	3,599	3,613

\*\*The vessel capacity does not include volume of nozzle, piping or other attachments.

Vessel Lift Condition	
Vessel Lift Weight, New (lb)	39,903
Center of Gravity from Datum (In)	55.6867

Note: Vessel lift weight includes weight of insulation supports as they are assumed to be shop installed.

## Hydrostatic Test

### Horizontal shop hydrostatic test based on MAWP per UG-99(b)

$$\begin{aligned}
 \text{Gauge pressure at } 70^{\circ}\text{F} &= \\
 &= 1.3 \cdot \text{MAWP} \cdot \text{LSR} \\
 &= 1.3 \cdot 1,100 \cdot 1 \\
 &= 1,430 \text{ psi}
 \end{aligned}$$

Horizontal shop hydrostatic test							
Identifier	Local test pressure (psi)	Test liquid static head (psi)	UG-99(b) stress ratio	UG-99(b) pressure factor	Stress during test (psi)	Allowable test stress (psi)	Stress excessive?
TOP HEAD (1)	1,433.05	3.05	1	1.30	22,595	34,200	No
Straight Flange on TOP HEAD	1,433.05	3.05	1	1.30	23,065	34,200	No
SHELL RG	1,433.05	3.05	1	1.30	23,065	34,200	No
Straight Flange on BOTTOM HEAD	1,433.05	3.05	1	1.30	23,065	34,200	No
BOTTOM HEAD	1,433.05	3.05	1	1.30	22,595	34,200	No
INLET W/DIVERTER (A)	1,431.78	1.78	1	1.30	25,147	51,300	No
LG (G1)	1,430.2	0.2	1	1.30	38,077	51,300	No
LG (G2)	1,430.2	0.2	1	1.30	38,077	51,300	No
LG (G3)	1,430.144	0.144	1	1.30	38,075	51,300	No
LG (G4)	1,430.144	0.144	1	1.30	38,075	51,300	No
LIQUID OUTLET (C)	1,433.429	3.429	1	1.30	23,272	51,300	No
LSHH (D1)	1,430.202	0.202	1	1.30	37,251	51,300	No
LSHH (D2)	1,430.202	0.202	1	1.30	37,251	51,300	No
LT (F1)	1,430.357	0.357	1	1.30	37,255	51,300	No
LT (F2)	1,430.357	0.357	1	1.30	37,255	51,300	No
MANWAY (H)	1,431.967	1.967	1	1.30	27,136	51,300	No
TE (J)	1,430.597	0.597	1	1.30	38,087	51,300	No
TI (E)	1,430.91	0.91	1	1.30	38,095	51,300	No
VAPOR OUTLET (B)	1,431.78	1.78	1	1.30	29,056	51,300	No

- (1) TOP HEAD limits the UG-99(b) stress ratio.
- (2)  $P_L$  stresses at nozzle openings have been estimated using the method described in Division 2 Part 4.5.
- (3)  $1.5 \cdot 0.9 \cdot S_y$  used as the basis for the maximum local primary membrane stress at the nozzle intersection  $P_L$ .
- (4) The zero degree angular position is assumed to be up, and the test liquid height is assumed to the top-most flange.

The test temperature of 70 °F is warmer than the minimum recommended temperature of -25 °F so the brittle fracture provision of UG-99(h) has been met.

**Vertical field hydrostatic test based on MAWP per UG-99(b)**

$$\begin{aligned} \text{Gauge pressure at } 70^\circ\text{F} &= \\ &= 1.3 \cdot \text{MAWP} \cdot \text{LSR} \\ &= 1.3 \cdot 1,100 \cdot 1 \\ &= 1,430 \text{ psi} \end{aligned}$$

Vertical field hydrostatic test							
Identifier	Local test pressure (psi)	Test liquid static head (psi)	UG-99(b) stress ratio	UG-99(b) pressure factor	Stress during test (psi)	Allowable test stress (psi)	Stress excessive?
TOP HEAD (1)	1,431.227	1.227	1	1.30	22,566	34,200	No
Straight Flange on TOP HEAD	1,431.227	1.227	1	1.30	23,035	34,200	No
SHELL RG	1,436.425	6.425	1	1.30	23,119	34,200	No
Straight Flange on BOTTOM HEAD	1,436.498	6.498	1	1.30	23,120	34,200	No
BOTTOM HEAD	1,437.201	7.201	1	1.30	22,660	34,200	No
INLET W/DIVERTER (A)	1,433.747	3.747	1	1.30	25,181	51,300	No
LG (G1)	1,433.85	3.85	1	1.30	38,174	51,300	No
LG (G2)	1,435.226	5.226	1	1.30	38,210	51,300	No
LG (G3)	1,434.874	4.874	1	1.30	38,201	51,300	No
LG (G4)	1,436.25	6.25	1	1.30	38,238	51,300	No
LIQUID OUTLET (C)	1,436.278	6.278	1	1.30	23,318	51,300	No
LSHH (D1)	1,434.017	4.017	1	1.30	37,350	51,300	No
LSHH (D2)	1,434.522	4.522	1	1.30	37,363	51,300	No
LT (F1)	1,433.85	3.85	1	1.30	37,346	51,300	No
LT (F2)	1,436.269	6.269	1	1.30	37,409	51,300	No
MANWAY (H)	1,436.064	6.064	1	1.30	27,214	51,300	No
TE (J)	1,435.145	5.145	1	1.30	38,208	51,300	No
TI (E)	1,435.145	5.145	1	1.30	38,208	51,300	No
VAPOR OUTLET (B)	1,430.371	0.371	1	1.30	29,028	51,300	No

(1) TOP HEAD limits the UG-99(b) stress ratio.  
 (2)  $P_L$  stresses at nozzle openings have been estimated using the method described in Division 2 Part 4.5.  
 (3)  $1.5 \cdot 0.9 \cdot S_y$  used as the basis for the maximum local primary membrane stress at the nozzle intersection  $P_L$ .

The test temperature of 70 °F is warmer than the minimum recommended temperature of -25 °F so the brittle fracture provision of UG-99(h) has been met.

**Wind Code**

<b>Building Code: ASCE 7-10</b>		
Elevation of base above grade	1.00 ft	
Increase effective outer diameter by	1.50 ft	
Wind Force Coefficient, $C_f$	0.7000	
Risk Category (Table 1.5-1)	III	
Basic Wind Speed, $V$	150.00 mph	
Exposure category	C	
Wind Directionality Factor, $K_d$	0.9500	
Topographic Factor, $K_{zt}$	1.0000	
Enforce min. loading of 16 psf	Yes	
<b>Vessel Characteristics</b>		
Height, $h$	16.9773 ft	
Minimum Diameter, $b$	Operating, Corroded	7.2500 ft
	Empty, Corroded	7.2500 ft
	Hydrotest, New, Field	7.2500 ft
Fundamental Frequency, $n_1$	Operating, Corroded	34.3783 Hz
	Empty, Corroded	38.1890 Hz
	Hydrotest, New, Field	28.7008 Hz
Damping coefficient, $\beta$	Operating, Corroded	0.0250
	Empty, Corroded	0.0210
	Hydrotest, New, Field	0.0260

Table Lookup Values

<b>2.4.1 Basic Load Combinations for Allowable Stress Design</b>	
<b>Load combinations considered in accordance with ASCE section 2.4.1:</b>	
5.	$D + P + P_s + 0.6W$
7.	$0.6D + P + P_s + 0.6W$
Parameter Description	
$D$	= Dead load
$P$	= Internal or external pressure load
$P_s$	= Static head load
$W$	= Wind load

**Wind Deflection Reports:**

Operating, Corroded

Empty, Corroded

Hydrotest, New, field

Wind Pressure Calculations

Wind Deflection Report: Operating, Corroded								
Component	Elevation of Bottom above Base (in)	Effective OD (ft)	Elastic Modulus E (10 <sup>6</sup> psi)	Inertia I (ft <sup>4</sup> )	Platform Wind Shear at Bottom (lb <sub>f</sub> )	Total Wind Shear at Bottom (lb <sub>f</sub> )	Bending Moment at Bottom (lb <sub>f</sub> -ft)	Deflection at Top (in)
TOP HEAD	180.0014	8.73	29.0	*	0	271	239	0.0011
SHELL RG	36.0014	8.75	29.0	24.16	0	2,124	23,813	0.0009
BOTTOM HEAD (top)	32.47	8.73	29.0	*	0	2,169	24,445	0.0001
SKIRT	0	8.42	26.0	4.006	0	2,569	30,855	0.0001
*Moment of Inertia I varies over the length of the component								

Wind Deflection Report: Empty, Corroded								
Component	Elevation of Bottom above Base (in)	Effective OD (ft)	Elastic Modulus E (10 <sup>6</sup> psi)	Inertia I (ft <sup>4</sup> )	Platform Wind Shear at Bottom (lb <sub>f</sub> )	Total Wind Shear at Bottom (lb <sub>f</sub> )	Bending Moment at Bottom (lb <sub>f</sub> -ft)	Deflection at Top (in)
TOP HEAD	180.0014	8.73	29.4	*	0	271	239	0.001
SHELL RG	36.0014	8.75	29.4	24.16	0	2,124	23,813	0.0008
BOTTOM HEAD (top)	32.47	8.73	29.4	*	0	2,169	24,445	0.0001
SKIRT	0	8.42	29.4	4.006	0	2,569	30,855	0.0001
*Moment of Inertia I varies over the length of the component								

Wind Deflection Report: Field Hydrotest, New								
Component	Elevation of Bottom above Base (in)	Effective OD (ft)	Elastic Modulus E (10 <sup>6</sup> psi)	Inertia I (ft <sup>4</sup> )	Platform Wind Shear at Bottom (lb <sub>f</sub> )	Total Wind Shear at Bottom (lb <sub>f</sub> )	Bending Moment at Bottom (lb <sub>f</sub> -ft)	Deflection at Top (in)
TOP HEAD	180.0014	8.73	29.4	*	0	140	123	0.0007
SHELL RG	36.0014	8.75	29.4	24.72	0	1,148	17,116	0.0006
BOTTOM HEAD (top)	32.47	8.73	29.4	*	0	1,172	17,458	0.0001
SKIRT	0	8.42	29.4	4.006	0	1,391	20,926	0.0001
*Moment of Inertia I varies over the length of the component								

**Wind Pressure (WP) Calculations**

Gust Factor (G<sub>f</sub>) Calculations

$$\begin{aligned}
 K_z &= 2.01 * (Z/Z_0)^{2/\alpha} \\
 &= 2.01 * (Z/900.00)^{0.2105} \\
 q_z &= 0.00256 * K_z * K_{zt} * K_d * V^2 \\
 &= 0.00256 * K_z * 1.0000 * 0.9500 * 150.0000^2 \\
 &= 54.7200 * K_z \\
 WP &= 0.6 * q_z * G * C_f \text{ (Minimum 16 lb/ft}^2\text{)} \\
 &= 0.6 * q_z * G * 0.7000 \text{ (Minimum 16 lb/ft}^2\text{)}
 \end{aligned}$$

Design Wind Pressures							
Height Z (')	Kz	qz (psf)	WP (psf)				
			Operating	Empty	Hydrotest New	Hydrotest Corroded	Vacuum
15.0	0.8489	46.45	17.55	17.55	9.60	N.A.	N.A.
20.0	0.9019	49.35	18.65	18.65	9.60	N.A.	N.A.

Design Wind Force determined from:  $F = \text{Pressure} * A_f$ , where  $A_f$  is the projected area.

### Gust Factor Calculations

Operating, Corroded

Empty, Corroded

Hydrotest, New, field

### Gust Factor Calculations: Operating, Corroded

Vessel is considered a rigid structure as  $n_1 = 34.3783 \text{ Hz} \geq 1 \text{ Hz}$ .

$$z^- = \max(0.60 * h, z_{\min})$$

$$= \max(0.60 * 16.9773, 15.0000)$$

$$= 15.0000$$

$$I_z^- = C * (33 / z^-)^{1/6}$$

$$= 0.2000 * (33 / 15.0000)^{1/6}$$

$$= 0.2281$$

$$L_z^- = I * (z^- / 33)^{0.2000}$$

$$= 500.0000 * (15.0000 / 33)^{0.2000}$$

$$= 427.0566$$

$$Q = \text{Sqr}(1 / (1 + 0.63 * ((b + h) / L_z^-)^{0.63}))$$

$$= \text{Sqr}(1 / (1 + 0.63 * ((7.2500 + 16.9773) / 427.0566)^{0.63}))$$

$$= 0.9520$$

$$G = 0.925 * (1 + 1.7 * g_Q * I_z^- * Q) / (1 + 1.7 * g_v * I_z^-)$$

$$= 0.925 * (1 + 1.7 * 3.40 * 0.2281 * 0.9520) / (1 + 1.7 * 3.40 * 0.2281)$$

$$= 0.8998$$

### Gust Factor Calculations: Empty, Corroded

Vessel is considered a rigid structure as  $n_1 = 38.1890 \text{ Hz} \geq 1 \text{ Hz}$ .

$$z^- = \max(0.60 * h, z_{\min})$$

$$= \max(0.60 * 16.9773, 15.0000)$$

$$= 15.0000$$

$$I_z^- = C * (33 / z^-)^{1/6}$$

$$= 0.2000 * (33 / 15.0000)^{1/6}$$

$$= 0.2281$$

$$L_z^- = I * (z^- / 33)^{0.2000}$$

$$= 500.0000 * (15.0000 / 33)^{0.2000}$$

$$= 427.0566$$

$$\begin{aligned}
Q &= \text{Sqr}(1 / (1 + 0.63 * ((b + h) / L_z)^{0.63})) \\
&= \text{Sqr}(1 / (1 + 0.63 * ((7.2500 + 16.9773) / 427.0566)^{0.63})) \\
&= 0.9520 \\
G &= 0.925 * (1 + 1.7 * g_Q * I_z * Q) / (1 + 1.7 * g_v * I_z) \\
&= 0.925 * (1 + 1.7 * 3.40 * 0.2281 * 0.9520) / (1 + 1.7 * 3.40 * 0.2281) \\
&= 0.8998
\end{aligned}$$

**Gust Factor Calculations: Hydrotest, New, field**

Vessel is considered a rigid structure as  $n_1 = 28.7008 \text{ Hz} \geq 1 \text{ Hz}$ .

$$\begin{aligned}
z^- &= \max(0.60 * h, z_{\min}) \\
&= \max(0.60 * 16.9773, 15.0000) \\
&= 15.0000
\end{aligned}$$

$$\begin{aligned}
I_z^- &= c * (33 / z^-)^{1/6} \\
&= 0.2000 * (33 / 15.0000)^{1/6} \\
&= 0.2281
\end{aligned}$$

$$\begin{aligned}
L_z^- &= l * (z^- / 33)^{ep} \\
&= 500.0000 * (15.0000 / 33)^{0.2000} \\
&= 427.0566
\end{aligned}$$

$$\begin{aligned}
Q &= \text{Sqr}(1 / (1 + 0.63 * ((b + h) / L_z)^{0.63})) \\
&= \text{Sqr}(1 / (1 + 0.63 * ((7.2500 + 16.9773) / 427.0566)^{0.63})) \\
&= 0.9520
\end{aligned}$$

$$\begin{aligned}
G &= 0.925 * (1 + 1.7 * g_Q * I_z * Q) / (1 + 1.7 * g_v * I_z) \\
&= 0.925 * (1 + 1.7 * 3.40 * 0.2281 * 0.9520) / (1 + 1.7 * 3.40 * 0.2281) \\
&= 0.8998
\end{aligned}$$

Table Lookup Values	
$\alpha = 9.5000, z_g = 900.00 \text{ ft}$	[Table 26.9-1, page 256]
$c = 0.2000, l = 500.0000, ep = 0.2000$	[Table 26.9-1, page 256]
$a^- = 0.1538, b^- = 0.6500$	[Table 26.9-1, page 256]
$z_{\min} = 15.0000 \text{ ft}$	[Table 26.9-1, page 256]
$g_Q = 3.40$	[26.9.4 page 254]
$g_v = 3.40$	[26.9.4 page 254]

**Seismic Code**

<b>Building Code: ASCE 7-10 ground supported</b>		
<b>Site Class</b>		D
<b>Importance Factor, I<sub>e</sub></b>		1.2500
<b>Spectral Response Acceleration at short period (% g), S<sub>s</sub></b>		100.00%
<b>Spectral Response Acceleration at period of 1 sec (% g), S<sub>1</sub></b>		40.00%
<b>Response Modification Coefficient from Table 15.4-2, R</b>		3.0000
<b>Acceleration-based Site Coefficient, F<sub>a</sub></b>		1.1000
<b>Velocity-based Site Coefficient, F<sub>v</sub></b>		1.6000
<b>Long-period Transition Period, T<sub>L</sub></b>		12.0000
<b>Redundancy factor, ρ</b>		1.0000
<b>Risk Category (Table 1.5-1)</b>		III
<b>User Defined Vertical Accelerations Considered</b>		No
<b>Vessel Characteristics</b>		
<b>Height</b>		16.9773 ft
<b>Weight</b>	Operating, Corroded	55,915 lb
	Empty, Corroded	39,751 lb
<b>Period of Vibration Calculation</b>		
<b>Fundamental Period, T</b>	Operating, Corroded	0.029 sec (f = 34.4 Hz)
	Empty, Corroded	0.026 sec (f = 38.2 Hz)

The fundamental period of vibration T (above) is calculated using the Rayleigh method of approximation

$$T = 2 * \pi * \text{Sqr}(\{\text{Sum}(W_i * y_i^2)\} / \{g * \text{Sum}(W_i * y_i)\}), \text{ where}$$

W<sub>i</sub> is the weight of the i<sup>th</sup> lumped mass, and  
y<sub>i</sub> is its deflection when the system is treated as a cantilever beam.

12.4.2.3 Basic Load Combinations for Allowable Stress Design			
Load combinations considered in accordance with ASCE section 2.4.1:			
5.	$D + P + P_s + 0.7E$	$= (1.0 + 0.14S_{DS})D + P + P_s + 0.7\rho Q_E$	
8.	$0.6D + P + P_s + 0.7E$	$= (0.6 - 0.14S_{DS})D + P + P_s + 0.7\rho Q_E$	
Parameter description			
$D$	= Dead load		
$P$	= Internal or external pressure load		
$P_s$	= Static head load		
$E$	= Seismic load	$= E_h +/ - E_v$	$= \rho Q_E +/ - 0.2S_{DS}D$

### Seismic Shear Reports:

Operating, Corroded

Empty, Corroded

Base Shear Calculations

Seismic Shear Report: Operating, Corroded					
Component	Elevation of Bottom above Base (in)	Elastic Modulus E (10 <sup>6</sup> psi)	Inertia I (ft <sup>4</sup> )	Seismic Shear at Bottom (lb <sub>f</sub> )	Bending Moment at Bottom (lb <sub>f</sub> -ft)
TOP HEAD	180.0014	29.0	*	2,180	2,285
SHELL RG	36.0014	29.0	24.1588	10,102	87,488
BOTTOM HEAD (top)	32.47	29.0	*	10,197	90,476
SKIRT	0	26.0	4.006	10,764	119,122
*Moment of Inertia I varies over the length of the component					

Seismic Shear Report: Empty, Corroded					
Component	Elevation of Bottom above Base (in)	Elastic Modulus E (10 <sup>6</sup> psi)	Inertia I (ft <sup>4</sup> )	Seismic Shear at Bottom (lb <sub>f</sub> )	Bending Moment at Bottom (lb <sub>f</sub> -ft)
TOP HEAD	180.0014	29.4	*	1,961	2,055
SHELL RG	36.0014	29.4	24.1588	7,237	72,566
BOTTOM HEAD (top)	32.47	29.4	*	7,285	74,703
SKIRT	0	29.4	4.006	7,652	95,063
*Moment of Inertia I varies over the length of the component					

### 11.4.3: Maximum considered earthquake spectral response acceleration

The maximum considered earthquake spectral response acceleration at short period,  $S_{MS}$

$$S_{MS} = E_a * S_a = 1.1000 * 100.00 / 100 = 1.1000$$

The maximum considered earthquake spectral response acceleration at 1 s period,  $S_{M1}$

$$S_{M1} = E_v * S_v = 1.6000 * 40.00 / 100 = 0.6400$$

### 11.4.4: Design spectral response acceleration parameters

Design earthquake spectral response acceleration at short period,  $S_{DS}$

$$S_{DS} = 2/3 * S_{MS} = 2/3 * 1.1000 = 0.7333$$

Design earthquake spectral response acceleration at 1 s period,  $S_{D1}$

$$S_{D1} = 2/3 * S_{M1} = 2/3 * 0.6400 = 0.4267$$

### 11.6 Seismic Design Category

The Risk Category is III.

From Table 11.6-1, the Seismic Design Category based on  $S_{DS} = 0.7333$  is D.

From Table 11.6-2, the Seismic Design Category based on  $S_{D1} = 0.4267$  is D.

This vessel is assigned to Seismic Design Category D.

### 12.4.2.3: Seismic Load Combinations: Vertical Term

Factor is applied to dead load.

$$\begin{aligned} \text{Compressive Side:} &= 1.0 + 0.14 * S_{DS} \\ &= 1.0 + 0.14 * 0.7333 \\ &= 1.1027 \end{aligned}$$

$$\begin{aligned} \text{Tensile Side:} &= 0.6 - 0.14 * S_{DS} \\ &= 0.6 - 0.14 * 0.7333 \\ &= 0.4973 \end{aligned}$$

### Base Shear Calculations

Operating, Corroded

Empty, Corroded

### Base Shear Calculations: Operating, Corroded

Paragraph 15.4.2:  $I < 0.06$ , so:

$$\begin{aligned} V &= 0.30 * S_{DS} * W * I_e \\ &= 0.30 * 0.7333 * 55,914.8359 * 1.2500 \\ &= 15,376.58 \text{ lb} \end{aligned}$$

### 12.4.2.1 Seismic Load Combinations: Horizontal Seismic Load Effect, $E_h$

$$Q_E = V$$

$$\begin{aligned} E_h &= 0.7 * \rho * Q_E \text{ (Only 70% of seismic load considered as per Section 2.4.1)} \\ &= 0.70 * 1.0000 * 15,376.58 \\ &= 10,763.61 \text{ lb} \end{aligned}$$

### Base Shear Calculations: Empty, Corroded

Paragraph 15.4.2:  $I < 0.06$ , so:

$$\begin{aligned} V &= 0.30 * S_{DS} * W * I_e \\ &= 0.30 * 0.7333 * 39,751.2969 * 1.2500 \\ &= 10,931.61 \text{ lb} \end{aligned}$$

### 12.4.2.1 Seismic Load Combinations: Horizontal Seismic Load Effect, $E_h$

$$Q_E = V$$

$$\begin{aligned} E_h &= 0.7 * \rho * Q_E \text{ (Only 70% of seismic load considered as per Section 2.4.1)} \\ &= 0.70 * 1.0000 * 10,931.61 \end{aligned}$$

= 7,652.12 lb

**TOP HEAD**

ASME Section VIII Division 1, 2015 Edition				
<b>Component</b>		Ellipsoidal Head		
<b>Material</b>		SA-516 70 (II-D p. 18, ln. 37)		
<b>Attached To</b>		SHELL RG		
<b>Impact Tested</b>	<b>Normalized</b>	<b>Fine Grain Practice</b>	<b>PWHT</b>	<b>Optimize MDMT/ Find MAWP</b>
Yes (-50°F)	Yes	No	Yes	No
		<b>Design Pressure (psi)</b>	<b>Design Temperature (°F)</b>	<b>Design MDMT (°F)</b>
<b>Internal</b>		1,100	150	-50
Static Liquid Head				
<b>Condition</b>		<b>P<sub>s</sub> (psi)</b>	<b>H<sub>s</sub> (in)</b>	<b>SG</b>
Test horizontal		3.05	84.5	1
Test vertical		1.16	32	1
Dimensions				
<b>Inner Diameter</b>		78"		
<b>Head Ratio</b>		2		
<b>Minimum Thickness</b>		2.2262"		
<b>Corrosion</b>	<b>Inner</b>	0.0625"		
	<b>Outer</b>	0"		
<b>Length L<sub>sf</sub></b>		2"		
<b>Nominal Thickness t<sub>sf</sub></b>		2.5"		
Weight and Capacity				
		<b>Weight (lb)<sup>1</sup></b>	<b>Capacity (US gal)<sup>1</sup></b>	
<b>New</b>		5,024.85	310.28	
<b>Corroded</b>		4,893.95	312.14	
Insulation				
		<b>Thickness (in)</b>	<b>Density (lb/ft<sup>3</sup>)</b>	<b>Weight (lb)</b>
<b>Insulation</b>		2	12	115.1
		<b>Spacing(In)</b>	<b>Individual Weight (lb)</b>	<b>Total Weight (lb)</b>
<b>Insulation Supports</b>		145	100	100
Radiography				
<b>Category A joints</b>		Seamless No RT		
<b>Head to shell seam</b>		Full UW-11(a) Type 1		

<sup>1</sup> includes straight flange

Results Summary	
Governing condition	internal pressure
Minimum thickness per UG-16	0.0625" + 0.0625" = 0.125"
Design thickness due to internal pressure (t)	2.2183"
Straight Flange governs MDMT	-58.9°F

Factor K		
K = (1/6)*[2 + (D / (2*h)) <sup>2</sup> ]		
Corroded	K = (1/6)*[2 + (78.125 / (2*19.5625)) <sup>2</sup> ]	0.9979
New	K = (1/6)*[2 + (78 / (2*19.5)) <sup>2</sup> ]	1

**Design thickness for internal pressure, (Corroded at 150 °F) Appendix 1-4(c)**

$$\begin{aligned}
 t &= P \cdot D \cdot K / (2 \cdot S \cdot E - 0.2 \cdot P) + \text{Corrosion} \\
 &= 1,100 \cdot 78.125 \cdot 0.997872 / (2 \cdot 20,000 \cdot 1 - 0.2 \cdot 1,100) + 0.0625 \\
 &= \underline{2.2182"}
 \end{aligned}$$

**% Extreme fiber elongation - UCS-79(d)**

$$\begin{aligned}
 \text{EFE} &= (75 \cdot t / R_f) \cdot (1 - R_f / R_o) \\
 &= (75 \cdot 2.5 / 14.51) \cdot (1 - 14.51 / \infty) \\
 &= 12.9221\%
 \end{aligned}$$

**Straight Flange on TOP HEAD**

<b>ASME Section VIII Division 1, 2015 Edition</b>				
<b>Component</b>		Cylinder		
<b>Material</b>		SA-516 70 (II-D p. 18, In. 37)		
<b>Impact Tested</b>	<b>Normalized</b>	<b>Fine Grain Practice</b>	<b>PWHT</b>	<b>Optimize MDMT/ Find MAWP</b>
Yes (-50°F)	Yes	No	Yes	No
		<b>Design Pressure (psi)</b>	<b>Design Temperature (°F)</b>	<b>Design MDMT (°F)</b>
<b>Internal</b>		1,100	150	-50
<b>Static Liquid Head</b>				
<b>Condition</b>		<b>P<sub>s</sub> (psi)</b>	<b>H<sub>s</sub> (in)</b>	<b>SG</b>
Test horizontal		3.05	84.5	1
Test vertical		1.23	34	1
<b>Dimensions</b>				
<b>Inner Diameter</b>		78"		
<b>Length</b>		2"		
<b>Nominal Thickness</b>		2.5"		
<b>Corrosion</b>	<b>Inner</b>	0.0625"		
	<b>Outer</b>	0"		
<b>Weight and Capacity</b>				
		<b>Weight (lb)</b>		<b>Capacity (US gal)</b>
<b>New</b>		357.85		41.37
<b>Corroded</b>		349.18		41.5
<b>Insulation</b>				
		<b>Thickness (in)</b>	<b>Density (lb/ft<sup>3</sup>)</b>	<b>Weight (lb)</b>
<b>Insulation</b>		2	12	0
		<b>Spacing(in)</b>	<b>Individual Weight (lb)</b>	<b>Total Weight (lb)</b>
<b>Insulation Supports</b>		0	0	0
<b>Radiography</b>				
<b>Longitudinal seam</b>		Seamless No RT		
<b>Bottom Circumferential seam</b>		Full UW-11(a) Type 1		

Results Summary	
Governing condition	Internal pressure
Minimum thickness per UG-16	0.0625" + 0.0625" = 0.125"
Design thickness due to internal pressure (t)	<u>2.2843"</u>
Design thickness due to combined loadings + corrosion	<u>0.9493"</u>
Rated MDMT	-58.9 °F

UCS-66 Material Toughness Requirements	
Material impact test temperature per UG-84 =	-50°F
$t_r = 1,100 \cdot 39.0625 / (20,000 \cdot 1 - 0.6 \cdot 1,100) =$	2.2218"
Stress ratio = $t_r \cdot E^* / (t_n - c) = 2.2218 \cdot 1 / (2.5 - 0.0625) =$	0.9115
UCS-66(i) reduction in MDMT, $T_R$ from Fig UCS-66.1 =	8.9°F
MDMT = $\max[T_{\text{impact}} - T_R, -155] = \max[-50 - 8.9, -155] =$	-58.9°F
Design MDMT of -50°F is acceptable.	

**Design thickness, (at 150 °F) UG-27(c)(1)**

$$\begin{aligned}
 t &= P \cdot R / (S \cdot E - 0.60 \cdot P) + \text{Corrosion} \\
 &= 1,100 \cdot 39.0625 / (20,000 \cdot 1.00 - 0.60 \cdot 1,100) + 0.0625 \\
 &= \underline{2.2843"}
 \end{aligned}$$

**% Extreme fiber elongation - UCS-79(d)**

$$\begin{aligned}
 \text{EFE} &= (50 \cdot t / R_f) \cdot (1 - R_f / R_o) \\
 &= (50 \cdot 2.5 / 40.25) \cdot (1 - 40.25 / \infty) \\
 &= 3.1056\%
 \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

**Thickness Required Due to Pressure + External Loads**

Condition	Pressure P (psi)	Allowable Stress Before UG-23 Stress Increase (psi)		Temperature (°F)	Corrosion C (in)	Load	Req'd Thk Due to Tension (in)	Req'd Thk Due to Compression (in)
		S <sub>t</sub>	S <sub>c</sub>					
Operating, Hot & Corroded	1,100	20,000	17,295	150	0.0625	Wind	0.8866	0.8862
						Seismic	0.8868	0.8859
Operating, Hot & New	1,100	20,000	17,301	150	0	Wind	0.8851	0.8847
						Seismic	0.8854	0.8844
Hot Shut Down, Corroded	0	20,000	17,295	150	0.0625	Wind	0.0006	0.001
						Seismic	0.0002	0.0014
Hot Shut Down, New	0	20,000	17,301	150	0	Wind	0.0006	0.0011
						Seismic	0.0002	0.0014
Empty, Corroded	0	20,000	17,295	70	0.0625	Wind	0.0006	0.001
						Seismic	0.0003	0.0013
Empty, New	0	20,000	17,301	70	0	Wind	0.0006	0.0011
						Seismic	0.0003	0.0014
Hot Shut Down, Corroded, Weight & Eccentric Moments Only	0	20,000	17,295	150	0.0625	Weight	0.0012	0.0012

SHELL RG

ASME Section VIII Division 1, 2015 Edition				
Component		Cylinder		
Material		SA-516 70 (II-D p. 18, In. 37)		
Impact Tested	Normalized	Fine Grain Practice	PWHT	Optimize MDMT/ Find MAWP
Yes (-50°F)	Yes	No	Yes	No
		Design Pressure (psi)	Design Temperature (°F)	Design MDMT (°F)
Internal		1,100	150	-50
Static Liquid Head				
Condition	P <sub>s</sub> (psi)	H <sub>s</sub> (in)	SG	
Operating	2.82	78	1	
Test horizontal	3.05	84.5	1	
Test vertical	6.43	178	1	
Dimensions				
Inner Diameter		78"		
Length		144"		
Nominal Thickness		2.5"		
Corrosion	Inner	0.0625"		
	Outer	0"		
Weight and Capacity				
		Weight (lb)	Capacity (US gal)	
New		25,338.07	2,978.72	
Corroded		24,724.12	2,988.27	
Insulation				
		Thickness (in)	Density (lb/ft <sup>3</sup> )	Weight (lb)
Insulation		2	12	534.07
		Spacing(in)	Individual Weight (lb)	Total Weight (lb)
Insulation Supports		145	100	100
Radiography				
Longitudinal seam		Full UW-11(a) Type 1		
Top Circumferential seam		Full UW-11(a) Type 1		
		Full UW-11(a) Type 1		

**Bottom Circumferential  
seam**

**Results Summary**

Governing condition	Internal pressure
Minimum thickness per UG-16	0.0625" + 0.0625" = 0.125"
Design thickness due to internal pressure (t)	<u>2.2902"</u>
Design thickness due to combined loadings + corrosion	<u>0.9554"</u>
Rated MDMT	-58.6 °F

**UCS-66 Material Toughness Requirements**

Material impact test temperature per UG-84 =	-50 °F
$t_r = 1,102.82 * 39.0625 / (20,000 * 1 - 0.6 * 1,102.82) =$	2.2276"
Stress ratio = $t_r * E' / (t_n - c) = 2.2276 * 1 / (2.5 - 0.0625) =$	0.9139
UCS-66(i) reduction in MDMT, $T_R$ from Fig UCS-66.1 =	8.6 °F
MDMT = $\max[T_{\text{impact}} - T_R, -155] = \max[-50 - 8.6, -155] =$	-58.6 °F
Design MDMT of -50 °F is acceptable.	

**Design thickness, (at 150 °F) UG-27(c)(1)**

$$\begin{aligned}
 t &= P * R / (S * E - 0.60 * P) + \text{Corrosion} \\
 &= 1,102.82 * 39.0625 / (20,000 * 1.00 - 0.60 * 1,102.82) + 0.0625 \\
 &= \underline{2.2902"}
 \end{aligned}$$

**% Extreme fiber elongation - UCS-79(d)**

$$\begin{aligned}
 \text{EFE} &= (50 * t / R_t) * (1 - R_t / R_o) \\
 &= (50 * 2.5 / 40.25) * (1 - 40.25 / \infty) \\
 &= 3.1056\%
 \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

**Thickness Required Due to Pressure + External Loads**

Condition	Pressure P (psi)	Allowable Stress Before UG-23 Stress Increase (psi)		Temperature (°F)	Corrosion C (In)	Load	Req'd Thk Due to Tension (In)	Req'd Thk Due to Compression (In)
		S <sub>t</sub>	S <sub>c</sub>					
Operating, Hot & Corroded	1,100	20,000	17,295	150	0.0625	Wind	0.8861	0.8793
						Seismic	0.8929	0.8725
Operating, Hot & New	1,100	20,000	17,301	150	0	Wind	0.8846	0.8777
						Seismic	0.8916	0.8707
Hot Shut Down, Corroded	0	20,000	17,295	150	0.0625	Wind	0.0011	0.009
						Seismic	0.0059	0.0169
Hot Shut Down, New	0	20,000	17,301	150	0	Wind	0.0011	0.0092
						Seismic	0.006	0.0172
Empty, Corroded	0	20,000	17,295	70	0.0625	Wind	0.0011	0.009
						Seismic	0.0044	0.0152
Empty, New	0	20,000	17,301	70	0	Wind	0.0011	0.0092
						Seismic	0.0045	0.0155
Hot Shut Down, Corroded, Weight & Eccentric Moments Only	0	20,000	17,295	150	0.0625	Weight	0.0063	0.0088

**Straight Flange on BOTTOM HEAD**

ASME Section VIII Division 1, 2015 Edition				
<b>Component</b>		Cylinder		
<b>Material</b>		SA-516 70 (II-D p. 18, In. 37)		
<b>Impact Tested</b>	<b>Normalized</b>	<b>Fine Grain Practice</b>	<b>PWHT</b>	<b>Optimize MDMT/ Find MAWP</b>
Yes (-50°F)	Yes	No	Yes	No
		<b>Design Pressure (psi)</b>	<b>Design Temperature (°F)</b>	<b>Design MDMT (°F)</b>
<b>Internal</b>		1,100	150	-50
Static Liquid Head				
<b>Condition</b>	<b>P<sub>s</sub> (psi)</b>	<b>H<sub>s</sub> (in)</b>	<b>SG</b>	
<b>Operating</b>	2.89	80	1	
<b>Test horizontal</b>	3.05	84.5	1	
<b>Test vertical</b>	6.5	180	1	
Dimensions				
<b>Inner Diameter</b>		78"		
<b>Length</b>		2"		
<b>Nominal Thickness</b>		2.5"		
<b>Corrosion</b>	<b>Inner</b>	0.0625"		
	<b>Outer</b>	0"		
Weight and Capacity				
		<b>Weight (lb)</b>	<b>Capacity (US gal)</b>	
<b>New</b>		357.85	41.37	
<b>Corroded</b>		349.18	41.5	
Insulation				
		<b>Thickness (in)</b>	<b>Density (lb/ft<sup>3</sup>)</b>	<b>Weight (lb)</b>
<b>Insulation</b>		2	12	0
		<b>Spacing(in)</b>	<b>Individual Weight (lb)</b>	<b>Total Weight (lb)</b>
<b>Insulation Supports</b>		0	0	0
Radiography				
<b>Longitudinal seam</b>		Seamless No RT		
<b>Top Circumferential seam</b>		Full UW-11(a) Type 1		

Results Summary	
Governing condition	Internal pressure
Minimum thickness per UG-16	$0.0625" + 0.0625" = 0.125"$
Design thickness due to internal pressure (t)	<u>2.2903"</u>
Design thickness due to combined loadings + corrosion	<u>0.9556"</u>
Rated MDMT	-58.6 °F

UCS-66 Material Toughness Requirements	
Material impact test temperature per UG-84 =	-50 °F
$t_r = 1,102.89 * 39.0625 / (20,000 * 1 - 0.6 * 1,102.89) =$	2.2278"
Stress ratio = $t_r * E' / (t_n - c) = 2.2278 * 1 / (2.5 - 0.0625) =$	0.914
UCS-66(i) reduction in MDMT, $T_R$ from Fig UCS-66.1 =	8.6 °F
MDMT = $\max[T_{\text{impact}} - T_R, -155] = \max[-50 - 8.6, -155] =$	-58.6 °F
Design MDMT of -50 °F is acceptable.	

**Design thickness, (at 150 °F) UG-27(c)(1)**

$$\begin{aligned}
 t &= P * R / (S * E - 0.60 * P) + \text{Corrosion} \\
 &= 1,102.89 * 39.0625 / (20,000 * 1.00 - 0.60 * 1,102.89) + 0.0625 \\
 &= \underline{2.2903"}
 \end{aligned}$$

**% Extreme fiber elongation - UCS-79(d)**

$$\begin{aligned}
 \text{EFE} &= (50 * t / R_t) * (1 - R_t / R_o) \\
 &= (50 * 2.5 / 40.25) * (1 - 40.25 / \infty) \\
 &= 3.1056\%
 \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

**Thickness Required Due to Pressure + External Loads**

Condition	Pressure P (psi)	Allowable Stress Before UG-23 Stress Increase (psi)		Temperature (°F)	Corrosion C (In)	Load	Req'd Thk Due to Tension (In)	Req'd Thk Due to Compression (In)
		S <sub>t</sub>	S <sub>c</sub>					
Operating, Hot & Corroded	1,100	20,000	17,295	150	0.0625	Wind	0.8861	0.8792
						Seismic	0.8931	0.8722
Operating, Hot & New	1,100	20,000	17,301	150	0	Wind	0.8846	0.8776
						Seismic	0.8918	0.8705
Hot Shut Down, Corroded	0	20,000	17,295	150	0.0625	Wind	0.0011	0.0091
						Seismic	0.006	0.0171
Hot Shut Down, New	0	20,000	17,301	150	0	Wind	0.0011	0.0093
						Seismic	0.0061	0.0175
Empty, Corroded	0	20,000	17,295	70	0.0625	Wind	0.0011	0.0091
						Seismic	0.0045	0.0154
Empty, New	0	20,000	17,301	70	0	Wind	0.0011	0.0093
						Seismic	0.0046	0.0157
Hot Shut Down, Corroded, Weight & Eccentric Moments Only	0	20,000	17,295	150	0.0625	Weight	0.0064	0.0089

**BOTTOM HEAD**

ASME Section VIII Division 1, 2015 Edition				
<b>Component</b>		Ellipsoidal Head		
<b>Material</b>		SA-516 70 (II-D p. 18, ln. 37)		
<b>Attached To</b>		SHELL RG		
<b>Impact Tested</b>	<b>Normalized</b>	<b>Fine Grain Practice</b>	<b>PWHT</b>	<b>Optimize MDMT/ Find MAWP</b>
Yes (-50°F)	Yes	No	Yes	No
		<b>Design Pressure (psi)</b>	<b>Design Temperature (°F)</b>	<b>Design MDMT (°F)</b>
<b>Internal</b>		1,100	150	-50
Static Liquid Head				
<b>Condition</b>	<b>P<sub>s</sub> (psi)</b>	<b>H<sub>s</sub> (in)</b>	<b>SG</b>	
<b>Operating</b>	3.59	99.5625	1	
<b>Test horizontal</b>	3.05	84.5	1	
<b>Test vertical</b>	7.2	199.5	1	
Dimensions				
<b>Inner Diameter</b>		78"		
<b>Head Ratio</b>		2		
<b>Minimum Thickness</b>		2.2262"		
<b>Corrosion</b>	<b>Inner</b>	0.0625"		
	<b>Outer</b>	0"		
<b>Length L<sub>sf</sub></b>		2"		
<b>Nominal Thickness t<sub>sf</sub></b>		2.5"		
Weight and Capacity				
		<b>Weight (lb)<sup>1</sup></b>	<b>Capacity (US gal)<sup>1</sup></b>	
<b>New</b>		5,095.4	310.28	
<b>Corroded</b>		4,962.51	312.14	
Insulation				
		<b>Thickness (in)</b>	<b>Density (lb/ft<sup>3</sup>)</b>	<b>Weight (lb)</b>
<b>Insulation</b>		2	12	115.1
		<b>Spacing(in)</b>	<b>Individual Weight (lb)</b>	<b>Total Weight (lb)</b>
<b>Insulation Supports</b>		145	100	100
Radiography				
<b>Category A joints</b>		Seamless No RT		

<b>Head to shell seam</b>	Full UW-11(a) Type 1
---------------------------	----------------------

<sup>1</sup> Includes straight flange

Results Summary	
Governing condition	internal pressure
Minimum thickness per UG-16	0.0625" + 0.0625" = 0.125"
Design thickness due to internal pressure (t)	<u>2.2254"</u>
<u>Straight Flange</u> governs MDMT	-58.6°F

Factor K		
K = (1/6)*[2 + (D / (2*h)) <sup>2</sup> ]		
Corroded	K = (1/6)*[2 + (78.125 / (2*19.5625)) <sup>2</sup> ]	0.9979
New	K = (1/6)*[2 + (78 / (2*19.5)) <sup>2</sup> ]	1

**Design thickness for internal pressure, (Corroded at 150 °F) Appendix 1-4(c)**

$$\begin{aligned}
 t &= P \cdot D \cdot K / (2 \cdot S \cdot E - 0.2 \cdot P) + \text{Corrosion} \\
 &= 1,103.59 \cdot 78.125 \cdot 0.997872 / (2 \cdot 20,000 \cdot 1 - 0.2 \cdot 1,103.59) + 0.0625 \\
 &= \underline{2.2253"}
 \end{aligned}$$

**% Extreme fiber elongation - UCS-79(d)**

$$\begin{aligned}
 EFE &= (75 \cdot t / R_t) \cdot (1 - R_t / R_o) \\
 &= (75 \cdot 2.5 / 14.51) \cdot (1 - 14.51 / \infty) \\
 &= 12.9221\%
 \end{aligned}$$

**SKIRT**

<b>ASME Section VIII Division 1, 2015 Edition</b>		
<b>Component</b>	Support Skirt	
<b>Material</b>	SA-516 70 (II-D p. 18, ln. 37)	
<b>Skirt is Attached To</b>	BOTTOM HEAD	
<b>Skirt Attachment Offset</b>	3.5314" down from the top seam	
<b>Design Temperature</b>		
<b>Internal</b>	650°F	
<b>Dimensions</b>		
<b>Inner Diameter</b>	<b>Top</b>	82.25"
	<b>Bottom</b>	82.25"
<b>Length (includes base ring thickness)</b>		32.47"
<b>Nominal Thickness</b>		0.375"
<b>Corrosion</b>	<b>Inner</b>	0"
	<b>Outer</b>	0"
<b>Weight</b>		
<b>New</b>		870.36 lb
<b>Corroded</b>		870.36 lb
<b>Joint Efficiency</b>		
<b>Top</b>		0.55
<b>Bottom</b>		0.8

Skirt design thickness, largest of the following + corrosion = 0.0588 in

The governing condition is due to seismic, compressive stress at the base, operating & new.

The skirt thickness of 0.375 in is adequate.

Results Summary							
Loading	Condition	Tensile or Compressive Side	Governing Skirt Location	Temperature (°F)	Allowable Stress (psi)	Calculated Stress/E (psi)	Required thickness (in)
Wind	operating, corroded	Tensile	top	650	8,676.92	-190.27	0.0082
		Compressive	bottom			753.35	0.0326
	operating, new	Tensile	top	650	8,676.92	-194.83	0.0084
		Compressive	bottom			762.86	0.033
	empty, corroded	Tensile	top	70	12,736.46	-90.64	0.0027
		Compressive	bottom			587.3	0.0173
	empty, new	Tensile	top	70	12,736.46	-95.56	0.0028
		Compressive	bottom			597.42	0.0176
	test, new	Tensile	top	70	12,736.46	-323.45	0.0095
		Compressive	bottom			846.56	0.0249
Seismic	operating, corroded	Tensile	bottom	650	18,800	534.81	0.0107
		Compressive			8,676.92	1,338.57	0.0579
	operating, new	Tensile	bottom	650	18,800	544.7	<u>0.0109</u>
		Compressive			8,676.92	1,360.55	<u>0.0588</u>
	empty, corroded	Tensile	bottom	70	20,000	458.56	0.0086
		Compressive			12,736.46	1,011.89	0.0298
	empty, new	Tensile	bottom	70	20,000	468.48	0.0088
		Compressive			12,736.46	1,034.88	0.0305

## Loading due to seismic, operating & new

### Tensile side

Required thickness, tensile stress at base:

$$\begin{aligned}
 t &= -(0.6 - 0.14 \cdot S_{DS}) \cdot W / (\pi \cdot D \cdot S_t \cdot E) + 48 \cdot M / (\pi \cdot D^2 \cdot S_t \cdot E) \\
 &= -(0.6 - 0.14 \cdot 0.7333) \cdot 56,262.03 / (\pi \cdot 82.625 \cdot 18,800 \cdot 0.8) + 48 \cdot 121,180.1 / (\pi \cdot 82.625^2 \cdot 18,800 \cdot 0.8) \\
 &= 0.0109 \text{ in}
 \end{aligned}$$

Required thickness, tensile stress at the top:

$$\begin{aligned}
 t &= -(0.6 - 0.14 \cdot S_{DS}) \cdot W_t / (\pi \cdot D_t \cdot S_t \cdot E) + 48 \cdot M_t / (\pi \cdot D_t^2 \cdot S_t \cdot E) \\
 &= -(0.6 - 0.14 \cdot 0.7333) \cdot 55,391.67 / (\pi \cdot 82.625 \cdot 18,800 \cdot 0.55) + 48 \cdot 91,649 / (\pi \cdot 82.625^2 \cdot 18,800 \cdot 0.55) \\
 &= 0.0096 \text{ in}
 \end{aligned}$$

### Compressive side

Required thickness, compressive stress at base:

$$\begin{aligned}
 t &= (1 + 0.14 \cdot S_{DS}) \cdot W / (\pi \cdot D \cdot S_c \cdot E_c) + 48 \cdot M / (\pi \cdot D^2 \cdot S_c \cdot E_c) \\
 &= (1 + 0.14 \cdot 0.7333) \cdot 56,262.03 / (\pi \cdot 82.625 \cdot 8,677 \cdot 1) + 48 \cdot 121,180.1 / (\pi \cdot 82.625^2 \cdot 8,677 \cdot 1) \\
 &= 0.0588 \text{ in}
 \end{aligned}$$

**Required thickness, compressive stress at the top:**

$$\begin{aligned} t &= (1 + 0.14*S_{DS})*W_t / (\pi*D_t*S_c*E_c) + 48*M_t / (\pi*D_t^2*S_c*E_c) \\ &= (1 + 0.14*0.7333)*55,391.67 / (\pi*82.625*8,677*1) + 48*91,649 / (\pi*82.625^2*8,677*1) \\ &= 0.0508 \text{ in} \end{aligned}$$

## BASE RING

Inputs	
Base configuration	single base plate without gussets
Base plate material	SA-516-70
Base plate allowable stress, $S_p$	20,000 psi
Foundation compressive strength	1,658 psi
Concrete ultimate 28-day strength	3,000 psi
Bolt circle, BC	88"
Base plate inner diameter, $D_i$	78"
Base plate outer diameter, $D_o$	93"
Base plate thickness, $t_b$	0.875"
Anchor Bolts	
Material	
Allowable stress, $S_b$	20,000 psi
Bolt size and type	1" series 8 threaded
Number of bolts, N	8
Corrosion allowance (applied to root radius)	0"
Anchor bolt clearance	0.375"
Bolt root area (corroded), $A_b$	0.55 in <sup>2</sup>
Diameter of anchor bolt holes, $d_b$	1.375"
Initial bolt preload	0% (0 psi)
Bolt at 0°	No

Results Summary							
Load	Vessel condition	Base V (lb)	Base M (lb-ft)	W (lb)	Required bolt area (in <sup>2</sup> )	t <sub>r</sub> Base (in)	Foundation bearing stress (psi)
Wind	operating, corroded	2,568.9	30,855	55,914.8	0	0.3735	37.2
Wind	operating, new	2,568.9	30,974.9	56,770.6	0	0.3758	37.66
Wind	empty, corroded	2,568.9	30,855	39,751.3	0	0.3305	29.13
Wind	empty, new	2,568.9	30,974.9	40,667.1	0	0.3333	29.62
Wind	test, new	1,390.9	20,925.7	70,756.7	0	0.3951	41.63
Seismic	operating, corroded	10,763.6	119,122	55,914.8	0.2323	0.7263	140.65
Seismic	operating, new	10,928.3	121,180.1	56,770.6	<u>0.2367</u>	<u>0.7325</u>	<u>143.08</u>
Seismic	empty, corroded	7,652.1	95,062.9	39,751.3	0.2005	0.6477	111.86
Seismic	empty, new	7,828.4	97,176.7	40,667.1	0.2049	0.6548	114.35

### Anchor bolt load (governing)

$$\begin{aligned}
 P &= -(0.6 - 0.14 \cdot S_{DS}) \cdot W / N + 48 \cdot M / (N \cdot BC) \\
 &= -(0.6 - 0.14 \cdot 0.7333) \cdot 56,770.58 / 8 + 48 \cdot 121,180.1 / (8 \cdot 88) \\
 &= 4,733.04 \text{ lb}_f
 \end{aligned}$$

$$\text{Required area per bolt} = P / S_b = \underline{0.2367} \text{ in}^2$$

The area provided (0.551 in<sup>2</sup>) by the specified anchor bolt is adequate.

### Support calculations (Jawad & Farr chapter 12, governing)

Base plate width, t<sub>c</sub>: 7.5 in  
 Average base plate diameter, d: 85.5 in  
 Base plate elastic modulus, E<sub>s</sub>: 29.0E+06 psi  
 Base plate yield stress, S<sub>y</sub>: 38,000 psi

$$E_c = 57,000 \cdot \text{Sqr}(3,000) = 3,122,019 \text{ psi}$$

$$n = E_s / E_c = 29.0E+06 / 3,122,019 = 9.2889$$

$$\begin{aligned}
 t_s &= (N \cdot A_b) / (\pi \cdot d) \\
 &= (8 \cdot 0.551) / (\pi \cdot 85.5) \\
 &= 0.0164 \text{ in}
 \end{aligned}$$

From table 12.4 for k = 0.283685:

$$\begin{aligned}
 K_1 &= 2.4774, & K_2 &= 1.4651 \\
 L_1 &= 18.4882, & L_2 &= 47.4955, & L_3 &= 19.231
 \end{aligned}$$

### Total tensile force on bolting

$$\begin{aligned}
 T &= (12 \cdot M - (0.6 - 0.14 \cdot S_{DS}) \cdot W \cdot (L_1 + L_3)) / (L_2 + L_3) \\
 &= (12 \cdot 121,180.1 - (0.6 - 0.14 \cdot 0.7333) \cdot 56,770.58 \cdot (18.4882 + 19.231)) / (47.4955 + 19.231) \\
 &= 5,832.81 \text{ lb}_f
 \end{aligned}$$

Tensile stress in bolts use the larger of  $f_s$  or bolt preload = 0 psi

$$\begin{aligned}f_s &= T / (t_s * (d / 2) * K_1) \\&= 5,832.81 / (0.0164 * (85.5 / 2) * 2.4774) \\&= 3,356 \text{ psi}\end{aligned}$$

#### Total compressive load on foundation

$$\begin{aligned}C_c &= T + (1 + 0.14 * S_{DS}) * W + \text{Bolt Preload} \\&= 5,832.81 + (1 + 0.14 * 0.7333) * 56,770.58 + 0 \\&= 68,431.84 \text{ lb}_f\end{aligned}$$

#### Foundation bearing stress

$$\begin{aligned}f_c &= C_c / (((t_c - t_s) + n * t_s) * (d / 2) * K_2) \\&= 68,431.84 / (((7.5 - 0.0164) + 9.2889 * 0.0164) * (85.5 / 2) * 1.4651) \\&= \underline{143} \text{ psi}\end{aligned}$$

As  $f_c \leq 1,658$  psi the base plate width is satisfactory.

$$\begin{aligned}k &= 1 / (1 + f_s / (n * f_c)) \\&= 1 / (1 + 3,356 / (9.2889 * 143)) \\&= 0.283685\end{aligned}$$

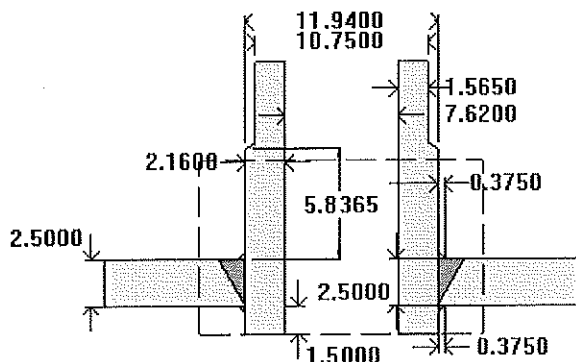
#### Base plate required thickness (governing)

$$\begin{aligned}t_r &= (3 * f_c * L^2 / S_p)^{0.5} \\&= (3 * 143 * 5^2 / 20,000)^{0.5} \\&= \underline{0.7325} \text{ in}\end{aligned}$$

The base plate thickness is satisfactory.

### INLET W/DIVERTER (A)

ASME Section VIII Division 1, 2015 Edition



Note: round inside edges per UG-76(c)

#### Location and Orientation

Located on	SHELL RG
Orientation	270°
Nozzle center line offset to datum line	66"
End of nozzle to shell center	51.5"
Passes through a Category A joint	No

#### Nozzle

Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, In. 28)
Inside diameter, new	7.62"
Wall thickness, $t_n$	2.16"
Minimum wall thickness	1.565"
Corrosion allowance	0.0625"
Projection available outside vessel, $L_{pr}$	7.56"
Heavy barrel length, $L_{hb}$	5.8365"
Internal projection, $h_{new}$	1.5"
Projection available outside vessel to flange face, $L_f$	10"
Local vessel minimum thickness	2.5"
Liquid static head included	0.14 psi
Longitudinal joint efficiency	1

#### Welds

Inner fillet, $Leg_{41}$	0.375"
--------------------------	--------

Lower fillet, Leg <sub>43</sub>	0.375"
Nozzle to vessel groove weld	2.5"

ASME B16.5-2013 Flange	
Description	NPS 8 Class 600 FVC HB A350 LF2 Cl.1 (Nut Relief)
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 344, ln. 31)
Blind Included	No
Rated MDMT	-55°F
Liquid static head	0 psi
MAWP rating	1,420 psi @ 150°F
MAP rating	1,480 psi @ 70°F
Hydrotest rating	2,225 psi @ 70°F
PWHT performed	Yes
Impact Tested	No
Notes	
Flange is impact tested per material specification to -50°F. UCS-66(i) reduction of 25.7°F applied (ratio = 0.7432). Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection	
Impact test temperature per material specification =	-50°F
$t_r = 1,100.14 * 3.8725 / (20,000 * 1 - 0.6 * 1,100.14) =$	0.2203"
Stress ratio = $t_r * E' / (t_n - c) = 0.2203 * 1 / (2.16 - 0.0625) =$	0.105
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,100.14 * 3.8725 / (20,000 * 1 - 0.6 * 1,100.14) =$	0.2203"
Stress ratio = $t_r * E' / (t_n - c) = 0.2203 * 1 / (1.565 - 0.0625) =$	0.1466
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

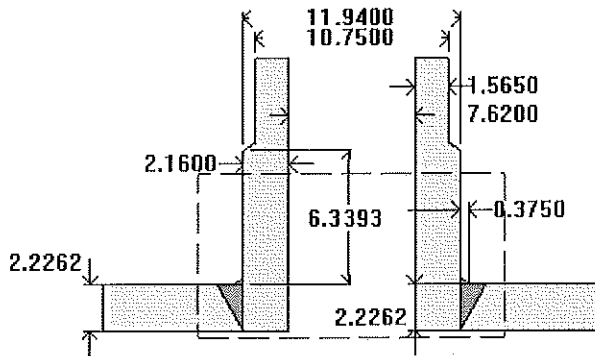
<b>UG-37 Area Calculation Summary (in<sup>2</sup>)</b>							<b>UG-45 Summary (in)</b>	
For P = 1,100.14 psi @ 150 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
17.2097	27.7141	1.9542	19.6871	5.8506	--	0.2222	0.3819	1.565

<b>UG-41 Weld Failure Path Analysis Summary</b>
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

<b>UW-16 Weld Sizing Summary</b>			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

VAPOR OUTLET (B)

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Note: Per UW-16(b) minimum inside corner radius  $r_1 = \min [1 / 4 * t, 0.125 \text{ in}] = 0.125 \text{ in}$

Location and Orientation

Located on	TOP HEAD
Orientation	0°
End of nozzle to datum line	166"
Calculated as hillside	No
Distance to head center, R	0"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, In. 28)
Inside diameter, new	7.62"
Wall thickness, $t_n$	2.16"
Minimum wall thickness	1.565"
Corrosion allowance	0.0625"
Projection available outside vessel, $L_{pr}$	8.0628"
Heavy barrel length, $L_{hb}$	6.3393"
Projection available outside vessel to flange face, $L_f$	10.5028"
Local vessel minimum thickness	2.2262"
Liquid static head included	0 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, $Leg_{41}$	0.375"
--------------------------	--------

Nozzle to vessel groove weld	2.2262"
------------------------------	---------

ASME B16.5-2013 Flange	
Description	NPS 8 Class 600 FVC HB A350 LF2 Cl.1 (Nut Relief)
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 344, ln. 31)
Blind included	No
Rated MDMT	-55°F
Liquid static head	0 psi
MAWP rating	1,420 psi @ 150°F
MAP rating	1,480 psi @ 70°F
Hydrotest rating	2,225 psi @ 70°F
PWHT performed	Yes
Impact Tested	No
Notes	
Flange is impact tested per material specification to -50°F. UCS-66(l) reduction of 25.7°F applied (ratio = 0.7432). Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection	
Impact test temperature per material specification =	-50°F
$t_r = 1,100 * 3.8725 / (20,000 * 1 - 0.6 * 1,100) =$	0.2203"
Stress ratio = $t_r * E^* / (t_n - c) = 0.2203 * 1 / (2.16 - 0.0625) =$	0.105
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,100 * 3.8725 / (20,000 * 1 - 0.6 * 1,100) =$	0.2203"
Stress ratio = $t_r * E^* / (t_n - c) = 0.2203 * 1 / (1.565 - 0.0625) =$	0.1466
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

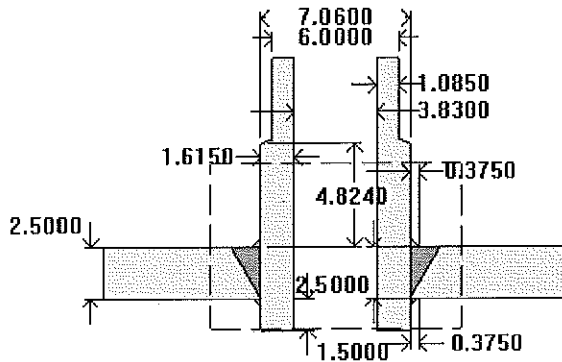
<b>UG-37 Area Calculation Summary (in<sup>2</sup>)</b>							<b>UG-45 Summary (in)</b>	
For P = 1,100 psi @ 150 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
15.0351	21.7234	1.8957	19.6871	--	--	0.1406	0.3819	1.565

<b>UG-41 Weld Failure Path Analysis Summary</b>
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

<b>UW-16 Weld Sizing Summary</b>			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

LIQUID OUTLET (C)

ASME Section VIII Division 1, 2015 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	180°
Nozzle center line offset to datum line	-6"
End of nozzle to shell center	49.5"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, In. 28)
Inside diameter, new	3.83"
Wall thickness, $t_n$	1.615"
Minimum wall thickness	1.085"
Corrosion allowance	0.0625"
Projection available outside vessel, $L_{pr}$	6.25"
Heavy barrel length, $L_{hb}$	4.824"
Internal projection, $h_{new}$	1.5"
Projection available outside vessel to flange face, $L_f$	8"
Local vessel minimum thickness	2.5"
Liquid static head included	2.67 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, $Leg_{41}$	0.375"
--------------------------	--------

Lower fillet, Leg <sub>43</sub>	0.375"
Nozzle to vessel groove weld	2.5"

ASME B16.5-2013 Flange	
Description	NPS 4 Class 600 FVC HB A350 LF2 Cl.1 (Nut Relief)
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 344, In. 31)
Blind included	No
Rated MDMT	-55°F
Liquid static head	2.6 psi
MAWP rating	1,420 psi @ 150°F
MAP rating	1,480 psi @ 70°F
Hydrotest rating	2,225 psi @ 70°F
PWHT performed	Yes
Impact Tested	No
Notes	
Flange is impact tested per material specification to -50°F. UCS-66(i) reduction of 25.5°F applied (ratio = 0.745). Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection	
Impact test temperature per material specification =	-50°F
$t_r = 1,102.67 * 1.9775 / (20,000 * 1 - 0.6 * 1,102.67) =$	0.1128"
Stress ratio = $t_r * E' / (t_n - c) = 0.1128 * 1 / (1.615 - 0.0625) =$	0.0726
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,102.67 * 1.9775 / (20,000 * 1 - 0.6 * 1,102.67) =$	0.1128"
Stress ratio = $t_r * E' / (t_n - c) = 0.1128 * 1 / (1.085 - 0.0625) =$	0.1103
Stress ratio ≤ 0.35, MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

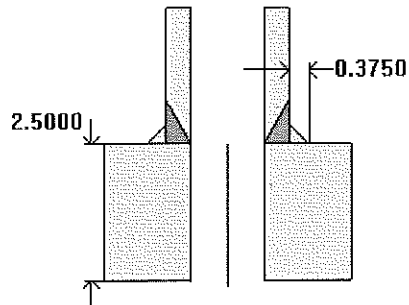
<b>UG-37 Area Calculation Summary (in<sup>2</sup>)</b>							<b>UG-45 Summary (in)</b>	
For P = 1,102.67 psi @ 150 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
8.8091	17.3589	1.6772	11.1757	4.2838	--	0.2222	0.3075	1.085

<b>UG-41 Weld Failure Path Analysis Summary</b>
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

<b>UW-16 Weld Sizing Summary</b>			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

LSHH (D1)

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Note: round inside edges per UG-76(c)

**Location and Orientation**

Located on	SHELL RG
Orientation	15°
Nozzle center line offset to datum line	55.375"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

**Nozzle**

Description	NPS 1 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.315"
Nominal wall thickness	0.4675"
Corrosion allowance	0.0625"
Projection available outside vessel, Lpr	4"
Local vessel minimum thickness	2.5"
Liquid static head included	0.41 psi
Longitudinal joint efficiency	1

**Welds**

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,100.41 * 0.72 / (20,000 * 1 - 0.6 * 1,100.41) =$	0.041"
Stress ratio = $t_r * E' / (t_n - c) = 0.041 * 1 / (0.4675 - 0.0625) =$	0.1012
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{Impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,100.41 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.4675

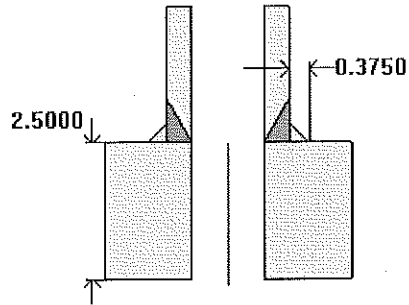
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

**This opening does not require reinforcement per UG-36(c)(3)(a)**

LSHH (D2)

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Note: round inside edges per UG-76(c)

**Location and Orientation**

Located on	SHELL RG
Orientation	15°
Nozzle center line offset to datum line	41.375"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

**Nozzle**

Description	NPS 1 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.315"
Nominal wall thickness	0.4675"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	0.91 psi
Longitudinal joint efficiency	1

**Welds**

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,100.91 * 0.72 / (20,000 * 1 - 0.6 * 1,100.91) =$	0.041"
Stress ratio = $t_r * E' / (t_n - c) = 0.041 * 1 / (0.4675 - 0.0625) =$	0.1012
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,100.91 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.4675

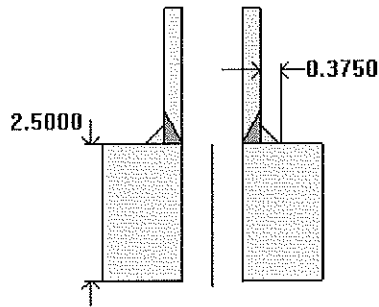
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg41)	0.25	0.2625	weld size is adequate

**This opening does not require reinforcement per UG-36(c)(3)(a)**

TI (E)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	300°
Nozzle center line offset to datum line	24"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	1.54 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,101.54 * 0.5875 / (20,000 * 1 - 0.6 * 1,101.54) =$	0.0335"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0335 * 1 / (0.35 - 0.0625) =$	0.1164
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,101.54 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

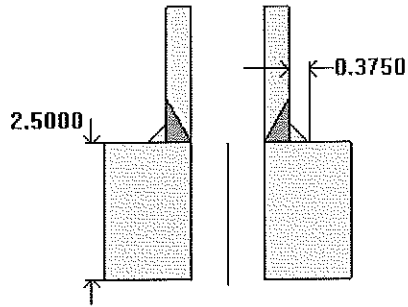
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

LT (F1)

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Note: round inside edges per UG-76(c)

**Location and Orientation**

Located on	SHELL RG
Orientation	330°
Nozzle center line offset to datum line	60"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

**Nozzle**

Description	NPS 1 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.315"
Nominal wall thickness	0.4675"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	0.24 psi
Longitudinal joint efficiency	1

**Welds**

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,100.24 \cdot 0.72 / (20,000 \cdot 1 - 0.6 \cdot 1,100.24) =$	0.041"
Stress ratio = $t_r \cdot E^* / (t_n - c) = 0.041 \cdot 1 / (0.4675 - 0.0625) =$	0.1011
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,100.24 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.4675

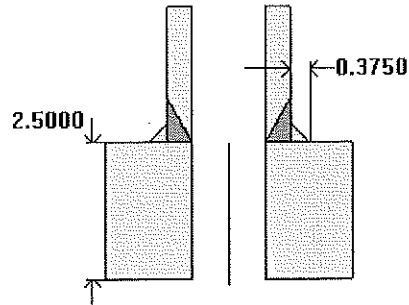
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

LT (F2)

ASME Section VIII Division 1, 2015 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	330°
Nozzle center line offset to datum line	-7"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 1 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.315"
Nominal wall thickness	0.4675"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	2.66 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,102.66 \cdot 0.72 / (20,000 \cdot 1 - 0.6 \cdot 1,102.66) =$	0.0411"
Stress ratio = $t_r \cdot E^* / (t_n - c) = 0.0411 \cdot 1 / (0.4675 - 0.0625) =$	0.1014
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,102.66 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.4675

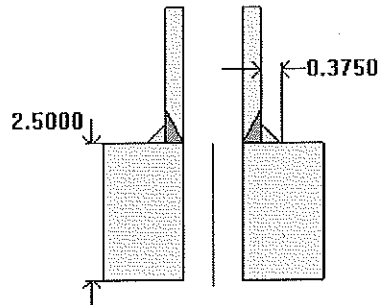
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

LG (G1)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	345°
Nozzle center line offset to datum line	59.875"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	0.24 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,100.24 * 0.5875 / (20,000 * 1 - 0.6 * 1,100.24) =$	0.0334"
Stress ratio = $t_r * E' / (t_n - c) = 0.0334 * 1 / (0.35 - 0.0625) =$	0.1163
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,100.24 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

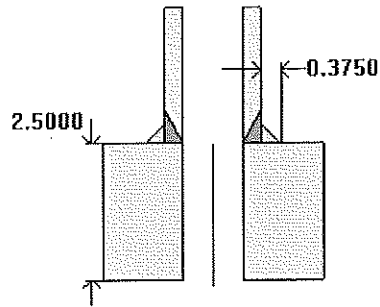
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

LG (G2)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	345°
Nozzle center line offset to datum line	21.75"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	1.62 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,101.62 * 0.5875 / (20,000 * 1 - 0.6 * 1,101.62) =$	0.0335"
Stress ratio = $t_r * E' / (t_n - c) = 0.0335 * 1 / (0.35 - 0.0625) =$	0.1164
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,101.62 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

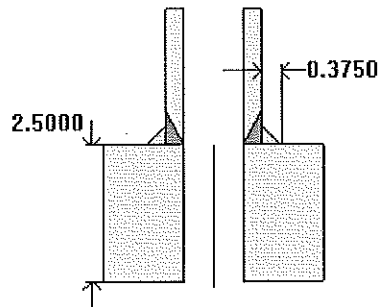
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

LG (G3)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	0°
Nozzle center line offset to datum line	31.5"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	1.26 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,101.26 * 0.5875 / (20,000 * 1 - 0.6 * 1,101.26) =$	0.0335"
Stress ratio = $t_r * E' / (t_n - c) = 0.0335 * 1 / (0.35 - 0.0625) =$	0.1164
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

**Reinforcement Calculations for Internal Pressure**

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,101.26 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

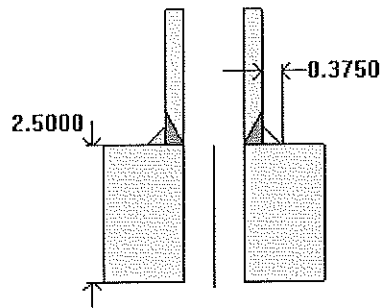
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

**This opening does not require reinforcement per UG-36(c)(3)(a)**

LG (G4)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	0°
Nozzle center line offset to datum line	-6.625"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	2.64 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,102.64 * 0.5875 / (20,000 * 1 - 0.6 * 1,102.64) =$	0.0335"
Stress ratio = $t_r * E' / (t_n - c) = 0.0335 * 1 / (0.35 - 0.0625) =$	0.1165
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,102.64 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

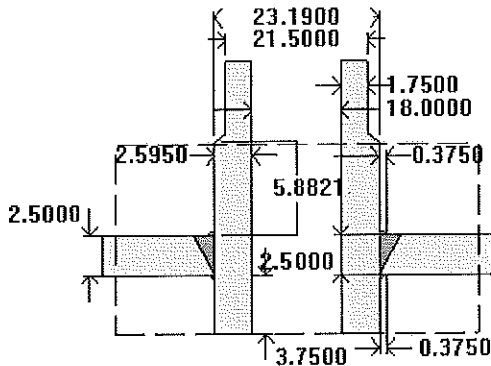
UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

MANWAY (H)

ASME Section VIII Division 1, 2015 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	270°
Nozzle center line offset to datum line	7"
End of nozzle to shell center	53.25"
Passes through a Category A joint	No

Nozzle

Access opening	Yes
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	18"
Wall thickness, $t_n$	2.595"
Minimum wall thickness	1.75"
Corrosion allowance	0.0625"
Projection available outside vessel, $L_{pr}$	8.25"
Heavy barrel length, $L_{hb}$	5.8821"
Internal projection, $h_{new}$	3.75"
Projection available outside vessel to flange face, $L_f$	11.75"
Local vessel minimum thickness	2.5"
Liquid static head included	2.45 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, $Leg_{41}$	0.375"
--------------------------	--------

Lower fillet, Leg <sub>43</sub>	0.375"
Nozzle to vessel groove weld	2.5"

ASME B16.5-2013 Flange	
Description	NPS 18 Class 600 FVC HB A350 LF2 Cl.1 (Nut Relief)
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 344, ln. 31)
Blind included	Yes
Rated MDMT	-55°F
Liquid static head	2.13 psi
MAWP rating	1,420 psi @ 150°F
MAP rating	1,480 psi @ 70°F
Hydrotest rating	2,225 psi @ 70°F
PWHT performed	Yes
Impact Tested	No
Notes	
Flange is impact tested per material specification to -50°F. UCS-66(i) reduction of 25.5°F applied (ratio = 0.7447). Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection	
Impact test temperature per material specification =	-50°F
$t_r = 1,102.45 \cdot 39.0625 / (20,000 \cdot 1 - 0.6 \cdot 1,102.45) =$	2.2269"
Stress ratio = $t_r \cdot E^* / (t_n - c) = 2.2269 \cdot 1 / (2.5 - 0.0625) =$	0.9136
UCS-66(i) reduction in MDMT, $T_R$ from Fig UCS-66.1 =	8.6°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, \max[T_{\text{impact}} - T_R, -155]] = \min[-50 - 5, \max[-50 - 8.6, -155]] =$	-58.6°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50°F
$t_r = 1,102.45 \cdot 9.0625 / (20,000 \cdot 1 - 0.6 \cdot 1,102.45) =$	0.5166"
Stress ratio = $t_r \cdot E^* / (t_n - c) = 0.5166 \cdot 1 / (1.75 - 0.0625) =$	0.3062
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155°F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155°F
Material is exempt from impact testing at the Design MDMT of -50°F.	

**Reinforcement Calculations for Internal Pressure**

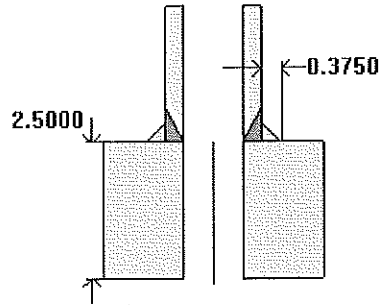
<b>UG-37 Area Calculation Summary (in<sup>2</sup>)</b>							<b>UG-45 Summary (in)</b>	
For P = 1,102.45 psi @ 150 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
40.3622	45.1661	3.8175	22.9101	18.2163	--	0.2222	0.5791	1.75

<b>UG-41 Weld Failure Path Analysis Summary</b>
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

<b>UW-16 Weld Sizing Summary</b>			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.25	0.2625	weld size is adequate

TE (J)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	SHELL RG
Orientation	315°
Nozzle center line offset to datum line	24"
End of nozzle to shell center	45.5"
Passes through a Category A joint	No

Nozzle

Description	NPS 0.75 Class 6000 - threaded
Access opening	No
Material specification	SA-350 LF2 Cl 1 (II-D p. 18, ln. 28)
Inside diameter, new	1.05"
Nominal wall thickness	0.35"
Corrosion allowance	0.0625"
Projection available outside vessel, L <sub>pr</sub>	4"
Local vessel minimum thickness	2.5"
Liquid static head included	1.54 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg <sub>41</sub>	0.375"
---------------------------------	--------

UCS-66 Material Toughness Requirements Nozzle	
Impact test temperature per material specification =	-50 °F
$t_r = 1,101.54 * 0.5875 / (20,000 * 1 - 0.6 * 1,101.54) =$	0.0335"
Stress ratio = $t_r * E' / (t_n - c) = 0.0335 * 1 / (0.35 - 0.0625) =$	0.1164
Stress ratio $\leq 0.35$ , MDMT per UCS-66(b)(3) =	-155 °F
MDMT = $\min[T_{\text{impact}} - T_{\text{UCS-66(g)}}, -155] = \min[-50 - 5, -155] =$	-155 °F
Material is exempt from impact testing at the Design MDMT of -50 °F.	

### Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in <sup>2</sup> )							UG-45 Summary (in)	
For P = 1,101.54 psi @ 150 °F							The nozzle passes UG-45	
A required	A available	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>5</sub>	A welds	t <sub>req</sub>	t <sub>min</sub>
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.125	0.35

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg <sub>41</sub> )	0.2012	0.2625	weld size is adequate

This opening does not require reinforcement per UG-36(c)(3)(a)

Liquid Level

ASME Section VIII Division 1, 2015 Edition	
Location from Datum (in)	66
Operating Liquid Specific Gravity	1

## LIFTING LUG

Geometry Inputs	
Attached To	SHELL RG
Material	SA-516-70
Distance of Lift Point From Datum	155"
Angular Position	0° and 180°
Length, L	23"
Width, B	13"
Thickness, t	1.25"
Hole Diameter, d	2"
Pin Diameter, Dp	1.625"
Diameter at Pin, D	7"
Load Angle from Vertical, $\phi$	0°
Has Brace Plate	No
<b>Welds</b>	
Size, $t_w$	0.75"
Weld Length, $L_3$	5"

Intermediate Values	
Load Factor	1.5000
Vessel Weight (new, incl. Load Factor), W	59,854.3 lb
Lug Weight (new), $W_{lug}$	248.2 lb (Qty=2)
Distance from Center of Gravity to Top Lug, $l_1$	99.3133"
Distance from Center of Gravity to Tail Lug, $l_2$	96.813"
Distance from Vessel Center Line to Tail Lug, $l_3$	44.5"
Allowable Stress, Tensile, $\sigma_t$	19,980 psi
Allowable Stress, Shear, $\sigma_s$	13,320 psi
Allowable Stress, Bearing, $\sigma_p$	29,970 psi
Allowable Stress, Bending, $\sigma_b$	22,201 psi
Allowable Stress, Weld Shear, $\tau_{allowable}$	13,320 psi
Allowable Stress set to 1/3 Sy per ASME B30.20	No

Summary Values	
Required Lift Pin Diameter, $d_{reqd}$	<u>1.196"</u>
Required Lug Thickness, $t_{reqd}$	<u>0.6145"</u>
Lug Stress Ratio, $\sigma_{ratio}$	<u>0.46</u>
Weld Shear Stress Ratio, $\tau_{ratio}$	<u>0.73</u>
Lug Design	Acceptable
Local Stresses WRC 107	Acceptable
Maximum Out of Plane Lift Angle - Weak Axis Bending	6.23°

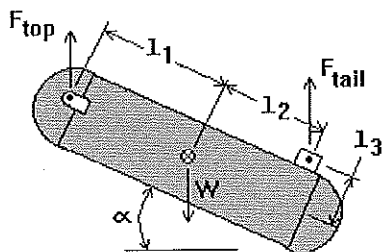
COMPRESS recommends a spreader beam be used to prevent weak axis bending of the top lugs. No consideration is given for any bracing plate from the lug to the vessel.

### Lift Forces

Lift force on lugs during rotational lift ( $0^\circ \leq \alpha \leq 90^\circ$ ):

$$2 * F_{top} = W * (l_2 * \cos(\alpha) + l_3 * \sin(\alpha)) / (l_1 * \cos(\alpha) + l_2 * \cos(\alpha) + l_3 * \sin(\alpha))$$

$$F_{tail} = W - (2 * F)$$



$\alpha$ [°]	$F_{top}$ [lbf]	$F_{tail}$ [lbf]
0	14,773	30,309
15	15,641	28,572
30	16,528	26,798
45	17,575	24,704
60	19,048	21,758
75	21,722	16,411
90	29,927	0
18 <sup>1</sup>	15,813	28,228
18 <sup>2</sup>	15,813	28,228
<sup>1</sup> Lift angle at maximum lug stress.		
<sup>2</sup> Lift angle at maximum weld stress.		
Shell angle at lift lug	0.00°	

### Lug Pin Diameter - Shear stress

$$d_{reqd} = (2*F_v / (\pi*\sigma_s))^{0.5}$$

$$= (2*29,927 / (\pi*13,320))^{0.5} = \underline{1.196"}$$

$$d_{reqd} / D_p = 1.196 / 1.625 = 0.74 \quad \text{Acceptable}$$

$$\sigma = F_v / A$$

$$= F_v / (2*(0.25*\pi*D_p^2))$$

$$= 29,927 / (2*(0.25*\pi*1.625^2)) = 7,215 \text{ psi}$$

$$\sigma / \sigma_s = 7,215 / 13,320 = 0.54 \quad \text{Acceptable}$$

### Lug Thickness - Tensile stress

$$t_{reqd} = F_v / ((D - d)*\sigma_t)$$

$$= 29,927 / ((7 - 2)*19,980) = 0.2996"$$

$$t_{reqd} / t = 0.2996 / 1.25 = 0.24 \quad \text{Acceptable}$$

$$\sigma = F_v / A$$

$$= F_v / ((D - d)*t)$$

$$= 29,927 / ((7 - 2)*1.25) = 4,788 \text{ psi}$$

$$\sigma / \sigma_t = 4,788 / 19,980 = 0.24 \quad \text{Acceptable}$$

### Lug Thickness - Bearing stress

$$t_{reqd} = F_v / (D_p*\sigma_p)$$

$$= 29,927 / (1.625*29,970) = \underline{0.6145"}$$

$$t_{\text{reqd}} / t = 0.6145 / 1.25 = 0.49 \quad \text{Acceptable}$$

$$\begin{aligned} \sigma &= F_v / A_{\text{bearing}} \\ &= F_v / (D_p * t) \\ &= 29,927 / (1.625 * (1.25)) = 14,733 \text{ psi} \end{aligned}$$

$$\sigma / \sigma_p = 14,733 / 29,970 = 0.49 \quad \text{Acceptable}$$

### Lug Thickness - Shear stress

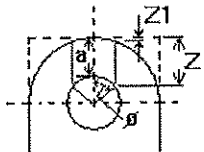
$$\begin{aligned} t_{\text{reqd}} &= [F_v / \sigma_s] / (2 * L_{\text{shear}}) \\ &= (29,927 / 13,320) / (2 * 2.6879) = \underline{0.4179"} \end{aligned}$$

$$t_{\text{reqd}} / t = 0.4179 / 1.25 = 0.33 \quad \text{Acceptable}$$

$$\begin{aligned} \tau &= F_v / A_{\text{shear}} \\ &= F_v / (2 * t * L_{\text{shear}}) \\ &= 29,927 / (2 * 1.25 * 2.6879) = 4,454 \text{ psi} \end{aligned}$$

$$\tau / \sigma_s = 4,454 / 13,320 = 0.33 \quad \text{Acceptable}$$

Shear stress length (per Pressure Vessel and Stacks, A. Keith Escoe)



$$\begin{aligned} \phi &= 55 * D_p / d \\ &= 55 * 1.625 / 2 \\ &= 44.6875^\circ \end{aligned}$$

$$\begin{aligned} Z &= 0.5 * (D - d) + 0.5 * D_p * (1 - \cos(\phi)) \\ &= 0.5 * (7 - 2) + 0.5 * 1.625 * (1 - \cos(44.6875)) \\ &= 2.7349" \end{aligned}$$

$$\begin{aligned} Z1 &= 0.5 * D - \text{sqr}(0.25 * D * D - (0.5 * D_p * \sin(\phi))^2) \\ &= 0.5 * 7 - \text{sqr}(0.25 * 7 * 7 - (0.5 * 1.625 * \sin(44.6875))^2) \\ &= 0.047" \end{aligned}$$

$$\begin{aligned} L_{\text{shear}} &= Z - Z1 \\ &= 2.6879" \end{aligned}$$

### Lug Plate Stress

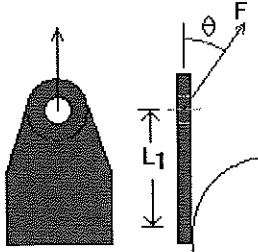
Lug stress, tensile + bending, during rotational lift:

$$\begin{aligned} \sigma_{\text{ratio}} &= [F_{\text{ten}} / (A_{\text{ten}} * \sigma_t)] + [M_{\text{bend}} / (Z_{\text{bend}} * \sigma_b)] \leq 1 \\ &= [(F_{\text{top}}(\alpha) * \sin(\alpha)) / (t * B * \sigma_t)] + [(6 * F_{\text{top}}(\alpha) * L * \cos(\alpha)) / (t * B^2 * \sigma_b)] \leq 1 \end{aligned}$$

$$\begin{aligned}
 &= 15,813 \cdot \sin(18.0) / (1.25 \cdot 13 \cdot 19,980) + 6 \cdot (15,813) \cdot 23 \cdot \cos(18.0) / \\
 &= (1.25 \cdot 13^2 \cdot 22,201) \\
 &= \underline{0.46} \quad \text{Acceptable}
 \end{aligned}$$

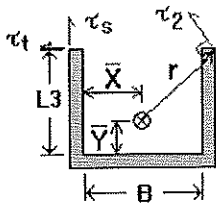
### Weak Axis Bending Stress

Maximum lift cable angle from vertical  $\theta = 6.23^\circ$



$$\begin{aligned}
 \sigma_b &= M / Z & &= (F \cdot \sin(\theta) \cdot L_1) / Z \\
 F \cdot \cos(\theta) &= 0.5 \cdot W & &\Rightarrow F = 0.5 \cdot W / \cos(\theta) \\
 \theta &= \arctan( (2 \cdot \sigma_b \cdot Z) / (W \cdot L_1) ) \\
 \theta &= \arctan( (2 \cdot 22,201 \cdot (13 \cdot 1.25^2 / 6)) / (59,854 \cdot 23) ) & &= 6.23^\circ
 \end{aligned}$$

### Weld Stress



Weld stress, direct and torsional shear, during rotational lift:

Direct shear:

Maximum weld shear stress occurs at lift angle  $18.00^\circ$ ; lift force = 15,813 lb,

$$\begin{aligned}
 A_{\text{weld}} &= 0.707 \cdot t_w \cdot (2 \cdot L_3 + B) \\
 &= 0.707 \cdot 0.75 \cdot (2 \cdot 5 + 13) = 12.1958 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 \tau_t &= F_{\text{lug}} \cdot \cos(\alpha) / A_{\text{weld}} \\
 &= 15,813 \cdot \cos(18.0) / 12.1958 = 1,233 \text{ psi}
 \end{aligned}$$

$$\begin{aligned}
 \tau_s &= F_{\text{lug}} \cdot \sin(\alpha) / A_{\text{weld}} \\
 &= 15,813 \cdot \sin(18.0) / 12.1958 = 401 \text{ psi}
 \end{aligned}$$

Torsional shear:

Weld centroid:

$$Y_{\text{bar}} = L_3^2 / (2 \cdot L_3 + B) \\ = 5^2 / (2 \cdot 5 + 13) = 1.087''$$

Second polar moment of area:

$$J = 0.707 \cdot t_w \cdot ((8 \cdot L_3^3 + 6 \cdot L_3 \cdot B^2 + B^3) / 12 - L_3^4 / (2 \cdot L_3 + B)) \\ = 0.707 \cdot 0.75 \cdot ((8 \cdot 5^3 + 6 \cdot 5 \cdot 13^2 + 13^3) / 12 - 5^4 / (2 \cdot 5 + 13)) = 350.89 \text{ in}^4$$

Radial distance from centroid to weld:

$$r = \text{sqr}((X_{\text{bar}})^2 + (L_3 - Y_{\text{bar}})^2) \\ = \text{sqr}((0.5 \cdot 13)^2 + (5 - 1.087)^2) = 7.587''$$

$$\theta_r = \arctan((L_3 - Y_{\text{bar}}) / (X_{\text{bar}})) \\ = \arctan(3.913 / 6.5) = 31.05^\circ$$

$$\tau_2 = M \cdot r / J \\ = [F(\alpha) \cdot \cos(\alpha) \cdot (L + L_3 - Y_{\text{bar}})] \cdot r / J \\ = (15,813 \cdot \cos(18.0) \cdot 26.913) \cdot 7.587 / 350.8891 \\ = 8,752 \text{ psi}$$

$$\tau_{\text{ratio}} = \text{sqr}((\tau_1 + \tau_2 \cdot \sin(\theta_r))^2 + (\tau_s + \tau_2 \cdot \cos(\theta_r))^2) / \tau_{\text{allowable}} \leq 1 \\ = \text{sqr}((1,233 + 8,752 \cdot \sin(31.05))^2 + (401 + 8,752 \cdot \cos(31.05))^2) / 13,320 \\ = \underline{0.73} \quad \text{Acceptable}$$

### WRC 107 Analysis

Maximum stress ratio occurs at lift angle = 90.00° with lift force = 29,927 lb<sub>f</sub>

Geometry	
Height (radial)	1.25"
Width (circumferential)	13"
Length	5"
Fillet Weld Size:	0.75"
Located On	SHELL RG (5" from top end)
Location Angle	0.00° and 180.00°

Applied Loads	
Radial load, $P_r$	0 $lb_f$
Circumferential moment, $M_c$	0 $lb_f\text{-in}$
Circumferential shear, $V_c$	0 $lb_f$
Longitudinal moment, $M_L$	18,704.5 $lb_f\text{-in}$
Longitudinal shear, $V_L$	29,927.13 $lb_f$
Torsion moment, $M_t$	0 $lb_f\text{-in}$
Internal pressure, $P$	0 psi
Mean shell radius, $R_m$	40.25"
Design factor	3

**Maximum stresses due to the applied loads at the lug edge**

$$\gamma = R_m / T = 40.25 / 2.5 = 16.1$$

$$C_1 = 7.25, C_2 = 3.25 \text{ in}$$

$$\text{Local circumferential pressure stress} = P \cdot R_i / T = 0 \text{ psi}$$

$$\text{Local longitudinal pressure stress} = P \cdot R_i / (2 \cdot T) = 0 \text{ psi}$$

$$\text{Maximum combined stress } (P_L + P_b + Q) = 1,842 \text{ psi}$$

$$\text{Allowable combined stress } (P_L + P_b + Q) = \pm 3 \cdot S = \pm 60,000 \text{ psi}$$

The maximum combined stress  $(P_L + P_b + Q)$  is within allowable limits.

$$\text{Maximum local primary membrane stress } (P_L) = -47 \text{ psi}$$

$$\text{Allowable local primary membrane stress } (P_L) = \pm 1.5 \cdot S = \pm 30,000 \text{ psi}$$

The maximum local primary membrane stress  $(P_L)$  is within allowable limits.

Stresses at the lug edge per WRC Bulletin 107										
Figure	value	$\beta$	$A_u$	$A_l$	$B_u$	$B_l$	$C_u$	$C_l$	$D_u$	$D_l$
3C*	2.808	0.1161	0	0	0	0	0	0	0	0
4C*	2.8391	0.1542	0	0	0	0	0	0	0	0
1C	0.1169	0.1582	0	0	0	0	0	0	0	0
2C-1	0.0848	0.1582	0	0	0	0	0	0	0	0
3A*	0.4457	0.1379	0	0	0	0	0	0	0	0
1A	0.0957	0.1696	0	0	0	0	0	0	0	0
3B*	1.238	0.1055	-47	-47	47	47	0	0	0	0
1B-1	0.0512	0.1295	-176	176	176	-176	0	0	0	0
Pressure stress*			0	0	0	0	0	0	0	0
Total circumferential stress			-223	129	223	-129	0	0	0	0
Primary membrane circumferential stress*			-47	-47	47	47	0	0	0	0
3C*	2.4854	0.1542	0	0	0	0	0	0	0	0
4C*	3.0075	0.1161	0	0	0	0	0	0	0	0
1C-1	0.1403	0.1305	0	0	0	0	0	0	0	0
2C	0.1041	0.1305	0	0	0	0	0	0	0	0
4A*	0.6306	0.1379	0	0	0	0	0	0	0	0
2A	0.0568	0.1354	0	0	0	0	0	0	0	0
4B*	0.3288	0.1055	-10	-10	10	10	0	0	0	0
2B-1	0.0863	0.114	-338	338	338	-338	0	0	0	0
Pressure stress*			0	0	0	0	0	0	0	0
Total longitudinal stress			-348	328	348	-328	0	0	0	0
Primary membrane longitudinal stress*			-10	-10	10	10	0	0	0	0
Shear from $M_l$			0	0	0	0	0	0	0	0
Circ shear from $V_c$			0	0	0	0	0	0	0	0
Long shear from $V_L$			0	0	0	0	-921	-921	921	921
Total Shear stress			0	0	0	0	-921	-921	921	921
Combined stress ( $P_L+P_b+Q$ )			-348	328	348	-328	1,842	1,842	1,842	1,842

\* denotes primary stress.

TAILING LUG

Geometry Inputs	
<p>The diagram illustrates the geometry of a tailing lug. The front view shows a rectangular plate of length <math>L</math> and height <math>H</math> with a central hole of diameter <math>d</math>. The distance from the hole center to the left edge is <math>a_1</math>, and to the right edge is <math>a_2</math>. The angle between the vertical axis and the line from the hole center to the top edge is <math>\beta</math>. The thickness of the plate is <math>t</math>. The side view shows the thickness <math>t</math> and the weld size <math>t_w</math>.</p>	
Attached To	SKIRT
Material	SA-516-70
Orientation	Longitudinal
Distance of Lift Point From Datum	-41.1264"
Angular Position	270°
Length, L	8"
Height, H	6.875"
Thickness, t	0.81"
Hole Diameter, d	1.5"
Pin Diameter, $D_p$	1.25"
Load Eccentricity, $a_1$	0"
Distance from Load to Shell or Pad, $a_2$	3"
Load Angle Normal to Vessel, $\beta$	0°
Load Angle from Vertical, $\phi$	0°
<b>Welds</b>	
Size, $t_w$	0.375"

Intermediate Values	
Load Factor	1.5000
Vessel Weight (new, incl. Load Factor), W	59,854.3 lb
Lug Weight (new), $W_{lug}$	12.6 lb
Distance from Center of Gravity to Top Lug, $l_1$	99.3133"
Distance from Center of Gravity to Tail Lug, $l_2$	96.813"
Distance from Vessel Center Line to Tail Lug, $l_3$	44.5"
Allowable Stress, Tensile, $\sigma_t$	19,980 psi
Allowable Stress, Shear, $\sigma_s$	13,320 psi
Allowable Stress, Bearing, $\sigma_p$	29,970 psi
Allowable Stress, Bending, $\sigma_b$	22,201 psi
Allowable Stress, Weld Shear, $\tau_{allowable}$	13,320 psi
Allowable Stress set to 1/3 Sy per ASME B30.20	No

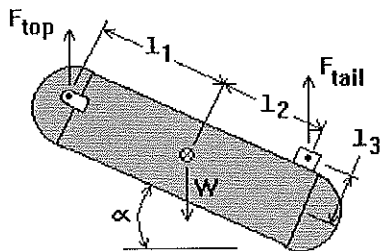
Summary Values	
Required Lift Pin Diameter, $d_{reqd}$	1.2036"
Required Lug Thickness, $t_{reqd}$	0.809"
Lug Stress Ratio, $\sigma_{ratio}$	0.41
Weld Shear Stress Ratio, $\tau_{ratio}$	0.86
Lug Design	Acceptable
Local Stresses WRC 107	Unacceptable

### Lift Forces

Lift force on lugs during rotational lift ( $0^\circ \leq \alpha \leq 90^\circ$ ):

$$2 * F_{top} = W * (l_2 * \cos(\alpha) + l_3 * \sin(\alpha)) / (l_1 * \cos(\alpha) + l_2 * \cos(\alpha) + l_3 * \sin(\alpha))$$

$$F_{tail} = W - (2 * F)$$



$\alpha$ [°]	$F_{top}$ [lbf]	$F_{tail}$ [lbf]
0	14,773	30,309
15	15,641	28,572
30	16,528	26,798
45	17,575	24,704
60	19,048	21,758
75	21,722	16,411
90	29,927	0
44 <sup>1</sup>	17,497	24,861
46 <sup>2</sup>	17,656	24,543
<sup>1</sup> Lift angle at maximum lug stress.		
<sup>2</sup> Lift angle at maximum weld stress.		

Lug loading at $\alpha = 0^\circ$	
Total lift force	
$F = F_{top} / \cos(\phi)$	
$F = 30,309 / \cos(0.0) =$	30,309 lb <sub>f</sub>
Tensile force (parallel to lug normal)	
$F_t = F \cdot \cos(\beta)$	
$F_t = 30,309 \cdot \cos(0.0) =$	30,309 lb <sub>f</sub>
Shear force (parallel to lug weld)	
$F_s = F \cdot \sin(\beta)$	
$F_s = 30,309 \cdot \sin(0.0) =$	0 lb <sub>f</sub>

### Lug Pin Diameter - Shear stress

$$d_{reqd} = (2 \cdot F / (\pi \cdot \sigma_s))^{0.5}$$

$$= (2 \cdot 30,309 / (\pi \cdot 13,320))^{0.5} = 1.2036"$$

$$d_{reqd} / D_p = 1.2036 / 1.25 = 0.96 \quad \text{Acceptable}$$

$$\sigma = F / A$$

$$= F / (2 \cdot (0.25 \cdot \pi \cdot D_p^2))$$

$$= 30,309 / (2 \cdot (0.25 \cdot \pi \cdot 1.25^2)) = 12,349 \text{ psi}$$

$$\sigma / \sigma_s = 12,349 / 13,320 = 0.93 \quad \text{Acceptable}$$

### Lug Thickness - Tensile stress

$$t_{reqd} = F_t / ((L - d) \cdot \sigma_t)$$

$$= 30,309 / ((8 - 1.5) \cdot 19,980) = 0.2334"$$

$$t_{\text{reqd}} / t = 0.2334 / 0.81 = 0.29 \quad \text{Acceptable}$$

$$\begin{aligned} \sigma &= F_r / A \\ &= F_r / ((L - d) * t) \\ &= 30,309 / ((8 - 1.5) * 0.81) = 5,757 \text{ psi} \end{aligned}$$

$$\sigma / \sigma_t = 5,757 / 19,980 = 0.29 \quad \text{Acceptable}$$

### Lug Thickness - Bearing stress

$$\begin{aligned} t_{\text{reqd}} &= F / (D_p * \sigma_p) \\ &= 30,309 / (1.25 * 29,970) = \underline{0.809"} \end{aligned}$$

$$t_{\text{reqd}} / t = 0.809 / 0.81 = 1.00 \quad \text{Acceptable}$$

$$\begin{aligned} \sigma &= F / A_{\text{bearing}} \\ &= F / (D_p * t) \\ &= 30,309 / (1.25 * (0.81)) = 29,934 \text{ psi} \end{aligned}$$

$$\sigma / \sigma_p = 29,934 / 29,970 = 1 \quad \text{Acceptable}$$

### Lug Thickness - Shear stress

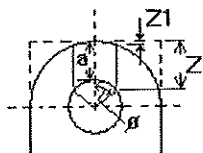
$$\begin{aligned} t_{\text{reqd}} &= [F_v / \sigma_s] / (2 * L_{\text{shear}}) \\ &= (30,309 / 13,320) / (2 * 3.3145) = \underline{0.3432"} \end{aligned}$$

$$t_{\text{reqd}} / t = 0.3432 / 0.81 = 0.42 \quad \text{Acceptable}$$

$$\begin{aligned} \tau &= F_v / A_{\text{shear}} \\ &= F_v / (2 * t * L_{\text{shear}}) \\ &= 30,309 / (2 * 0.81 * 3.3145) = 5,645 \text{ psi} \end{aligned}$$

$$\tau / \sigma_s = 5,645 / 13,320 = 0.42 \quad \text{Acceptable}$$

Shear stress length (per Pressure Vessel and Stacks, A. Keith Escoe)



$$\begin{aligned} \phi &= 55 * D_p / d \\ &= 55 * 1.25 / 1.5 \\ &= 45.8333^\circ \end{aligned}$$

$$L_{\text{shear}} = (H - a2 - 0.5 * d) + 0.5 * D_p * (1 - \cos(\phi))$$

$$\begin{aligned}
&= (6.875 - 3 - 0.5 \cdot 1.5) + 0.5 \cdot 1.25 \cdot (1 - \cos(45.8333)) \\
&= 3.3145''
\end{aligned}$$

### Lug Plate Stress

Lug stress tensile + bending during lift:

$$\begin{aligned}
\sigma_{\text{ratio}} &= [F_{\text{ten}} / (A_{\text{ten}} \cdot \sigma_t)] + [M_{\text{bend}} / (Z_{\text{bend}} \cdot \sigma_b)] \leq 1 \\
&= [(F_{\text{tail}}(\alpha) \cdot \cos(\alpha)) / (t \cdot L \cdot \sigma_t)] + [(6 \cdot \text{abs}(F_{\text{tail}}(\alpha) \cdot \sin(\alpha) \cdot \text{Hght} - F_{\text{tail}}(\alpha) \cdot \cos(\alpha) \cdot a_1)) / (t \cdot L^2 \cdot \sigma_b)] \leq 1 \\
&= (24,861 \cdot \cos(44.0)) / (0.81 \cdot 8 \cdot 19,980) + 6 \cdot \text{abs}(24,861 \cdot \sin(44.0) \cdot 3 - 24,861 \cdot \cos(44.0) \cdot 0) / \\
&= (0.81 \cdot 8^2 \cdot 22,201) \\
&= \underline{0.41} \quad \text{Acceptable}
\end{aligned}$$

### Weld Stress

Weld stress, tensile, bending and shear during lift:

Direct shear:

Maximum shear stress occurs at lift angle 46.00°; lift force = 24,543 lb<sub>f</sub>

$$\begin{aligned}
F_{\text{lug}} &= F_{\text{top}} / \cos(\phi) \\
&= 24,543 / \cos(0.0) = 24,543 \text{ lb}_f
\end{aligned}$$

$$\begin{aligned}
A_{\text{weld}} &= 2 \cdot (0.707) \cdot t_w \cdot (L + t) \\
&= 2 \cdot (0.707) \cdot 0.375 \cdot (8 + 0.81) = 4.6715 \text{ in}^2
\end{aligned}$$

$$\begin{aligned}
\tau_t &= F_{\text{tail}} \cdot \cos(\alpha) / A_{\text{weld}} \\
&= 24,543 \cdot \cos(46.0) / 4.6715 = 3,650 \text{ psi}
\end{aligned}$$

$$\begin{aligned}
\tau_s &= F_{\text{tail}} \cdot \sin(\alpha) / A_{\text{weld}} \\
&= 24,543 \cdot \sin(46.0) / 4.6715 = 3,779 \text{ psi}
\end{aligned}$$

$$\begin{aligned}
\tau_b &= M \cdot c / I \\
&= 3 \cdot (F_{\text{lug}} \cdot \sin(\beta) \cdot \text{Hght} - F_{\text{lug}} \cdot \cos(\beta) \cdot a_1) / (0.707 \cdot h \cdot L \cdot (3 \cdot t + L)) \\
&= 3 \cdot \text{abs}(24,543 \cdot \sin(46.0) \cdot 3 - 24,543 \cdot \cos(46.0) \cdot 0) / \\
&= (22.1220) \\
&= 7,183 \text{ psi}
\end{aligned}$$

$$\begin{aligned}
\tau_{\text{ratio}} &= \text{sqr}((\tau_t + \tau_b)^2 + \tau_s^2) / \tau_{\text{allowable}} \leq 1 \\
&= \text{sqr}((3,650 + 7,183)^2 + (3,779)^2) / 13,320 \\
&= \underline{0.86} \quad \text{Acceptable}
\end{aligned}$$

## WRC 107 Analysis

Maximum stress ratio occurs at lift angle =  $0.00^\circ$  with lift force = 30,309 lb<sub>f</sub>

Geometry	
Height (radial)	6.875"
Width (circumferential)	0.81"
Length	8"
Fillet Weld Size:	0.375"
Located On	SKIRT (2.875" from bottom end)
Location Angle	270.00°

Applied Loads	
Radial load, $P_r$	-30,308.65 lb <sub>f</sub>
Circumferential moment, $M_c$	0 lb <sub>f</sub> -in
Circumferential shear, $V_c$	0 lb <sub>f</sub>
Longitudinal moment, $M_L$	0 lb <sub>f</sub> -in
Longitudinal shear, $V_L$	0 lb <sub>f</sub>
Torsion moment, $M_t$	0 lb <sub>f</sub> -in
Internal pressure, $P$	0 psi
Mean shell radius, $R_m$	41.3125"
Design factor	3

### Maximum stresses due to the applied loads at the lug edge

$$\gamma = R_m / T = 41.3125 / 0.375 = 110.1667$$

$$C_1 = 0.78, C_2 = 3.12 \text{ in}$$

Note: Actual lug  $C_1 / C_2 < 1 / 4$ ,  $C_1 / C_2 = 1 / 4$  used as this is the minimum ratio covered by WRC 107.

$$\text{Local circumferential pressure stress} = P \cdot R_i / T = 0 \text{ psi}$$

$$\text{Local longitudinal pressure stress} = P \cdot R_i / (2 \cdot T) = 0 \text{ psi}$$

$$\text{Maximum combined stress } (P_L + P_b + Q) = 290,444 \text{ psi}$$

$$\text{Allowable combined stress } (P_L + P_b + Q) = \pm 3 \cdot S = \pm 60,000 \text{ psi}$$

**WRC 107: The combined stress ( $P_L + P_b + Q$ ) is excessive**

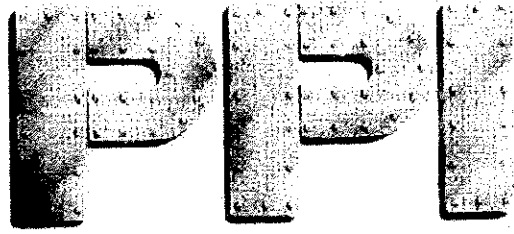
$$\text{Maximum local primary membrane stress } (P_L) = 38,742 \text{ psi}$$

$$\text{Allowable local primary membrane stress } (P_L) = \pm 1.5 \cdot S = \pm 30,000 \text{ psi}$$

**WRC 107: The local primary membrane stress ( $P_L$ ) is excessive**

**Stresses at the lug edge per WRC Bulletin 107**

Figure	value	$\beta$	$A_u$	$A_l$	$B_u$	$B_l$	$C_u$	$C_l$	$D_u$	$D_l$
3C*	18.1103	0.0559	0	0	0	0	35,431	35,431	35,431	35,431
4C*	19.6782	0.0453	38,498	38,498	38,498	38,498	0	0	0	0
1C	0.1972	0.0332	0	0	0	0	255,013	-255,013	255,013	-255,013
2C-1	0.1436	0.0332	185,699	-185,699	185,699	-185,699	0	0	0	0
3A*	1.6356	0.03	0	0	0	0	0	0	0	0
1A	0.1002	0.0346	0	0	0	0	0	0	0	0
3B*	9.2612	0.0476	0	0	0	0	0	0	0	0
1B-1	0.0552	0.0382	0	0	0	0	0	0	0	0
<b>Pressure stress*</b>			0	0	0	0	0	0	0	0
<b>Total circumferential stress</b>			224,197	-147,201	224,197	-147,201	290,444	-219,582	290,444	-219,582
<b>Primary membrane circumferential stress*</b>			38,498	38,498	38,498	38,498	35,431	35,431	35,431	35,431
3C*	19.8031	0.0453	38,742	38,742	38,742	38,742	0	0	0	0
4C*	19.0774	0.0559	0	0	0	0	37,323	37,323	37,323	37,323
1C-1	0.1549	0.0472	200,312	-200,312	200,312	-200,312	0	0	0	0
2C	0.1142	0.0472	0	0	0	0	147,680	-147,680	147,680	-147,680
4A*	1.9536	0.03	0	0	0	0	0	0	0	0
2A	0.059	0.043	0	0	0	0	0	0	0	0
4B*	2.6738	0.0476	0	0	0	0	0	0	0	0
2B-1	0.08	0.0526	0	0	0	0	0	0	0	0
<b>Pressure stress*</b>			0	0	0	0	0	0	0	0
<b>Total longitudinal stress</b>			239,054	-161,570	239,054	-161,570	185,003	-110,357	185,003	-110,357
<b>Primary membrane longitudinal stress*</b>			38,742	38,742	38,742	38,742	37,323	37,323	37,323	37,323
<b>Shear from <math>M_l</math></b>			0	0	0	0	0	0	0	0
<b>Circ shear from <math>V_c</math></b>			0	0	0	0	0	0	0	0
<b>Long shear from <math>V_L</math></b>			0	0	0	0	0	0	0	0
<b>Total Shear stress</b>			0	0	0	0	0	0	0	0
<b>Combined stress (<math>P_L+P_b+Q</math>)</b>			239,054	-161,570	239,054	-161,570	290,444	-219,582	290,444	-219,582
* denotes primary stress.										



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

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Item: V-402, COLD SEPARATOR

# **Materials**

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**Heat Number Map**

**Pg. 3-42**

**Material Test Reports (MTR'S)**



Professional Projects Inc.  
18115 Telge Rd. Cypress, TX 77429

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MANUFACTURER'S MTR + WELDER ID MAP

CUSTOMER  
UOP THOMAS RUSSELL

JOB # 5654

S/O# 5654-1

WELD IDENTIFIER	DESCRIPTION	MATERIAL	HEAT NO. / HEAT CODE	WELDER ID.
<b>HEAD MATERIAL</b>				
C-1(CAT.B)	78"ID X 2.2262" MIN THK ELLIP HD	SA-516-70N	3W893 (HBZ-06)	K
C-2(CAT.B)	78"ID X 2.2262" MIN THK ELLIP HD	SA-516-70N	3W893 (HBZ-06)	K
<b>SHELL &amp; SKIRT RING MATERIAL</b>				
L-1(CAT.A)	2.5" X 78" ID CYLINDER	SA-516-70N	3W963 (HBZ-05)	K
SKIRT(CAT.B)	3/8" X 83" OD X 3'	SA-516-70	813W61910 (HBZ-109)	Q
<b>FALNGES &amp; NOZZLES</b>				
A(CAT.C)	8" 600# "HB" LWN X 14" LG	SA-350-LF2-CL.1	Z573 (XAN-83)	K
B(CAT.C)	8" 600# "HB" LWN X 14" LG	SA-350-LF2-CL.1	Z573 (XAN-83)	Q
C(CAT.C)	4" 600# "HB" LWN X 12" LG	SA-350-LF2-CL.1	W353 (XAN-84)	DOT.T
C-PIPE(CAT.D)	4" SCH/40 SMLS PIPE	SA-106B	1013341771 (AFC-140)	DOT.T
C-WELD ELL(CAT.D)	4" LR 90° WELD ELL	SA-234-WPB	LW14 (XAN-85)	DOT.T
D1(CAT.C)	1" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LRB4 (XAN-86)	Q
D2(CAT.C)	1" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LRB4 (XAN-86)	Q
E(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
F1(CAT.C)	1" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LRB4 (XAN-86)	Q
F2(CAT.C)	1" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LRB4 (XAN-86)	Q
G1(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
G2(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
G3(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
G4(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
H(CAT.C)	18" 600# RF "HB" LWN X 18" LG	SA-350-LF2-CL.1	Z580 (XAN-88)	DOT.T
J(CAT.C)	3/4" X 4" LG 6M THD CPLTS	SA-350-LF2-CL.1	LSJ4 (XAN-87)	Q
<b>PIPE MATERIAL</b>				
SKIRT ACCESS	18" STD WT. SMLS PIPE	SA-106B	M33891 (AFI-59)	I
SKIRT VENT	1-1/2" STD WT. SMLS PIPE	SA-106B	1013347382 (AFB-37)	I
INLET DIV. PIPE	1" X-STG SMLS PIPE	SA-106B	1016386730 (AFI-61)	E
<b>PLATE MATERIAL</b>				
GROUNDING LUG	1/4" X 2" PLATE	SA-36	A3R1772-03 (YAK-21)	E
LIFTING LUG	1-1/4" PLATE	SA-516-70	E5E005-C47 (HBZ-77)	E



Professional Projects Inc.  
18115 Telge Rd. Cypress, TX 77429

PAGE 2 OF 2

MANUFACTURER'S MTR + WELDER ID MAP

CUSTOMER  
UOP THOMAS RUSSELL

JOB # 5654

S/O# 5654-1

WELD IDENTIFIER	DESCRIPTION	MATERIAL	HEAT NO. / HEAT	WELDER ID.
	<b>PLATE MATERIAL</b>			
ISR-1A PLATE	3/8" X 2" X 1" LG	SA-36	JW15101084 (YAL-5)	I
ISR-2 PLATE	3/8" X 2" X 1" LG	SA-36	JW15101084 (YAL-5)	I
ISR-3 PLATE	3/8" X 2" X 1" LG	SA-36	JW15101084 (YAL-5)	I
INLET DIVERTER	5/8" PLATE	SA-516-70	812B34840 (HBZ-76)	I
BASEPLATE	7/8" PL	SA-516-70	821P00650 (HBZ-74)	E
DEMISTER DETAIL	3/8" PLATE	SA-516-70	E6K162-A10 (HBZ-75)	E
	<b>BAR MATERIAL</b>			
ISR-1A	1/2" ROUND BAR	SA-36	JW14105769 (YAK-125)	I
ISR-2	1/2" ROUND BAR	SA-36	JW14105769 (YAK-125)	I
ISR-3	1/2" ROUND BAR	SA-36	JW14105769 (YAK-125)	I
	<b>BLIND FLANGE</b>			
H BLIND	18" 600# RF BLIND	SA-350-LF2-CL.1	91436 (XAN-89)	N/A

Rank Head Manufacturing Complex  
10703 Sheldon Road  
Houston, TX 77044

# UNI-FORM COMPONENTS CO.

(281) 456-9310  
(800) 231-3272 toll-free  
(281) 456-0245 fax

Packlist No.	Customer ID
PL-84599	PROPRO

## MATERIAL CERTIFICATION

Customer PO No.	UCC Job No.	Date Cert. Originated
5654-1	128421	3/27/2017

**Sold To:**  
PROFESSIONAL PROJECTS  
18115 TELGE RD

**Ship To:**  
PROFESSIONAL PROJECTS  
18115 TELGE RD

CYPRESS TX 77410

CYPRESS TX 77410

Ln	Order Qty	Ship Qty	B/O Qty	Part Description
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1	2	2	0	HEAD 2:1 ELLIP, 78 ID X 2-1/2 SA516-70 Unit of Measure: EA	2.2317" MIN
---	---	---	---	---	-------------

Code: 3W893 HEAT/SLAB: 813V65970 / E043960 GRADE: SA516-70 Size: 2.5 X 108 X 216 MILL: ARCELOR MITTAL

3/28/17 PPI  
G.C. HBZ-06  
F.W.

### MILL TEST REPORTS ATTACHED

The chemical and physical properties as indicated on the attached report are the results of the Mill Tests of the raw material used in the manufacture of these products and are certified to meet only the minimum requirements of the ASME and/or ASTM specifications for the material.

1. We hereby certify that these heads were hot formed at the required normalizing temperature and air cooled, in accordance with all applicable specifications.
2. We hereby certify that these heads comply with tolerances of UG-81 of ASME Section VIII, Div. 1.

WE HEREBY CERTIFY THAT THIS REPORT COVERING THE ABOVE AND ATTACHED INFORMATION IS TRUE AND CORRECT AS SHOWN AND CONTAINED IN OUR RECORDS.



Quality Control

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

C-1 & C-2 HEADS

**ARCELORMITTAL BURNS HARBOR PLATE**  
 QUALITY ASSURANCE  
 REPORT OF TEST AND ANALYSES

*5W892-893*

U.S. STEEL BURNS HARBOR, Indiana

SHIPMENT NO. <b>803-16765</b>		DATE SHIPPED <b>02-14-17</b>	CAR OR VEHICLE NO. <b>CSS-CHGO-UP</b>	BVRY 062149	PAGE <b>2</b>
S O L D I D O	UNI-FORM COMPONENTS CO 10703 SHELDON RD HOUSTON TX 77044-6003			UNI-FORM COMPONENTS CO THEIR SIDING HOUSTON TX	

SERIAL NUMBER	PAT NO.	HEAT NUMBER	NO. PCS.	SIZE AND QUANTITY				YIELD POINT	TENSILE STRENGTH	AF FRAC. ELONG.	RED.
				THICKNESS	WIDTH OR DIA.	LENGTH	WEIGHT				
				INCHES	INCHES	INCHES	POUNDS	PSI	PSI	IN	%

**QUALITY STEEL MELTED & MANUFACTURED IN THE U. S. A.**  
**PLATES - ASME SA516 GR 70 PVQ KLD FINE GRAIN**  
 PRAC 2015 EDITION --- GAS CUT 4  
 SIDES MILL TEST PCS NORM 1650F FOR  
 1HR/IN AIRCL --- TEST CERTS ARE  
 PREPARED IN ACCORD WITH PROCEDURES  
 OUTLINED IN EN 10204:2004 TYPE 3.1  
 NO WELD REPAIR WAS PERFORMED ON BELOW PLATE(S)  
**MFST - MFST PPI 0069378- 0001 MFST TEST CERTS ARE**  
 PREPARED IN ACCORD WITH PROCEDURES OUTLINED IN  
 EN MFST 10204:2004 TYPE 3.1  
 - LIFT MAX 10  
 TON UNLDG FORK LIFT-SIDE  
 CO# 35158 GH 353-1631K

TEST SPECIMENS LABORATORY HEAT TREATED AND YIELD STRENGTH @ .5% E.U.L.

E043959	813V65960	1	2	1/2	108	216	16540	50800	74100	2	39	<i>3W892</i>
E043960	823V65970	1	2	1/2	108	216	16540	48500	74900	2	37	<i>3W893</i>

Q-QUENCH TEMPERATURE	T-TEMPERATURE	N-NORMALIZE TEMPERATURE
----------------------	---------------	-------------------------

SERIAL NUMBER	PAT NO.	HEAT NUMBER	HARD BHN	BEND	THICKNESS INCHES	TYPE	SIZE	DIR	TEST TEMP F	CHARPY IMPACT								
										ENERGY FT LBS			SHEAR(%)			LAT. EXP MILS		
										1	2	3	1	2	3	1	2	3

PPI  
*3/28/17* Q.C. #B2-06  
 F.W.

HEAT NUMBER	CHEMICAL ANALYSIS																	MQLAID GRAIN SIZE
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Ti	Al	B	Cb	N	Sn		
813V65960	.19	1.10	.012	.004	.321	.227	.18	.03	.040	.002	.002	.036	.0002	.003	.004	.004		
823V65970	.18	1.08	.011	.004	.322	.227	.18	.03	.039	.002	.002	.033	.0002	.002	.005	.004		

I certify that the above results are a true and correct copy of actual results contained in records maintained by ArcelorMittal Burns Harbor and are in full compliance with the requirements of the specification cited above. This test report cannot be altered and must be transmitted intact with any subsequent third party test reports, if required.  
**R. SPANGLER II** PER **LSS**

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429  
 C-1 & C-2 HEADS



# GOOLSBY TESTING, INC.

2620 WILSON ROAD - P.O. BOX 1416  
HUMBLE, TEXAS 77347-1416  
(281) 540-1255 FAX (281) 540-8125

CLIENT: UNIFORM COMPONENTS 10703 SHELDON RD. HOUSTON, TEXAS 77044	DATE RECEIVED: 3-24-17 DATE TESTED: 3-24-17 REPORT DATE: 3-24-17
PURCHASE ORDER: 143120	LABORATORY TEST NO: 17-03-108584
GT# :3003 SHOP ORDER#:128421	PROCEDURE: #15 #16
HEAT # : 3W893 SLAB # : N/A	LIGHTING: 205FC
HUMIDITY: 53.0	TEMP: 72.1°F
ENVIRONMENTAL CONDITIONS: BP: 30.0	
MATERIAL THICKNESS: 2-1/2"	
MATERIAL/DESCRIPTION: SA516-70N BASE PLATE	
SPECIFICATIONS: ASME SECT. VIII DIV. 1	
SPECIAL REQUIREMENTS: N/A	

### CHARPY IMPACT TEST

TESTING MACHINE: BALDWIN SATEC S1-1 K3 S/N 1706					
LINEAR VELOCITY OF HAMMER: 17 FT/SEC.			TEST METHOD: SIMPLE BEAM CHARPY		
COOLANT BATH: FTS SYSTEMS S/N G6-1			EFFECTIVE ENERGY: 300 FT/LBS./406.7 JOULES		
SPECIMEN TYPE: ASTM TYPE A LVNC			SPECIMEN SIZE: 10 MM X 10 MM		
SPECIMEN TEMP: -50° F			ACCEPTANCE CRITERIA: 15/12 FT/LBS		
SPECIMEN LOCATION	WIDTH	EFFECTIVE SECTION SIZE	IMPACT VALUES FOOT POUNDS	% SHEAR FRACTURE	LATERAL EXPANSION
BASE	.394	.315	40	20	.028
BASE	.394	.315	49	20	.034
BASE	.394	.315	44	20	.031

MATERIALS TESTED ARE:  ACCEPTABLE  REJECTABLE  RECORDABLE

TECHNICIAN:		GOOLSBY TESTING, INC.	
CHARLES WILLIAMS		PER:	APPROVED SIGNEE
Accepted by:		Company:	

Our letters and reports are for the use of our client to whom they are addressed. Our name may be used only with our prior written approval. Our letters and reports apply only to the sample tested and/or inspected, and do not necessarily represent the quality of other apparently similar or identical materials. The results recorded represent opinions only and are not to be considered as warranties or guarantees of quality, classification or usability of material examined. In no event shall the liability of Goolsby Testing, Inc. as to any items inspected or tested (including liability as to selection and/or results of such tests) exceed the charge of Goolsby Testing, Inc. for the inspection of such items. We shall assume no responsibility following the acceptance by the customer's field representative upon signing of field ticket. Goolsby Testing reporting and certification are completed in accordance with ISO 17025.

3/28/17

PPH  
Q.C.  
F.W.

HBZ-06

Bank Head Manufacturing Complex  
10703 Sheldon Road  
Houston, TX 77044

# UNI-FORM COMPONENTS CO.

(281) 456-9310  
(800) 231-3272 toll-free  
(281) 456-0245 fax

Packlist No	Customer ID
PL-84479	PROPRO

## MATERIAL CERTIFICATION

Customer PO No	UCC Job No	Date Cert. Originated
5654-1	128420	3/21/2017

**Sold To:**  
PROFESSIONAL PROJECTS  
18115 TELGE RD

**Ship To:**  
PROFESSIONAL PROJECTS  
18115 TELGE RD

CYPRESS TX 77410

CYPRESS TX 77410

Ln	Order Qty	Ship Qty	B/O Qty	Part Description
----	-----------	----------	---------	------------------

1	1	1	0	CYLINDER, 78 ID X 2-1/2 SA 516-70 Unit of Measure: SQFT
---	---	---	---	--

Code: 3W963 HEAT/SLAB: S22326 / 03B1 GRADE: SA516-70 Size: 2.5 X 144 X 261 MILL: JSW

3/28/17 PPI  
Q.C. HBZ-05  
F.W.

### MILL TEST REPORTS ATTACHED

The chemical and physical properties as indicated on the attached report are the results of the Mill Tests of the raw material used in the manufacture of these products and are certified to meet only the minimum requirements of the ASME and/or ASTM specifications for the material.

1. Cylinder/Cone comply with tolerances of ASME Section VIII, Div 1, UG-80

WE HEREBY CERTIFY THAT THIS REPORT COVERING THE ABOVE AND ATTACHED INFORMATION IS TRUE AND CORRECT AS SHOWN AND CONTAINED IN OUR RECORDS.

*Stephen C. Shelton PS*

Quality Control

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

L-1 SHELL RING

MET - 05  
9/6/2017

**METALLURGICAL TEST REPORT**

**JSW Steel (USA) INC.**  
5200 East McKinney Road,  
BAYTOWN, TX 77520

**3w9b3**

<b>Bulletin</b> T011559 JSW07400-01 S22326 35191A	<b>Order Item</b> Heat FO No. S22326 35191A	<b>Shipping Mode</b> TRUCK	<b>Order Dimensions</b> 2.5x144x261	<b>Slab Origin</b> JTC No. T011559-2326-1
<b>100% UT PER A435 / A435M</b>				
<b>Plates Certified for the Following grades</b> ASME SA516-70 PN LCVNUT 2015 EDITION				
<b>Hot Rolled Carbon Steel Plates</b> Plates Manufactured in the USA				
<b>Sold To:</b> UNI-FORM COMPONENTS CO. 18969 OLD BEAUMONT HWY 90 HOUSTON, TX 77049				
<b>Ship To:</b> UNI-FORM COMPONENTS 10703 SHELDON RD HOUSTON, TX 77064				



**Specifications**  
PLATE NORMALIZED AT 1650°F FOR 75 MINS.

**Marking Instructions**  
Stencil in 2 locations (S), X Loc. 18 Y Loc. 30; CUST; MADE IN USA (PN F0); DIM GRADE; FREIGHT ORDER ITEM FLA TEID SHIPWEEK SLAB ID; TRANS MODE Stamp in 2 locations (S), X Loc. 18 Y Loc. 12; Slab ID; Slab ID

Carbon Equivalents: CE = C + Mn/6 + (Cr + Mo + V) x 5 + (Ni + Nb) x 15  
PCA = C + Si x 30 + Mn x 20 + Cu x 20 + Ni x 60 + Cr x 20 + Mo x 15 + V x 15 + Nb x 50

Test	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Sa	Al	N	V	B	Ti	Nb	Ca	CE
TABLE	0.24	1.12	0.015	0.010	0.21	0.007	0.008	0.011	0.001	0.009	0.030	0.0058	0.001	0.0002	0.003	0.001	0.0021	0.43

Plate	Slab Identity	Gauge Tested	Yield Point	Tensile Stgth.	Elong. in 2"	YS/UTS Ratio	Yield Strength Determined At	Charpy Impact Test (LCVN) Full Energy in FtLb - F						
								Temp	Test1	Test2	Test3			
1028877A	0351	2.5000	PN	T	45	78	31.0%	0.56	0.2%	50	32	40	32	35

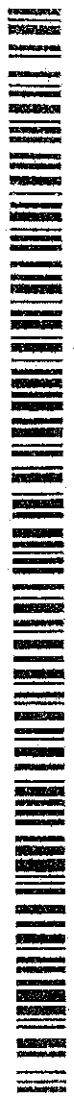
**Plates Certified For The Above Tests**

Material	Thick (IN)	Width (IN)	Len (IN)	Wgt (LB)	Material	Thick (IN)	Width (IN)	Len (IN)	Wgt (LB)
1028877A	2.5000	144.000	261.00	26647					

3/28/17  
PPI  
Q.C. HBZ-05  
F.W.

*Jackie Tamayo*

DIN: EN 10204 2004 3.1 This is to certify that the product described herein was manufactured, sampled, and tested in accordance with the specifications and requirements in such specifications. Fine Grain, Si-Al Fully Killed Steel. We certify that delivery of this product with the requirement of the specification and purchase order received from customer.



Jackie Tamayo 281-383-5325 Jackie.Tamayo@jswsteelus  
Page 1 of 1

<b>CUSTOMER INDIVIDUAL ULTRASONIC OBSERVATION REPORT</b>	Form # MS 15B
	Rev: 0
	Date: 2/24/11
	Pg 1 of 1

Order Item: JSW07400-01 PC:35191A Part No.

Customer Name:	UNI-FORM COMPON
Technique:	LONGITUDINAL
Equipment Make:	KRUATKRAMER
Equipment Number:	USN-58
Surface Condition:	125-RMS
Couple Used:	WATER-COLUMN
Procedure Code:	PL-QA-009 Meets or exceeds the requirements of ASTM A-435 A-578 A. B. C
Acceptance Standard:	1'

Inspection Report Number:	11028877A
Date:	12/22/2017
Probe Type:	TECHSONIC
Probe Frequency:	2.25MHZ
Probe Diameter:	11"
Type of Crystal:	SINGLE
Gains:	139-55

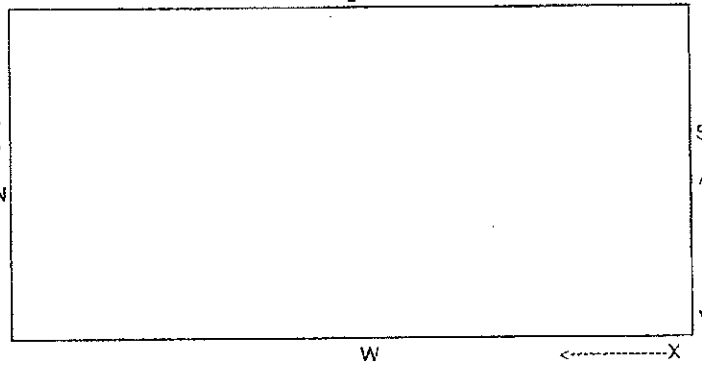
Gauge	2.5000
Heat	S22326
Material Grade(s)	
Grade(s) if applicable	

PL-QA-009  
Meets or exceeds the requirements of  
ASTM  
A-435  
A-578 A. B. C

Linerarity / Horizontal    Vertical  
 Deviation Performed    Daily  
 Indicate the defect location on the sketch below

- Accept
- Reject
- Manual Hold

- 25 - 50%
- ▒ 50 - 75%
- >75%



3/28/17    PPI  
 Q.C. HBZ-05  
 F.W.

Signature

Phillip Martin 2-22-17 3:12 am



06/09/2017 From: AMERICAN ALLOY STEEL, INC.

To: PROFESSIONAL PROJECTS INC

P.O.#: 5654-6

S.O.#: 573999

AA PL#: 5183481

Item: 1 (1 PC) 3/8" X 36" X 264"

TAG #5654

### ArcelorMittal Burns Harbor Plate

QUALITY ASSURANCE REPORT OF TEST AND ANALYSES

US HWY 12 Burns Harbor, Indiana

SHIPMENT NO. 804-00295	DATE SHIPPED 03-31-17	CAR OR VEHICLE NO. AMERICAN COMMERCIAL	PAGE 1
---------------------------	--------------------------	---	-----------

S O L D I D	AMERICAN ALLOY STEEL INC PO BOX 40469 HOUSTON TX 77240-0469			S H I P T O	AMERICAN ALLOY STEEL INC C/O FREIGHT MANAGEMENT & LOGISTICS INBESA TERMINAL-PORT OF HOUSTON 16335 PENINSULA BLVD HOUSTON TX 77015		

S E R I A L N U M B E R	P A T N O.	H E A T N U M B E R	N O. P C S.	S I Z E A N D Q U A N T I T Y				Y I E L D P O I N T	T E N S I L E S T R E N G T H	A F F R A C. E L O N G.	R E D.
				T H I C K N E S S	W I D T H O R D I A.	L E N G T H	W E I G H T				

QUALITY STEEL MELTED & MANUFACTURED IN THE U. S. A.

PLATES - ASTM A516-06 GR 70 PVQ MOD C.20 MAX CU.15 MAX KLD FINE GRAIN PRAC,  
 ASTM A516-06 GR 65 PVQ, ASME SA516 GR 70 PVQ 2015 EDITION, ASME  
 SA516 GR 65 PVQ 2015 EDITION, FIRST TST AS ROLLED-ADD'L TENSION PER  
 TST PC HEAT TREATMENT --- MILL TEST PCS NORM 1650+/-25F FOR  
 30MIN/IN (30 MINUTES MIN), AIRCOOL --- TEST CERTS ARE PREPARED IN  
 ACCORD WITH PROCEDURES OUTLINED IN EN 10204:2004 TYPE 3.1  
 NO WELD REPAIR WAS PERFORMED ON BELOW PLATE(S)

CO# 110777 GH 354-5455A

E549376	813W61910	4	.375	96	360	14700	51700	77800	8	23
(M55)MFST REF#:2							51700	73500	8	24
E549377	813W61910	4	.375	96	360	14700	54400	78500	8	24
(M55)MFST REF#:2							52100	75100	8	26

PPI  
 6/9/17 Q.C. HBZ-109  
 F.W.

Q-QUENCH TEMPERATURE	T-TEMPER TEMPERATURE	N-NORMALIZE TEMPERATURE
----------------------	----------------------	-------------------------

S E R I A L N U M B E R	P A T N O.	H E A T N U M B E R	H A R D B R I N	B E N D	T H I C K N E S S I N C H E S	T Y P E	S I Z E	D I R	T E M P F	C H A R P Y I M P A C T								
										E N E R G Y F T L B S			S H E A R (%)			L A T. E X P		M I L S
										1	2	3	1	2	3	1	2	3

Certified a true copy of the original, retained in our file.  
 AMERICAN ALLOY STEEL, INC.  
 Reviewed By:  
 JP 5/14/2017

H E A T N U M B E R	C H E M I C A L A N A L Y S I S																M O U L D G R A I N S I Z E
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Ti	Al	B	Ca	N	Sn	
813W61910	.18	1.10	.010	.006	.325	.020	.01	.13	.081	.001	.002	.034	.0002	.002	.005	.004	

I certify that the above results are a true and correct copy of actual results contained in records maintained by ArcelorMittal Burns Harbor and are in full compliance with the requirements of the specification cited above. This test report cannot be altered and must be transmitted intact with any subsequent third party test reports, if required.

BHPLTRPT.TIF SUPV. QUALITY ASSURANCE R. SPANGLER II LSS

AMERICAN ALLOY PLATE #813W61910

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX 77429 SKIRT RING



14527 Smith Rd.  
Humble, Texas 77396  
TEL: (281) 441-4088  
FAX: (281) 441-8899

PAGE: 1 of 1  
REPORT # 17-030307  
DATE: 5/1/2017  
FCI ORDER # 77823  
I.A.W. ASME 2015 ED.

CUSTOMER ORDER # 1287649-JG  
SOLD / SHIPPED TO: NORTH SHORE STEEL

Item	Quantity	Description
1	2	8" X 600 X 14" LG RF HB WITH NUT RELIEF

Heat Number: Z573  
Material Type: SA350LF2CL1

CHEMICAL ANALYSIS

PHYSICAL PROPERTIES

C	.160
Mn	1.190
P	.0100
S	.0020
Si	.220
Cr	.140
Mo	.030
V	.046
Cu	.240
Ni	.100
Cb(Nb)	.001
N	.0118
Sn	.011
As	.006
Sb	.001
Ti	.0022
Al	.029
B	.0001
C E	.424

Yield PSI	51,500
Tensile PSI	78,100
Elongation	33.8
Reduction of Area	67.7
Hardness	163/163 HBW
CVN -50 °F	FT LBS 118/115/83
	% Shear 100/100/100
	MLE .083/.075/.056

Heat Treatment: NORMALIZED  
Temperature: 1650 °F  
Time at Temperature: 1/2 HR/IN THK MIN  
Cooling Media: AIR

PPI  
Q.C.  
F.W.

4/11/17

XAN-83

We hereby certify that all test results and process information contained herein are correct and true as contained in the records of the company.

Prepared by:

*Erika Marquez*

Name: Erika Marquez

Title: QA Representative

*[Handwritten Signature]*

A & B



14627 Smith Rd.  
Humble, Texas 77396  
TEL: (281) 441-4088  
FAX: (281) 441-8899

PAGE: 1 of 1  
REPORT # 17-030308  
DATE: 5/1/2017  
FCI ORDER # 77823  
I.A.W. ASME 2015 ED.

CUSTOMER ORDER # 1287649-JG  
SOLD / SHIPPED TO: NORTH SHORE STEEL

Item	Quantity	Description
2	1	4" X 600 X 12" LG RF HB WITH NUT RELIEF

Heat Number: W353  
Material Type: SA350LF2CL1

CHEMICAL ANALYSIS

PHYSICAL PROPERTIES

C	.180
Mn	1.100
P	.0080
S	.0030
Si	.200
Cr	.140
Mo	.010
V	.017
Cu	.200
Ni	.080
Cb(Nb)	.001
Sn	.011
As	.004
Sb	.001
Ti	.0020
Al	.020
B	.0001
C E	.415
Other	Ca=18pp m

Yield PSI	47,900
Tensile PSI	74,000
Elongation	36.1
Reduction of Area	72.4
Hardness	156/156 HBW
CVN -50 °F	FT LBS 97/62/93
	% Shear 100/100/100
	MLE .072/.052/.073

Heat Treatment: NORMALIZED  
Temperature: 1650 °F  
Time at Temperature: 1/2 HR/IN THK MIN  
Cooling Media: AIR

4/11/17 PPI  
Q.C. XAN-84  
F.W.

We hereby certify that all test results and process information contained herein are correct and true as contained in the records of the company.

Prepared by: Erika Marquez  
Name: Erika Marquez Title: QA Representative

UOP-RUSSELL-P.O. # 4500754097-S/O # 5654-1-V-402-COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429



voestalpine Tubulars GmbH & Co KG

5546-21



MIP00010#HT\$A#1/1

Material Test Report (MTR)

FSVAT4STD SL

INSPECTION - CERTIFICATE 3.1

(according to EN 10204)

ABNAHMEPRUEFZEUGNIS 3.1

(gem. EN 10204)

CERTIFICAT DE CONTROLE DES PRODUITS PAR L'USINE 3.1

(selon EN 10204)

Hersteller: voestalpine Tubulars GmbH & Co KG, Austria  
 Manufacturer: voestalpine Tubulars GmbH & Co KG, Austria  
 Producteur: voestalpine Tubulars GmbH & Co KG, Austria

Besteller: VOEST-ALPINE TUBULAR CORPORATION  
 Purchaser: USA-77042 HOUSTON TEXAS  
 Archeteur: INDUSTRIAL PIPING SPEC., TULSA OK 74158-1270

Prüfgegenstand: SEAMLESS STEEL TUBES, LINE PIPE  
 Object of tests: SEAMLESS STEEL TUBES, LINE PIPE  
 Epreuve: SEAMLESS STEEL TUBES, LINE PIPE

Werkstoff: GRADE B / GRADE X42/ GRADE C  
 Material: LP-USA-02  
 Matières: LP-USA-02

Anforderungen: Gr B acc. ASTM A 106 / A 106 M - ASME SA 106-2011  
 Requirements: Gr B acc. ASTM A 53 / A 53 M - ASME SA 53-2012  
 Exigence: Gr B acc. API SPEC 5 L (PSL1)-2007  
 X42 acc. API SPEC 5 L (PSL1)-2007  
 NACE MR 0175 / ISO 15156-2009  
 NACE MR0103-2010 (latest edition)  
 LINEPIPE-01.0

Ausführung: NU, PLAIN END, PE, BOTH ENDS BEVELLED ACC. TO API/ASTM  
 Condition: NU, PLAIN END, PE, BOTH ENDS BEVELLED ACC. TO API/ASTM  
 Cond. de livraison: NU, PLAIN END, PE, BOTH ENDS BEVELLED ACC. TO API/ASTM

Wärmebehandlung: AS ROLLED  
 Heat treatment: AS ROLLED  
 Traitement de chaleur: AS ROLLED

Coupl. die stamped: Coupl. paint stencilling: Fully painted: Bands: heat va SPEC 5L-0033 "API" 04/13 API 5L B/API 5L X42 PSL1 A/SA 53 GRADE B S A/SA 106 GRADE B 4,500" x 0,237" SCHED 40 2660 PSI length ft heat no PO# MIP00010/( ) MADE IN AUSTRIA/( ).

Colour coding: Fully painted: Bands: Purple

Label: PO # MIP 00010, DAT PORT of Houston, TX

Remarks: \*) Grade C without marking on tubes

Alpinestrasse 17  
8652 Kindberg-Aumuehl  
T. +43/3865/22 15-0  
F. +43/3865/2215-532  
www.vatubulars.com

Legal Structure: Limited Partnership  
Location: Kindberg/Austria  
Company Registry Number 165400k  
Commercial Court of Leoben  
DPR 0592684, VAT Nr. ATU 43630406

General Partner: voestalpine Tubulars GmbH  
Legal Structure: Limited Liability Company  
Location: Linz, Company Registry Number 106833f  
Commercial Court of Linz

No. 88776

Auftrags-Nr.: 12977 / 7  
Our works order No.:  
No usine:

Bestellnr.: MIP00010/VATC  
Your order No.: PO#302628

No de la commande:

Zeichen des Lieferwerks: va  
Marking of producer:  
Marque du fabricant:

Erschmelzungsart: BOF  
Melting process: fully killed, produced to  
Procédé d'élaboration: fine grain practice

AFC-140

PPI

Q.C.

F.W.

3/16/15

Kindberg, 26.04.2013

Page 1 of 5

No. 88776

voestalpine Tubulars GmbH & Co KG  
Quality Control / Quality Department

SCHNEIDHOFER

Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

Umfang der Lieferung / Volume of delivery / Contenu de la livraison:

Versandanzeige: Dispatch advice No. Avis d'expédition:	Pos.: Pos.:	Abmessung: Dimension: Dimension:	Bundnr.: Bundle No.: Nombre Fret:	Stückzahl: Number Of: Pièces:	Länge: Length: Longueur:	Gewicht: Weight: Poids:	Los: Lot: Lot:	Schmelze: Heat: Soufflage:
	7	4,500 in x 0,237 in 10,79 lbs/ft	1-38	666	15259,556ft	74968,60kg		

Volume of delivery

Heat	Lot	Remark
1013341444	172813	AD 01
1013341445	172814	AD 01
1013341771	172812	AD 01
1013341794	172811	AD 01

Test results

- 1 Visuelle Inspektion/ Visual inspection: o.B./satisfactory
- 2 Dimensionskontrolle/ Dimensional inspection: o.B./satisfactory
- 3 Wasserinnendruckversuch/Hydrostatic test: 2660 (duration min. 5 sec.) o.B./satisfactory
- 4 Ringfallversuch/Flattening test: o.B./satisfactory
- 5 Streuflussprüfung gem. ASTM E 570 / Flux leakage testing acc. ASTM E 570 (N 12,5 longitudinal, type and size of reference indicator used): o.B./satisfactory

Test remarks

Wir bestätigen, dass die gelieferten Erzeugnisse den Anforderungen der Bestellung entsprechen.  
We hereby certify that the goods delivered are in compliance with the requirements of the order.

AFC-140

PPI  
Q.C.  
P.W.

3/16/15

Kindberg, 26.04.2013

Page 2 of 5

No. 88776

voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department  
**SCHNEIDHOFER**  
Abnahmebeauftragter  
authorized inspection representative  
representant autorisé du contrôle  
**voestalpine**  
ONE STEP AHEAD.

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

C PIPE NOZZLE



voestalpine Tubulars GmbH & Co KG

Tensile testing

Lot No	Test Type	Heat treatment	Temp [°C]	Specimen		Yield Strength [ PSI ]	Tensile Strength [ PSI ]	Elong. [%]	Reduct. in area [%]	
				No.	Type					Dimension [mm]
						Requ. from 42061	60190	23.50		
						Requ. to				
172811	AD 01 Standard	as rolled	20	1	Strip	25.39 x 6.30	R10.50 51198	73824	31.60	0.69
172812	AD 01 Standard	as rolled	20	1	Strip	25.13 x 6.18	R10.50 46847	71648	33.30	0.65
172813	AD 01 Standard	as rolled	20	1	Strip	25.31 x 6.29	R10.50 51198	71938	31.90	0.71
172814	AD 01 Standard	as rolled	20	1	Strip	25.17 x 6.40	R10.50 49022	72228	31.20	0.68

yield strength:  
Gr B: 35500 PSI  
X42: 42100 PSI  
Gr C: 40000 PSI

tensile strength:  
Gr B: 60200 PSI  
X42: 60200 PSI  
Gr C: 70000 PSI

Hardness testing

Lot No	Test Type	Heat treatment	Specimen		Hardness Number		Mean Hardness Number		Variation	
			No.	Location	Test Method	from	to	from		to
								99.50		
172811	AD 01 Standard	as rolled	1	Body	HRB	80.50	81.50	80.67	81.33	0.67
172812	AD 01 Standard	as rolled	1	Body	HRB	78.90	80.50	79.60	80.30	0.70
172813	AD 01 Standard	as rolled	1	Body	HRB	80.00	80.90	80.30	80.43	0.13
172814	AD 01 Standard	as rolled	1	Body	HRB	79.80	80.80	80.10	80.50	0.40

AFC-140

PPI  
Q.C.  
P.W.

3/16/15

Kindberg, 26.04.2013

Page 3 of 5

No. 88776

voestalpine Tubulars GmbH & Co KG  
Quality Testing / Quality Department  
**SCHNEIDER**  
Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle  
**voestalpine**  
ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

Chemical test results

Heat analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
max																	
0.2300		1.0600	0.0300	0.0300	0.4000	0.4000	0.4000			0.1500	0.0800						0.4000

min

0.0000 0.1000 0.2900

1013341444

0.1772 0.2626 0.9790 0.0168 0.0044 0.0394 0.0210 0.0197 0.0231 0.0019 0.0108 0.0015 0.0018 0.0000 0.0045 0.0368 0.0015 0.3532

1013341445

0.1670 0.2629 0.9713 0.0160 0.0033 0.0417 0.0183 0.0207 0.0255 0.0020 0.0051 0.0014 0.0020 0.0000 0.0048 0.0379 0.0021 0.3411

1013341771

0.1717 0.2578 0.9562 0.0165 0.0047 0.0470 0.0196 0.0157 0.0256 0.0018 0.0035 0.0016 0.0031 0.0001 0.0055 0.0353 0.0025 0.3438

1013341794

0.1730 0.2553 0.9629 0.0134 0.0057 0.0316 0.0178 0.0211 0.0324 0.0019 0.0036 0.0018 0.0028 0.0001 0.0064 0.0380 0.0021 0.3435

Chemical test results

Product analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
Lot No. 172811 AD 01 1 Standard Heat No. 1013341794																	
0.1778	0.2491	0.9613	0.0120	0.0067	0.0302	0.0189	0.0218	0.0303	0.0025	0.0034	0.0039	0.0024	0.0003	0.0000	0.0401	0.0000	0.3482

Lot No. 172811 AD 01 2 Standard Heat No. 1013341794

0.1760 0.2446 0.9541 0.0119 0.0071 0.0301 0.0189 0.0216 0.0297 0.0023 0.0036 0.0038 0.0020 0.0003 0.0000 0.0380 0.0000 0.3452

Lot No. 172812 AD 01 1 Standard Heat No. 1013341771

0.1689 0.2242 0.9400 0.0127 0.0040 0.0334 0.0224 0.0141 0.0207 0.0017 0.0034 0.0025 0.0011 0.0003 0.0000 0.0292 0.0000 0.3359

Lot No. 172812 AD 01 2 Standard Heat No. 1013341771

0.1683 0.2566 0.9448 0.0144 0.0041 0.0354 0.0217 0.0157 0.0242 0.0023 0.0041 0.0040 0.0022 0.0003 0.0000 0.0347 0.0000 0.3370

Lot No. 172813 AD 01 1 Standard Heat No. 1013341444

0.1777 0.2566 0.9527 0.0148 0.0045 0.0374 0.0195 0.0202 0.0232 0.0024 0.0058 0.0039 0.0016 0.0003 0.0000 0.0361 0.0000 0.3486

Lot No. 172813 AD 01 2 Standard Heat No. 1013341444

0.1777 0.2561 0.9601 0.0155 0.0039 0.0376 0.0189 0.0205 0.0224 0.0024 0.0058 0.0037 0.0015 0.0003 0.0000 0.0372 0.0000 0.3498

Kindberg, 26.04.2013

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No. 88776

AFC-140

PPJ  
Q.C.  
P.W.

3/6/15

voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department

SCHNEIDER  
Kundenbeauftragter  
authorized inspection representative  
représentant autorisé au contrôle

voestalpine

ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

Chemical test results

Product analysis

Lot No. 172814 AD 01 1 Standard Heat No. 1013341445

0.1758 0.2295 0.9018 0.0133 0.0034 0.0347 0.0198 0.0192 0.0202 0.0019 0.0051 0.0025 0.0008 0.0004 0.0000 0.0322 0.0000 0.3372

Lot No. 172814 AD 01 2 Standard Heat No. 1013341445

0.1744 0.2326 0.9137 0.0139 0.0035 0.0351 0.0199 0.0204 0.0206 0.0019 0.0051 0.0026 0.0009 0.0004 0.0000 0.0339 0.0000 0.3379

AFC-140

PPI

Q.C.

F.W.

3/6/15

Kindberg, 26.04.2013

Page 5 of 5.

No. 88776

voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department

**SCHNEIDLER**

Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

**voestalpine**

ONE STEP AHEAD.

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

C PIPE NOZZLE



Vallourec Fittings

B.P 10132 59002 MAUBERGE FRANCE

Tél : 03.27.69.11.01

Raccords à Souder  
Bull Welding Fittings  
Schweißformstücke

60.00017

Client :  
Consigneur  
Destinataire

VALLOUREC USA CORPORATION  
4424 Woot Sam Houston Parkway North  
Suite 150  
Richto Units

INSPECTION CERTIFICATE  
EN 10204 3.1

N° de Cde Usine  
M/B Ref 1500241 004  
Works-Nr 1502011  
N° Certificat  
Certificato Nr  
Zougais Nr 15-08023

Cde Client N° : SAP 21003986 - PO 107477000  
Your Order Nr  
Bestell-Nr

Specifications :  
Specifications :  
Spezifikationen :

Acier et Normes WPB ASTM A234 (2014) ASTM A860 (2014) PED 97/23/EC Annex 1 par.4.3 + 7.6  
Steel and Standard ASME SA234 SH PART A (2013) Certificate No : 01 202 F/Q-02 0035  
Werkstoff und Norm ASME B16-9 (2012) ASME B16-25 (2012) ASME SA 234 Section II - Part D - Table Y1 (2013)  
NACE MR0175 / ISO 15166 (2009) NACE MR0103 (2012)

Matière de départ Tubes sans soudure / Seamless Tube / Nahtlose Rohre VALLOUREC TUBES FRANCE - Saint Souve  
Raw Material / Werkstoff Acier protégé Oxygène / Oxygen Steel / Sauerstoff Stahl Acier calé / Killed Steel / beruhigter Stahl

Etat de livraison Formés à chaud entre / Hot formed between / Warmverformt / 780° C - 800° C  
Delivery Condition / Lieferzustand

Marquage Sur pièces en creux low stress V° 4" STD WPB FRANCE LW14  
Marking / Stempelung Low stress hand stamp Keinezeichnung auf dem Fitting durch Leichter Einprägung

Poste N° Item Nr Pos Nr	Nombre Number Stückzahl	N° Certificat Matière Raw Material Rohrzeug Nr	Code Marking Markierung	Goulo N° Heat Nr Schmelze	Dimensions / Sizes / Abmessungen
004	1000	5074Sv15	LW14	337131	90° LONG RADIUS ELBOW 4" STD

**CARACTERISTIQUES CHIMIQUES - CHEMICAL ANALYSIS - SCHMELZENANALYSE** Sur Goulo  
On pipe analysis

Goulo N° Heat Nr Schmelze	C	Si	Mn	P	S	Cr	Mo	Ni	Cu	V	Al	Sn	Ti	Nb	B
337131	0,300 0,160	0,100 0,20	0,200 0,80	0,050 0,011	0,050 0,001	0,400 0,07	0,160 0,02	0,400 0,05	0,400 0,03	0,080 0,001		0,003	0,004	0,001	

Carbone équivalent / Carbon equivalent / Kohlenstoffäquivalent (Max : 0,41)

$$C_F : C + \frac{Mn}{6} = 0,310$$

$$L_F : C + \frac{Mn}{6} + \frac{Cr + V + Mo}{5} + \frac{Cu + Ni}{15} = 0,334$$

**CARACTERISTIQUES MECANIQUEES - MECHANICAL PROPERTIES - MECHANISCHE EIGENSCHAFTEN** Sur Matière de départ  
Raw Material  
vom Vorwerkstoff

Essais de Traction / Tensile Tests / Zugversuch (longitudinal direction)

Limite Elastique Yield Point / Streckgrenze Re ≥ 240 MPa	Résistance Rupture Tensile strength / Zugfestigkeit 416 ≤ Rm ≤ 670 MPa	Allongement Elongation / Dehnung ≥ 30	Dureté Hardness test on fittings H120 H90
321 MPa	460 MPa	39,8 %	140 144

Résilience / Impact Test / Kerbschlagarbeit : Sur pièces / On fittings / am Fittings

Essai Test Versuch	Test 1	Test 2	Test 3	Moyenne ; Unilé Mean ; Unilé Mittelwert ; Einzel	Type : KV Specimen Muster	Température Pos de résilience

Date : 07/09/2016  
LE RESPONSABLE  
QUALITE  
P. LEFEBVRE

WE CERTIFY THAT THE DELIVERED PRODUCTS WERE MANUFACTURED, SAMPLED, TESTED AND INSPECTED IN ACCORDANCE WITH THE SPECIFICATION OF THE ORDER.

4/11/17 PPI  
O.C. XAN-85  
F.W.

ISO 9001 / ISO 14001 / OHSAS 18001

**CGP MFG, INC.**  
 8363 MARKET STREET ROAD  
 HOUSTON, TX 77029  
 Phone: 713-641-5544  
 FAX: 713-641-5564

# Material Test Report

Page : 1 of 2  
 SALES ORDER #: 111650

**SOLD TO:**  
 NORTHSHORE SUPPLY  
 P.O. BOX 9940  
 HOUSTON, TX 77213

**SHIP TO:**

CUST P.O.#: 1287649-JG1 TAG NUMBER: DATE SHIPPED:

ITEM #	QUANTITY	ITEM DESCRIPTION
1	4 EA	1 X 4 6M THD CPLET PER DWG SA350-2008A LF2 CL1

ITEM #	HEAT CODE	CHEMICAL ANALYSIS											
		C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb	C.Eqv
1	LRB4	.20	1.06	.011	.025	.23	.22	.09	.19	.06	.003	.000	.45

ITEM #	PHYSICAL PROPERTIES						
	TENSILE (PSI)	YIELD (PSI)	ELONG (2 IN)	REDUCTIO N OF AREA. %	HARDNESS	CHARPY V-NOTCH	
1	73700	48400	30.00	65.00	152 BHN	CVN@-50°F	74/50/39 FT LBS

ITEM #	SUPPLEMENTAL INFORMATION
1	NORMALIZED@1670°F/ 3.5HRS AIR COOL FORGED RD EN 10204-3.1B

4/11/17 PPI  
 Q.C. XAN-86  
 E.W.

WE CERTIFY THAT THE FITTINGS COVERED BY THIS REPORT WERE MANUFACTURED PER THE SPECIFICATIONS NOTED & THAT THE PHYSICAL & CHEMICAL PROPERTIES ARE THOSE REFLECTED IN THE RECORDS OF THE COMPANY. MERCURY FREE MFG IN THE USA

JORGE GARCIA, JR. - Q.A. MGR.

04/28/2017

CGP MFG, INC.  
 8363 MARKET STREET ROAD  
 HOUSTON, TX 77029  
 Phone: 713-641-5544  
 FAX: 713-641-5564

# Material Test Report

Page : 2 of 2  
 SALES ORDER #: 111650

**SOLD TO:**  
 NORTSHORE SUPPLY  
 P.O. BOX 9940  
 HOUSTON, TX 77213

**SHIP TO:**

CUST P.O.#: 1287649-JG1 TAG NUMBER: DATE SHIPPED:

ITEM #	QUANTITY	ITEM DESCRIPTION
2	6 EA	3/4 X 4 6M THD CPLET PER DWG SA350-2008A LF2 CL1

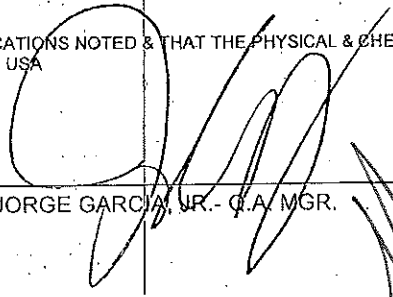
ITEM #	HEAT CODE	CHEMICAL ANALYSIS											
		C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb	C.Eqv
2	LSJ4	.20	1.10	.009	.020	.21	.17	.07	.14	.04	.002	.001	.44

ITEM #	PHYSICAL PROPERTIES						
	TENSILE (PSI)	YIELD (PSI)	ELONG (2 IN)	REDUCTIO N OF AREA %	HARDNESS	CHARPY V-NOTCH	
2	77200	51900	30.00	59.00	157/152 BHN CVN@-50°F	98/106/110 FT LBS	

ITEM #	SUPPLEMENTAL INFORMATION
2	NORMALIZED@1670°F/ 3.5HRS AIR COOL FORGED RD EN 10204-3.1B

4/11/17 PPI  
 Q.C. XAN-87  
 F.W.

WE CERTIFY THAT THE FITTINGS COVERED BY THIS REPORT WERE MANUFACTURED PER THE SPECIFICATIONS NOTED & THAT THE PHYSICAL & CHEMICAL PROPERTIES ARE THOSE REFLECTED IN THE RECORDS OF THE COMPANY. MERCURY FREE MFG IN THE USA

  
 JORGE GARCIA, JR. - Q.A. MGR. 04/28/2017

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429  
 E, G1, G2, G3, G4 & J



14527 Smith Rd.  
Humble, Texas 77396  
TEL: (281) 441-4088  
FAX: (281) 441-8899

PAGE: 1 of 1  
REPORT # 17-030309  
DATE: 5/1/2017  
FCI ORDER # 77823  
I.A.W. ASME 2015 ED.

CUSTOMER ORDER # 1287649-JG  
SOLD / SHIPPED TO: NORTH SHORE STEEL

Item	Quantity	Description
3	1	18" X 600 X 18" LG RF HB WITH NUT RELIEF

Heat Number: Z580  
Material Type: SA350LF2CL1

CHEMICAL ANALYSIS

PHYSICAL PROPERTIES

C	.168
Mn	1.180
P	.0050
S	.0030
Si	.220
Cr	.110
Mo	.020
V	.050
Cu	.110
Ni	.070
Cb(Nb)	.001
N	.0102
Sn	.006
As	.004
Sb	.001
Ti	.0024
Al	.027
B	.0004
C E	.413

Yield PSI	54,000
Tensile PSI	79,200
Elongation	33.9
Reduction of Area	73.1
Hardness	154/156 HBW
CVN -50 °F	FT LBS 98/102/92
	% Shear 100/100/100
	MLE .065/.076/.061

Heat Treatment: NORMALIZED  
Temperature: 1650 °F  
Time at Temperature: 1/2 HR/IN THK MIN  
Cooling Media: AIR

4/11/17 PPI  
Q.C. XAN-88  
F.W.

We hereby certify that all test results and process information contained herein are correct and true as contained in the records of the company.

Prepared by: Erika Marquez

Name: Erika Marquez Title: QA Representative





voestalpine Tubulars GmbH & Co KG

5550-8



HR046587#HT#A#1/1

Material Test Report (MTR)

FSVAT 1.5 STD

INSPECTION - CERTIFICATE 3.1

(according to EN 10204)

ABNAHMEPRUEFZEUGNIS 3.1

(gem. EN 10204)

CERTIFICAT DE CONTROLE DES PRODUITS PAR L'USINE 3.1

(selon EN 10204)

Hersteller: voestalpine Tubulars GmbH & Co KG, Austria  
 Manufacturer: voestalpine Tubulars GmbH & Co KG, Austria  
 Producteur: voestalpine Tubulars GmbH & Co KG, Austria

Besteller: VOEST-ALPINE TUBULAR CORPORATION  
 Purchaser: USA-77042 HOUSTON TEXAS  
 Archaieur: INDUSTRIAL PIPING SPEC. INC., TULSA OK 74158-1270

Pruefgegenstand: SEAMLESS STEEL TUBES, LINE PIPE  
 Object of tests: SEAMLESS STEEL TUBES, LINE PIPE  
 Epreuve: SEAMLESS STEEL TUBES, LINE PIPE

Werkstoff: GRADE B / GRADE C  
 Material: LP-USA-01  
 Matières: GRADE B / GRADE C LP-USA-01

Anforderungen: ASTM A 53 A 53 / A 53 M - ASME SA 53-2012  
 Requirements: ASTM A106 / A 106 M - ASME SA 106-2011  
 Exigence: (ASME Sec II Part A 1.Jull 2010)  
 API 5L, PSL 1 -2007 and  
 NACE MR 0175 / ISO 15156-2009  
 NACE MR0103-2010 (latest edition)  
 LINEPIPE-01.0

Ausführung: NU, PLAIN END, PE,  
 Condition: NU, PLAIN END, PE,  
 Cond. de livraison: NU, PLAIN END, PE,  
 Wärmebehandlung: AS ROLLED  
 Heat treatment: AS ROLLED  
 Traitement de chaleur: AS ROLLED  
 Coupl.die stamped:  
 Coupl.painl stencilling:  
 Colour coding: Fully painted: Bands:  
 Tube die stamped:  
 Tube paint stencilling: va SPEC 5L-0033 "API" 09.2013 1,900" 0.145" B PSL1 SMLS TESTED 2500PSI length ft heat no A/SA 53 GRADE B S A/SA 106 GRADE B SCHED.40 PO No.: HR046587 Made in Austria

Colour coding: Fully painted: Bands: purple  
 Label: PO No.: HR046587 DAT Port of Houston, TX  
 Remarks: \*) Grade C without marking on tubes

Alpinestrasse 17  
8652 Kindberg-Aumuhl  
T. +43/3866/22 15-0  
F. +43/3866/2215-532  
www.vetubulars.com

Legal Structure: Limited Partnership  
Location: Kindberg/Austria  
Company Registry Number 165400k  
Commercial Court of Leoben  
DPR 0592684, VAT Nr. ATU 43630406

General Partner: voestalpine Tubulars GmbH  
Legal Structure: Limited Liability Company  
Location: Linz, Company Registry Number 106933f  
Commercial Court of Linz

No. 92433

Auftrags-Nr.: 14227 / 2  
Our works order No.:  
No usine:

Bestellnr.: HR046587/VATC  
Your order No.: PO#307610

No de la commande:

Zeichen des Lieferwerks: va  
Marking of producer:  
Marque du fabricant:

Erschmelzungsart: BOF  
Melting process: fully killed, produced to  
Procédé d'elaboration: fine grain practice

5/12/15 PPI Q.C. F,W, AFB-37

Kindberg, 30.09.2013

Page 1 of 4

No. 92433

voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle Quality Department  
SIGNED/HTER  
Annahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

5550-8

Umfang der Lieferung / Volume of delivery / Contenu de la livraison:

Versandanzeige: Dispatch advice No. Avls d'expédition:	Pos.: Pos.:	Abmessung: Dimension: Dimension:	Bundnr.: Bundle No.: Nombre Fret:	Stückzahl: Number Of: Pièces:	Länge: Length: Longueur:	Gewicht: Weight: Poids:	Los: Lot: Lot:	Schmelze: Heat: Soufflage:
	2	1,900 In x 0,145 In 2,72 lbs/ft	1-8	900	21 112.205ft	26 140.00kg		

Volume of delivery

Heat	Lot	Remark
1013347382	177538	-- 01
1013347381	177537	-- 01

Test results

- 1 Biegeversuch/Bend test: o.B./satisfactory
- 2 Dimensionskontrolle/ Dimensional inspection: o.B./satisfactory
- 3 Streifflussprüfung gem. ASTM E 570 / Flux leakage testing acc. ASTM E 570 (N 12,5 longitudinal, type and size of reference indicator used); o.B./satisfactory
- 4 Visuelle Inspektion/ Visual inspection: o.B./satisfactory
- 5 Wasserinnendruckversuch/Hydrostatic test: 2500 PSI (duration min 5.sec) o.B./satisfactory

Test remarks

S/12/15 PPI  
Q.C.  
F.W. AFB-37

Wir bestätigen, dass die gelieferten Erzeugnisse den Anforderungen der Bestellung entsprechen.  
We hereby certify that the goods delivered are in compliance with the requirements of the order.

Kindberg, 30.09.2013

Page 2 of 4

No. 92433

voestalpine Tubulars GmbH & Co KG  
Qualitätssystem / Quality Department  
SCHWEIDRÜCKER  
Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD.

SKIRT VENT

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429



voestalpine Tubulars GmbH & Co KG

5550-8

Tensile testing

Lot No	Test Type	Heat treatment	Temp [°C]	Specimen		Yield Strength [ PSI ]	Tensile Strength [ PSI ]	Elong. in area [%]	Reduct. of Area [%]	R <sub>m</sub> /R <sub>e</sub>		
				No.	Type						Dimension [mm]	
						Requ. from	35 534	60 190	20.00			
						Requ. to						
177537	AD 01	Standard	as rolled	20	1	Strip	18.84 x 3.62	R10.50	67 877	85 427	32.00	0.79
177537	AD 01	Standard	as rolled	20	2	Strip	18.81 x 3.82	R10.50	63 671	80 786	29.40	0.79
177538	AD 01	Standard	as rolled	20	1	Strip	18.83 x 3.70	R10.50	65 557	84 121	30.90	0.78

yield strength:  
Grade B : 35500 PSI  
Grade C: 40000 PSI

tensile strength:  
Grade B: 60200 PSI  
Grade C: 70000 PSI

Hardness testing

Lot No	Test Type	Heat treatment	Specimen		Hardness Number from	to	Mean Hardness Number		Variation		
			No.	Location			Test Method	from		to	
					Requ.:		99.50				
177537	AC 01	Standard	as rolled	1	Body	HRB	85.10	86.20	85.27	86.03	0.77
177538	AC 01	Standard	as rolled	1	Body	HRB	86.70	88.20	87.07	87.60	0.53

S/12/15

PPI  
Q.C.  
F.W.

AFB-37

Kindberg, 30.09.2013

Page 3 of 4

No. 92433

voestalpine Tubulars GmbH & Co KG  
Qualitätsreferat / Quality Department  
**SCHNEIDHOFER**  
Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

**voestalpine**

ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

5550-8

Chemical test results

Heat analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
max																	
0.2300		1.0600	0.0300	0.0300	0.4000	0.4000	0.4000			0.1500	0.0800						0.4000

min

0.0000 0.1000 0.2900

1013347381

0.1736 0.2608 0.9482 0.0141 0.0082 0.0664 0.0198 0.0191 0.0272 0.0018 0.0068 0.0016 0.0009 0.0002 0.0077 0.0447 0.0016 0.3492

1013347382

0.1785 0.2696 0.8853 0.0151 0.0076 0.0324 0.0197 0.0160 0.0344 0.0017 0.0147 0.0013 0.0006 0.0001 0.0048 0.0448 0.0016 0.3514

5/12/15 PPI  
Q.C. AFB-37  
F.W.

Chemical test results

Product analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
Lot No. 177537 AD 01 1 Standard Heat No. 1013347381																	
0.1800	0.2503	0.9505	0.0149	0.0067	0.0649	0.0205	0.0181	0.0218	0.0020	0.0072	0.0040	0.0017	0.0005	0.0000	0.0401	0.0000	0.3562

Lot No. 177537 AD 01 2 Standard Heat No. 1013347381

0.1848 0.2513 0.9529 0.0148 0.0076 0.0649 0.0205 0.0183 0.0216 0.0021 0.0075 0.0040 0.0018 0.0005 0.0000 0.0410 0.0000 0.3615

Lot No. 177537 AD 01 3 Standard Heat No. 1013347381

0.1808 0.2624 0.9648 0.0149 0.0076 0.0653 0.0198 0.0190 0.0234 0.0023 0.0075 0.0045 0.0023 0.0005 0.0000 0.0432 0.0000 0.3596

Lot No. 177537 AD 01 4 Standard Heat No. 1013347381

0.1784 0.2586 0.9616 0.0146 0.0067 0.0649 0.0197 0.0190 0.0236 0.0022 0.0073 0.0044 0.0022 0.0005 0.0000 0.0413 0.0000 0.3566

Lot No. 177538 AD 01 1 Standard Heat No. 1013347382

0.1880 0.2735 0.9744 0.0153 0.0079 0.0348 0.0200 0.0171 0.0307 0.0023 0.0163 0.0045 0.0014 0.0005 0.0000 0.0438 0.0000 0.3640

Lot No. 177538 AD 01 2 Standard Heat No. 1013347382

0.1824 0.2672 0.9633 0.0149 0.0089 0.0342 0.0196 0.0165 0.0301 0.0022 0.0161 0.0043 0.0013 0.0004 0.0000 0.0418 0.0000 0.3563

Kindberg, 30.09.2013

Page 4 of 4

No. 92433

voestalpine Tubulars GmbH & Co KG  
Qualitätsbereich / Quality Department  
**SCHNEIDHOPFER**  
Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD.



voestalpine Tubulars GmbH & Co KG

Alpinestrasse 17  
8552 Kindberg-Aumuehl  
T. +43/3865/22 15-0  
F. +43/3865/2215-532  
www.voestalpine.com

Legal Structure: Limited Partnership  
Location: Kindberg/Austria  
Company Registry Number 165400k  
Commercial Court of Leoben  
DPR 0592684, VAT Nr. ATU 43630406

General Partner: voestalpine Tubulars GmbH  
Legal Structure: Limited Liability Company  
Location: Linz, Company Registry Number 100933f  
Commercial Court of Linz

FSVAT1XH

MILL TEST CERTIFICATE 3.1

(according to EN 10204)

ABNAHMEPRUEFZEUGNIS 3.1

(gem. EN 10204)

No. 122697 Rev. 0

CERTIFICAT DE CONTROLE DES PRODUITS PAR L'USINE 3.1

(selon EN 10204)

Hersteller: voestalpine Tubulars GmbH & Co KG, Austria  
Manufacturer:  
Producteur:

Besteller: VOEST-ALPINE TUBULAR CORPORATION  
Purchaser: USA-77077 HOUSTON, TEXAS  
Archeteur: INDUSTRIAL PIPING SPECIALISTS, INC. TULSA OK 74158-1270, US

Pruefgegenstand: Line Pipe  
Object of tests: LP-USA-01  
Epreuve: LINEPIPE-01.0  
non upset ends (API 5 D + 5 L) - non upset  
UV coating

Werkstoff: GRADE B  
Material:  
Matières:

Anforderungen: Grade B acc. to ASTM A 53 / A 53M-2012  
Requirements: ASME SA 53-2015  
Exigence: Grade B acc. to ASTM A 106 / A 106M-2015, ASME SA 106-2015  
Grade B acc. to API 5 L, 45, edL-2012 (PSL1)  
NACE MR 0175 / ISO 15156-2015  
NACE MR 0103-2015  
LINEPIPE-01.0; LP-USA-01

Ausführung: NU, PLAIN END, PE,  
Condition:  
Cond. de livraison:

Wärmebehandlung: AS ROLLED  
Heat treatment:  
Traitement de chaleur:

Coupl. die stamped:  
Coupl. paint stencilling:

Colour coding: Fully painted; Bands:

Tube die stamped:  
Tube paint stencilling:

va SPEC 5L-0033 "API" 07.2016 1.315" 0.179" B PSL1 SMLS TESTED 2500 PSI Length ft Heat No. A/SA 53 GRADE B S A/SA 106 GRADE B SCHED.80 PO No.: HR068855 Made in Austria

Colour coding: Fully painted; Bands: purple

Label: PO No.: HR068855; DAT Port of Houston TX

Remarks: \*) SI units have been converted to US customary units

Auftrags-Nr.: 21600 / 1  
Our works order No.:  
No usine:

Bestellnr.: HR068855/VATC PO#  
Your order No.: 605620

No de la commande:

Zeichen des Lieferwerks: va  
Marking of producer:  
Marque du fabricant:

Erschmelzungsart: BOF  
Melting process: fully killed, produced to  
Procédé d'élaboration: fine grain practice

12/8/16

PPI  
Q.C.  
F,W,

AFI-61

Kindberg, 28.09.2016

Page 1 of 4

No. 122697

Abnahmeprüfzeugnis wurde digital signiert und ist ohne Originalunterschrift gültig/  
Inspection certificate has been signed digitally and is valid without an original signature

voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department  
WEITZER

Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD.

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

INLET DIV. PIPE



**voestalpine Tubulars GmbH & Co KG**

**Umfang der Lieferung / Volume of delivery / Contenu de la livraison:**

Versandanzeige: Dispatch advice No. Avis d'expédition:	Pos.: Pos.:	Abmessung: Dimension: Dimension:	Bundnr.: Bundle No.: Nombre Fret:	Stückzahl: Number Of: Pièces:	Länge: Length: Longueur:	Gewicht: Weight: Poids:	Los: Lot: Lot:	Schmelze: Heat Soufflage:
	1	1,315 in x 0,179 in; 2,17 lbs/ft SCHED.80	1-8	1028	23 469.488ft	23 077.50kg		

**Volume of delivery**

Heat	Lot	Remark
1016486321	208595	AD 01
1016386730	209495	AD 01

**Test results**

- 1 Blegeversuch/Bend test: bestanden/passed
- 2 Dimensionskontrolle/ Dimensional inspection: bestanden/passed
- 3 Streifflussprüfung gem. ASTM E 570 / Flux leakage testing acc. ASTM E 570 (N 12,6 longitudinal, type and size of reference indicator used): bestanden/passed
- 4 Visuelle Inspektion/ Visual inspection: bestanden/passed
- 5 Wasserinnendruckversuch/Hydrostatic test: bestanden/passed, Mindestprüfdruck/min test pressure: 2500 PSI, min. Haltezeit/min duration: 5 sec

**Test remarks**

Wir bestätigen, dass die gelieferten Erzeugnisse den Anforderungen der Bestellung entsprechen.  
We hereby certify that the goods delivered are in compliance with the requirements of the order.

12/8/16 PPI  
Q.C.  
F.W. AFI-61

Kindberg, 28.09.2016

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No. 122697

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ONE STEP AHEAD.

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

INLET DIV. PIPE



voestalpine Tubulars GmbH & Co KG

onsile testing

Lot No	Test Type	Heat treatment	Loc. Temp	Specimen	Yield Strength	Tensile Strength	Elong.	Gage Reduct. length	R <sub>1</sub> /R <sub>m</sub> In area		
										[°F]	No.
					Requ. from	35 534	60 190	30.00			
					Requ. to						
208685	AD01	Standard	as rolled	Rear 20 1 Full Sector	33.73 x 4.41	R10.50	44 381	67 152	45.60	2	0.66
208585	AD01	Standard	as rolled	Rear 20 2 Full Sector	33.72 x 4.61	R10.50	42 641	64 686	42.10	2	0.66
208585	AD01	Standard	as rolled	Rear 20 3 Full Sector	33.70 x 4.70	R10.50	43 801	64 106	47.10	2	0.68
209496	AD01	Standard	as rolled	Rear 20 1 Full Sector	33.40 x 4.55	R10.50	46 847	67 792	45.40	2	0.69
209496	AD01	Standard	as rolled	Rear 20 2 Full Sector	33.40 x 4.55	R10.50	46 122	67 442	44.10	2	0.68

Hardness testing

Lot No	Test Type	Heat treatment	Specimen	Test	Hardness Number	Mean Hardness Number		Variation					
						Loc. No.	Location		Method	from	to	from	to
					Requ.:			99.50					
208585	AD01	Standard	as rolled	Rear 1 Body	HRB	76.50	77.20	76.80	77.00	0.20			
Quadrant	1_Outer	2_Outer	3_Outer	AVG_Outer	1_Mid	2_Mid	3_Mid	AVG_Mid	1_Inner	2_Inner	3_Inner	AVG_Inner	AVG_Variation
1	76.80	77.20	75.90	76.97	76.90	76.50	77.00	76.80	77.00	76.80	77.20	77.00	0.20
209496	AD01	Standard	as rolled	Rear 1 Body	HRB	77.50	78.90	77.80	78.37	0.57			
Quadrant	1_Outer	2_Outer	3_Outer	AVG_Outer	1_Mid	2_Mid	3_Mid	AVG_Mid	1_Inner	2_Inner	3_Inner	AVG_Inner	AVG_Variation
1	77.90	78.00	77.50	77.80	78.30	78.90	77.90	78.37	78.50	78.40	77.80	78.23	0.57

12/8/16

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AFI-61

Kindberg, 28.09.2016

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No. 122697

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voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department  
WEITZER

Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

voestalpine

ONE STEP AHEAD



### voestalpine Tubulars GmbH & Co KG

#### Chemical test results

##### Heat analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
min. Requ.																	
0.0000	0.1000	0.2900															
max. Requ.																	
0.2300	1.0500	0.0300	0.0300	0.4000	0.4000	0.4000				0.1500	0.0800						0.4000
1016386730																	
0.1451	0.2149	0.7135	0.0096	0.0055	0.0162	0.0148	0.0153	0.0313	0.0011	0.0016	0.0013	0.0004	0.0001	0.0055	0.0000	0.0024	0.2698
1016486321																	
0.1487	0.1993	0.6943	0.0127	0.0070	0.0143	0.0170	0.0164	0.0232	0.0014	0.0028	0.0010	0.0005	0.0002	0.0048	0.0000	0.0016	0.2703

#### Chemical test results

##### Product analysis

C	Si	Mn	P	S	Cr	Ni	Cu	Al	Ti	Mo	V	Sn	B	N2	Nb	Ca	CEQ
Lot No. 208585 AD 01 1 Standard Heat No. 1016486321																	
0.1707	0.1979	0.6803	0.0138	0.0064	0.0153	0.0190	0.0193	0.0192	0.0020	0.0028	0.0030	0.0015	0.0002	0.0050	0.0009	0.0000	0.2909
Lot No. 208585 AD 01 2 Standard Heat No. 1016486321																	
0.1625	0.1970	0.6798	0.0134	0.0087	0.0153	0.0191	0.0195	0.0190	0.0020	0.0030	0.0029	0.0014	0.0002	0.0047	0.0010	0.0000	0.2826
Lot No. 208585 AD 01 3 Standard Heat No. 1016486321																	
0.1574	0.1995	0.6852	0.0135	0.0096	0.0155	0.0191	0.0201	0.0195	0.0021	0.0032	0.0031	0.0017	0.0002	0.0045	0.0013	0.0000	0.2786
Lot No. 208585 AD 01 4 Standard Heat No. 1016486321																	
0.1773	0.2008	0.6892	0.0138	0.0086	0.0155	0.0191	0.0201	0.0193	0.0022	0.0031	0.0031	0.0017	0.0002	0.0076	0.0012	0.0000	0.2991
Lot No. 208585 AD 01 5 Standard Heat No. 1016486321																	
0.1619	0.1983	0.6804	0.0131	0.0074	0.0164	0.0190	0.0201	0.0193	0.0020	0.0031	0.0031	0.0014	0.0002	0.0052	0.0013	0.0000	0.2722
Lot No. 208585 AD 01 6 Standard Heat No. 1016486321																	
0.1566	0.1973	0.6831	0.0136	0.0093	0.0153	0.0190	0.0194	0.0189	0.0019	0.0030	0.0029	0.0015	0.0002	0.0047	0.0011	0.0000	0.2773
Lot No. 209495 AD 01 1 Standard Heat No. 1016386730																	
0.1661	0.2184	0.6942	0.0094	0.0063	0.0182	0.0165	0.0175	0.0270	0.0019	0.0028	0.0037	0.0015	0.0002	0.0099	0.0010	0.0000	0.2890
Lot No. 209495 AD 01 2 Standard Heat No. 1016386730																	
0.1537	0.2210	0.7016	0.0110	0.0069	0.0185	0.0168	0.0187	0.0269	0.0019	0.0031	0.0038	0.0019	0.0002	0.0080	0.0012	0.0000	0.2781
Lot No. 209495 AD 01 3 Standard Heat No. 1016386730																	
0.1539	0.2188	0.7021	0.0103	0.0063	0.0184	0.0167	0.0182	0.0269	0.0019	0.0029	0.0038	0.0019	0.0002	0.0077	0.0012	0.0000	0.2783
Lot No. 209495 AD 01 4 Standard Heat No. 1016386730																	
0.1509	0.2181	0.7014	0.0105	0.0069	0.0185	0.0168	0.0188	0.0265	0.0018	0.0031	0.0037	0.0019	0.0002	0.0076	0.0012	0.0000	0.2752

12/8/16

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Kindberg, 28.09.2016

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No. 122697

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voestalpine Tubulars GmbH & Co KG  
Qualitätsstelle / Quality Department  
WEITZER

Abnahmebeauftragter  
authorized inspection representative  
représentant autorisé du contrôle

**voestalpine**

ONE STEP AHEAD.

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

INLET DIV. PIPE



NUCOR STEEL TUSCALOOSA, INC.

MILL TEST CERTIFICATE

1700 HOLT RD N.E.  
Tuscaloosa, AL 35404-1000  
800-827-8872

AAA FLAME CUT STEEL, INC. Page #1 of 6  
THK 1/4" GR: A-36 Mod  
HT & SL A3R1772-03  
PLATE # 2308

Load Number	Tally	Mill Order Number	PO NO   Line NO	Part Number	Certificate Number	Prepared
B032740	0000000503272	N-121202-004	11719 4		L419952-1	05/23/2013 19:40
Grade						

Shipped Item	Heat/Slab Number	Certified By	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Cb	V	Al	Ti	N2	B	Ca	Sn	CEV
Customer: (2) B16																				
Order Description: A36, 0.2500 IN x 96.000 IN x 240.000 IN PPI																				
Quality Plan Description: YAK-21 Q.C.																				
A36MODMN20C: ASTM A36-05/A36M/ASME SA36-00 MOD MN 20 MAX C F.W.																				
3E2079C	A3R1772-01 ***	A3R1772	0.18	0.85	0.011	0.003	0.05	0.26	0.08	0.07	0.026	0.000	0.001	0.033	0.001	0.007	0.0001	0.0018	0.009	0.37
3E2079D	A3R1772-01 ***	A3R1772	0.18	0.85	0.011	0.003	0.05	0.26	0.08	0.07	0.026	0.000	0.001	0.033	0.001	0.007	0.0001	0.0018	0.009	0.37
3E2081C	A3R1772-03 ***	A3R1772	0.18	0.85	0.011	0.003	0.05	0.26	0.08	0.07	0.026	0.000	0.001	0.033	0.001	0.007	0.0001	0.0018	0.009	0.37
3E2081D	A3R1772-03 ***	A3R1772	0.18	0.85	0.011	0.003	0.05	0.26	0.08	0.07	0.026	0.000	0.001	0.033	0.001	0.007	0.0001	0.0018	0.009	0.37
3E2083C	B3R6682-01 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2083D	B3R6682-01 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2085C	B3R6682-03 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2085D	B3R6682-03 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2086C	B3R6682-02 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2086D	B3R6682-02 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2087C	B3R6682-04 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2087D	B3R6682-04 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2088C	B3R6682-05 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2088D	B3R6682-05 ***	B3R6682	0.19	0.87	0.012	0.005	0.04	0.25	0.07	0.07	0.020	0.000	0.002	0.036	0.001	0.006	0.0000	0.0022	0.008	0.37
3E2089C	A3R1773-02 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2089D	A3R1773-02 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2090C	A3R1773-01 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2090D	A3R1773-01 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2092C	A3R1773-03 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2092D	A3R1773-03 ***	A3R1773	0.19	0.84	0.014	0.005	0.06	0.26	0.08	0.08	0.025	0.000	0.001	0.037	0.001	0.008	0.0001	0.0018	0.008	0.37
3E2093C	B3R6683-02 ***	B3R6683	0.19	0.87	0.012	0.004	0.06	0.30	0.08	0.07	0.031	0.000	0.002	0.035	0.001	0.008	0.0001	0.0020	0.009	0.38

Mercury has not come in contact with this product during the manufacturing process not has any mercury been used by the manufacturing process. Certified in accordance with EN 10204 3.1. No weld repair has been performed on this material. Manufactured in a fully killed fine grain practice. NUTEMPER TEMPER PASSED plate from coil ISO 9001:2008 Registered, PED Certified

We hereby certify that the product described above passed all of the tests required by the specifications.

Dr. Chulin Yu - Jveitdrgist

\*\*\* Indicates Heats melted and Manufactured in the U.S.A.

GROUNDING LUG

1700 HOLT RD N.E.  
 Tuscaloosa, AL 35404-1000  
 800-827-8872

Load Number	Tally	Mill Order Number	PO NO   Line NO	Part Number	Certificate Number	Prepared														
B032740	0000000503272	N-121202-004	11719   4		L419952-1	05/23/2013 19:40														
Grade	Customer:																			
Order Description:	YAK-21 12/8/16																			
A36, 0.2500 IN x 96.000 IN x 240.000 IN	PPI																			
Quality Plan Description:	Q.C.																			
A36MODMN2DC: ASTM A36-05/A36M/ASME SA36-00 MOD MN .20 MAX C	F.W.																			
Shipped Item	Heat/Slab Number	Certified By	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Cb	V	Al	Ti	N2	B	Ca	Sn	CEV
3E2093D	B3R6683-02 ***	B3R6683	0.19	0.87	0.012	0.004	0.06	0.30	0.08	0.07	0.031	0.000	0.002	0.035	0.001	0.008	0.0001	0.0020	0.009	0.38

Mercury has not come in contact with this product during the manufacturing process nor has any mercury been used by the manufacturing process. Certified in accordance with EN 10204 3.1. No weld repair has been performed on this material. Manufactured to a fully killed fine grain practice. NUTEMPER TEMPER PASSED plate from coil ISO 9001:2008 Registered, PED Certified

We hereby certify that the product described above passed all of the tests required by the specifications.

*Quilin Yu*  
 Qi: Quilin Yu - Metallurgist

\*\*\* indicates heats melted and Manufactured in the U.S.A.



**MILL TEST CERTIFICATE**

1700 HOLT RD N.E.  
 Tuscaloosa, AL 35404-1000  
 800-827-8872

Load Number	Tally	Mill Order Number	PO NO   Line NO	Part Number	Certificate Number	Prepared
8032740	0000000503272	N-121202-004	11719 4		L419952-1	05/23/2013 19:40
Grade	Customer:					

Order Description:  
 A36, 0.2500 IN X 96.000 IN X 240.000 IN  
 Quality Plan Description:  
 A36MODM20C: ASTM A36-03/A36M/ASME SA36-00 MOD MN .20 MAX C

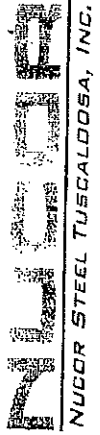
YAK-Z1  
 PPI Q.C.  
 F.W. 12/8/16

Shipped Item	Certified By	Heat/Slab Number	Yield ksi	Tensile ksi	Y/T %	ELONGATION %		Bend OK?	Hard HB	Charpy Impacts (ft-lbs)			Test Temp
						2" 8"	8"			Size mm	1	2	
3E2085C	S3E2085MTT	B3R6682-03 ***	51.3	69.3	74.0	30.9							
3E2085D	S3E2085FTT	B3R6682-03 ***	57.3	75.0	76.4	28.5							
3E2085D	S3E2085MTT	B3R6682-03 ***	51.3	69.3	74.0	30.9							
3E2086C	S3E2083FTT	B3R6682-02 ***	52.5	75.1	69.9	31.5	20.5						
3E2086C	S3E2085FTT	B3R6682-02 ***	57.3	75.0	76.4	28.5							
3E2086C	S3E2083MTT	B3R6682-02 ***	51.3	69.8	73.5	30.9							
3E2086C	S3E2085MTT	B3R6682-02 ***	51.3	69.3	74.0	30.9							
3E2086D	S3E2083FTT	B3R6682-02 ***	52.5	75.1	69.9	31.5	20.5						
3E2086D	S3E2085FTT	B3R6682-02 ***	57.3	75.0	76.4	28.5							
3E2086D	S3E2083MTT	B3R6682-02 ***	51.3	69.8	73.5	30.9							
3E2086D	S3E2085MTT	B3R6682-02 ***	51.3	69.3	74.0	30.9							
3E2087C	S3E2083FTT	B3R6682-04 ***	52.5	75.1	69.9	31.5	20.5						
3E2087C	S3E2085FTT	B3R6682-04 ***	57.3	75.0	76.4	28.5							
3E2087C	S3E2083MTT	B3R6682-04 ***	51.3	69.8	73.5	30.9							
3E2087C	S3E2085MTT	B3R6682-04 ***	51.3	69.3	74.0	30.9							
3E2087D	S3E2083FTT	B3R6682-04 ***	52.5	75.1	69.9	31.5	20.5						
3E2087D	S3E2085FTT	B3R6682-04 ***	57.3	75.0	76.4	28.5							
3E2087D	S3E2083MTT	B3R6682-04 ***	51.3	69.8	73.5	30.9							
3E2087D	S3E2085MTT	B3R6682-04 ***	51.3	69.3	74.0	30.9							
3E2088C	S3E2083FTT	B3R6682-05 ***	52.5	75.1	69.9	31.5	20.5						
3E2088C	S3E2085FTT	B3R6682-05 ***	57.3	75.0	76.4	28.5							

Mercury has not come in contact with this product during the manufacturing process not has any mercury been used by the manufacturing process. Certified in accordance with EN 10204 3.1. No weld repair has been performed on this material. Manufactured to a fully killed fine grain practice. NUTEMPER TEMPER PASSED plate from coil ISO 9001:2008 Registered. PED Certified

We hereby certify that the product described above passed all of the tests required by the specifications.

*Quilin Yu*  
 Dr. Quilin Yu - Metallurgist



**NUCOR STEEL TUSCALOOSA, INC.**  
 1700 HOLT RD N.E.  
 Tuscaloosa, AL 35404-1000  
 800-827-8872

# MILL TEST CERTIFICATE

Load Number	Tally	Mill Order Number	PO NO   Line NO	Part Number	Certificate Number	Prepared
8032740	0000000503272	N-121202-004	11719   4		L419952-1	05/23/2013 19:40
Grade	Customer:					

Shipped Item	Certified By	Heat/Slab Number	Yield ksi	Tensile ksi	Y/T %	ELONGATION %		Bend OK?	Hard HB	Charpy Impacts (ft-lbs)			Test Temp
						2"	8"			Size mm	1	2	
3E2088C	S3E2089MTT	B3R6682-05 ***	51.3	69.8	73.5	30.9							
3E2088C	S3E2085MTT	B3R6682-05 ***	51.3	69.3	74.0	30.9							
3E2088D	S3E2083FTT	B3R6682-05 ***	52.5	75.1	69.9	31.5	20.5						
3E2088D	S3E2085FTT	B3R6682-05 ***	57.3	75.0	76.4	28.5							
3E2088D	S3E2083MTT	B3R6682-05 ***	51.3	69.8	73.5	30.9							
3E2088D	S3E2085MTT	B3R6682-05 ***	51.3	69.3	74.0	30.9							
3E2089C	S3E2089FTT	A3R1773-02 ***	55.1	73.7	74.8	30.4							
3E2089C	S3E2089MTT	A3R1773-02 ***	52.5	72.2	72.7	28.1							
3E2089D	S3E2089FTT	A3R1773-02 ***	55.1	73.7	74.8	30.4							
3E2089D	S3E2089MTT	A3R1773-02 ***	52.5	72.2	72.7	28.1							
3E2090C	S3E2090FTT	A3R1773-01 ***	60.4	80.0	75.5	31.2							
3E2090C	S3E2090MTT	A3R1773-01 ***	51.2	70.2	72.9	29.3							
3E2090D	S3E2090FTT	A3R1773-01 ***	60.4	80.0	75.5	31.2							
3E2090D	S3E2090MTT	A3R1773-01 ***	51.2	70.2	72.9	29.3							
3E2092C	S3E2089FTT	A3R1773-03 ***	55.1	73.7	74.8	30.4							
3E2092C	S3E2090FTT	A3R1773-03 ***	60.4	80.0	75.5	31.2							
3E2092C	S3E2089MTT	A3R1773-03 ***	52.5	72.2	72.7	28.1							
3E2092C	S3E2090MTT	A3R1773-03 ***	51.2	70.2	72.9	29.3							
3E2092D	S3E2089FTT	A3R1773-03 ***	55.1	73.7	74.8	30.4							
3E2092D	S3E2090FTT	A3R1773-03 ***	60.4	80.0	75.5	31.2							
3E2092D	S3E2089MTT	A3R1773-03 ***	52.5	72.2	72.7	28.1							

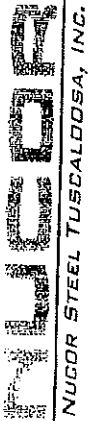
YAK-ZI  
 PPT  
 Q.C. 12/8/16  
 F.W.

Mercury has not been in contact with this product during the manufacturing process not has any mercury been used by the manufacturing process. Certified in accordance with EN 10204 3.1. No weld repair has been performed on this material. Manufactured to a fully killed fine grain practice. NUTEMPER TEMPER PASSED plate from coil ISO 9001:2008 Registered, PED Certified

We hereby certify that the product described above passed all of the tests required by the specifications.

*Dr. Qulin Yu*  
 Dr. Qulin Yu - Metallurgist

\*\*\* indicates Heats melted and Manufactured in the U.S.A.



# MILL TEST CERTIFICATE

1700 HOLT RD N.E.  
Tuscaloosa, AL 35404-1000  
800-827-8872

Load Number	Tally	Mill Order Number	PO NO   Line NO	Part Number	Certificate Number	Prepared
B032740	00000000503272	N-121202-004	11719 4		L419952-1	05/23/2013 19:40
Grade	Customer:					

Order Description:		Customer: <b>YAK-ZI</b> PPI Q.C. 12/8/16 F.W.											
A36, 0.2500 IN x 96.000 IN x 240.000 IN													
Quality Plan Description:													
A36MODMN20C: ASTM A36-05/A36M/ASME SA36-00 MOD MN .20 MAX C													
Shipped Item	Certified By	Heat/Slab Number	Yield ksi	Tensile ksi	V/T %	ELONGATION %		Bend OK?	Hard HB	Charpy Impacts (ft-lbs)			Test Temp
						2"	8"			Size mm	1	2	
3E2092D	S3E2090MTT	A3R1773-03 ***	51.2	70.2	72.9	29.3							
3E2093C	S3E2094FTT	B3R6683-02 ***	53.5	76.9	69.6	30.3							
3E2093C	S3E2095FTT	B3R6683-02 ***	57.3	76.8	74.6	31.7							
3E2093C	S3E2094MTT	B3R6683-02 ***	51.4	71.7	71.7	28.3							
3E2093C	S3E2095MTT	B3R6683-02 ***	52.6	72.0	73.1	27.4							
3E2093D	S3E2094FTT	B3R6683-02 ***	53.5	76.9	69.6	30.3							
3E2093D	S3E2095FTT	B3R6683-02 ***	57.3	76.8	74.6	31.7							
3E2093D	S3E2094MTT	B3R6683-02 ***	51.4	71.7	71.7	28.3							
3E2093D	S3E2095MTT	B3R6683-02 ***	52.6	72.0	73.1	27.4							

Items: 22 PCS: 309 Weight: 504763 LBS

Mercury has not come in contact with this product during the manufacturing process not has any mercury been used by the manufacturing process. Certified in accordance with EN 10204 3.1. No weld repair has been performed on this material. Manufactured to a fully killed line grain practice. NUTEMPER TEMPER PASSED plate from coil ISO 9001:2008 Registered, PED Certified

We hereby certify that the product described above passed all of the tests required by the specifications.

*Quilin Yu*  
Dr. Quilin Yu - Metallurgist

\*\*\* indicates Heats melted and Manufactured in the U.S.A.



6/3/2015 6:20 PM FROM: Fax Server

TO: +18665981572

P. 5

**NUCOR**  
NUCOR CORPORATION  
NUCOR STEEL TEXAS

**Mill Certification**  
6/3/2015

MTR #: 0000103107  
8812 Hwy 79 W  
Jewett, TX 75846  
(903) 626-4461  
Fax: (903) 626-6290

Sold To: KLOECKNER METALS CORP  
500 COLONIAL CENTER PARKWAY  
SUITE 500  
ROSWELL, GA 30076-0000  
(678) 259-8817  
Fax: (678) 259-8894

Ship To: KLOECKNER METALS  
14200 ALMEDA RD  
HOUSTON, TX 77053  
(713) 433-7211

Customer P.O.	6933311	Sales Order	219534.6
Product Group	Merchant Bar Quality	Part Number	5337520024004W0
Grade	A36/A529GR50/CSA44W/50W	Lot #	JW1510108401
Size	3/8x2" Flat	Heat #	JW15101084
Product	3/8x2" Flat 20' A36/A529-50/44W/50W	B.L. Number	J1-706384
Description	A36/A529-50/44W/50W	Load Number	J1-310134
Customer Spec.		Customer Part #	MB382FLTA360240

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Roll Date: 4/23/2015 Melt Date: 4/20/2015 Qty Shipped LBS: 5,206 Qty Shipped Pcs: 102

ASTM A36/A36M-12, A709/709M-13 GR36, ASME SA36-10 Ed '11 Ad.  
ASME SA36-2010 EDITION-2011 ADDENDA  
ASTM A709/A709M-13 GR 36 [250]

C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb
0.13%	0.84%	0.011%	0.027%	0.20%	0.29%	0.15%	0.19%	0.040%	0.0340%	0.001%

Yield 1: 54,600psi

Tensile 1: 73,300psi

Elongation: 24% in 8"(% in 203.3mm)

Yield 2: 55,600psi

Tensile 2: 73,300psi

Elongation 25% in 8"(% in 203.3mm)

Specification Comments: MEETS THE REQUIREMENTS OF: ASTM A36/A36M-08, A529/A529-05 GR50(345), A709/A709M-10 GR36(250); CSA G40.21-04 GR44W(300W)&GR50W(350W); AASHTO M270/270M-10 GR36(270); ASME SA36/SA36M-10 MEETS REPORTING REQUIREMENTS OF EN10204 SEC 3.1

Comments: E-mail: websales@nstexas.com

8/3/15 PPI  
YAL-5 Q.C.  
F.W.

- All manufacturing processes of the steel, including melting, have been performed in the U.S.A.
- Mercury in any form has not been used in the production or testing of this product.
- Welding or weld repair was not performed on this material.
- This material conforms to the specifications described on this document and may not be reproduced, except in full, without written approval of Nucor Corporation.
- Results reported for ASTM E45 (Inclusion content) and ASTM E381 (Macro-etch) are provided as interpretation of ASTM procedures.

*Bhargava R Vantari*

Bhargava R Vantari  
Division Metallurgist

**ArcelorMittal Burns Harbor Plate**

US HWY 12 Burns Harbor, Indiana

QUALITY ASSURANCE  
REPORT OF TEST AND ANALYSES

SHIPMENT NO. 803-02754	DATE SHIPPED 02-13-16	CAR OR VEHICLE NO. CSS-CHGO-BNSF	BVRY 062065	PAGE 2
AMERICAN ALLOY STEEL INC PO BOX 40469 HOUSTON TX 77240-0469		AMERICAN ALLOY STEEL INC BNSF TR# 7226 MILE 66.4 LN SEG 492 6230 N HOUSTON ROSSLYN RD HOUSTON TX 77091-3410		

S E R I A L N O.	P A T N O.	H E A T N U M B E R	N O. P C S.	S I Z E A N D Q U A N T I T 				Y I E L D P O I N T	T E N S I L E S T R E N G T H	A P F R A C. E L O N G.	R E D.
				T H I C K N E S S	W I D T H O R D I A	L E N G T H	W E I G H T				

QUALITY STEEL MELTED & MANUFACTURED IN THE U. S. A.  
 PLATES - ASTM A516-06 GR 70 PVO MOD C.20 MAX, ASTM A516-06 GR 65 PVO, ASTM A516-06 GR 60 PVO, ASME SA516 GR 70 PVO 2013 EDITION, ASME SA516 GR PVO 2013 EDITION, ASME SA516 GR 60 PVO 2013 EDITION, FIRST TST AS ROLLED-ADD'L TENSION PER TST PC HEAT TREATMENT --- MILL TEST PCS NO 1650+/-25F FOR 30MIN/IN (30 MINUTES MIN), AIRCOOL --- TEST CERTS AR PREPARED IN ACCORD WITH PROCEDURES OUTLINED IN EN 10204:2004 TYPE 3 NO WELD REPAIR WAS PERFORMED ON BELOW PLATE(S)

CO# 106950 GH 354-4932E

B045362	812S34840	2	.625	120	480	20420	48300	74300	8	25
							51900	73500	8	29
(M55)MFST REF#:6										
B045363	812S34840	2	.625	120	480	20420	48300	74200	8	25
							52500	73800	8	31
(M55)MFST REF#:6										

Q-QUENCH TEMPERATURE	T-TEMPERATURE	N-NORMALIZE TEMPERATURE
----------------------	---------------	-------------------------

S E R I A L N O.	P A T N O.	H E A T N U M B E R	H A R D S H N	B E N D	T H I C K N E S S I N C H E S	T Y P E	S I Z E	D I R	T E M P E R A T U R E	C H A R P Y I M P A C T											
										E N E R G Y F T L B B			S H E A R (%)			L A T. E X P			M I L L S		
										1	2	3	1	2	3	1	2	3	1	2	3

Certified a true copy of the original, retained in our file.  
 AMERICAN ALLOY STEEL, INC.

Reviewed by:  
 JR 3/4/2016

H E A T N U M B E R	C H E M I C A L A N A L Y S I S																I S O Q U I D G R A I N S I Z E
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Ti	Al	B	Ca	H	Sn	

812S34840 .17 1.07 .012 .005 .335.261 .21 .04.008.003.002.033.0002 .003.004.004

5/31/17 PPI  
 Q.C. HBZ-76  
 F.W.

*[Signature]*

AMERICAN ALLOY  
 PLATE # 5171936

I certify that the above results are a true and correct copy of actual results contained in records maintained by ArcelorMittal Burns Harbor and are in full compliance with the requirements of the specification cited above. This test report cannot be altered and must be transmitted intact with any subsequent third party test reports, if required.

BHPLTRPT.TIF

SUPV. QUALITY ASSURANCE

D. W. ELWOOD PER WNR

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-202 COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18.115 TELGE RD CYPRESS TX 77429

SINLET DIVERTER

**ArcelorMittal Burns Harbor Plate**

US HWY 12 Burns Harbor, Indiana

SHIPMENT NO. <b>803-13212</b>		DATE SHIPPED <b>11-04-15</b>	CAR OR VEHICLE NO. <b>CSS-CHGO-BNSF</b>	CSS <b>019049</b>	PAGE <b>6</b>
AMERICAN ALLOY STEEL INC PO BOX 40469 HOUSTON TX 77240-0469			AMERICAN ALLOY STEEL INC BNSF TR# 7226 MILE 66.4 LN SZG 492 6230 N HOUSTON ROSSLYN RD HOUSTON TX 77091-3410		

SERIAL NUMBER	PAT NO.	HEAT NUMBER	NO. PCS.	SIZE AND QUANTITY			WEIGHT	YIELD POINT	TENSILE STRENGTH	AF FRAC. ELONG.	RED.
				THICKNESS	WIDTH OR DIA.	LENGTH					

QUALITY STEEL MELTED & MANUFACTURED IN THE U. S. A.

PLATES - ASTM A516-06 GR 70 PVQ MOD C.20 MAX, ASTM A516-06 GR 65 PVQ, ASTM A516-06 GR 60 PVQ, ASME SA516 GR 70 PVQ 2013 EDITION, ASME SA516 GR PVQ 2013 EDITION, ASME SA516 GR 60 PVQ 2013 EDITION, FIRST TST AS ROLLED-ADD'L TENSION PER TST PC HEAT TREATMENT --- MILL TEST PCS NO 1650+/-25F FOR 30MIN/IN (30 MINUTES MIN), AIRCOOL --- TEST CERTS AR PREPARED IN ACCORD WITH PROCEDURES OUTLINED IN EN 10204:2004 TYPE 3 N ACCORD WITH PROCEDURES OUTLINED IN EN 10204:2004 TYPE 3.1 DURES

NO WELD REPAIR WAS PERFORMED ON BELOW PLATE(S)

CO# 106119 GH 354-4859F											
A057805	821P00650	1	.875	96	480	11435	48100	73500	8	23	
							50000	72600	8	29	
(M55)MFST REF#:7											
→ A057807	821P00650	2	.875	96	480	22870	47900	74500	8	29	
							50200	71000	8	29	
(M55)MFST REF#:7											
A057808	821P00650	1	.875	96	480	11435	54000	78400	8	29	
							50500	73400	8	28	
(M55)MFST REF#:7											

Q-QUENCH TEMPERATURE	T-TEMPERATURE	N-NORMALIZE TEMPERATURE
----------------------	---------------	-------------------------

SERIAL NUMBER	PAT NO.	HEAT NUMBER	HARD BHN	BEND	THICKNESS INCHES	TYPE	SIZE	DIR	TEST TEMP °F	CHARPY IMPACT								
										ENERGY FT LBS			SHEAR(S)			LAT. EXP MILLS		

Certified a true copy of the original, retained in our file.  
AMERICAN ALLOY STEEL, INC.  
Reviewed By:  
*DR* 11/23/2015

HEAT NUMBER	CHEMICAL ANALYSIS															MILLARD GRAIN SIZE
	C	Mn	P	S	Si	Cr	Ni	Co	Mo	V	Ti	Al	B	Cu	N	

821P00650 .18 1.07 .012 .004 .323.015 .01 .12.078.004.002.033.0002 .002.004.003  
CE .40 PCM .26

5/31/17 PPI  
Q.C. HBZ-74  
F.W.

I certify that the above results are a true and correct copy of actual results contained in records maintained by ArcelorMittal Burns Harbor and are in full compliance with the requirements of the specification cited above. This test report cannot be altered and must be transmitted intact with any subsequent third party test reports, if required.

D. W. ELWOOD PER WNR

718

516720

2639

UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429

AMERICAN ALLOY PLATE # S170015

# SSAB

## Test Certificate

13609 Industrial Road, Houston, TX 77015, US

Customer: SAMUEL SPECIALTY METALS 5022 ASHLEY COURT HOUSTON TX 77041		Customer P.O. No.: 016S-7248246		Mill Order No.: 41-486172-03		Shipping Manifest: HT108155											
Product Description: ASTM A516-70(10/15)/ASME SA516-70(15) 0.43% MAX CEV (IIW); AS-ROLLED, TENSILE COUPON NORMALIZED 1650F+/-25F/1HR/"																	
Size: 0.375 X 96.00 X 240.0 (IN)																	
Tensiles				Charpy Impact Tests													
Heat Id	Piece Id	Tested Thickness	YS (KSI)	UTS (KSI)	%RA	Elong 2in	%Tst Dir										
E6K162	A10	0.372 (DISCRT)	L 54	76		25	T										
E6K162	A10*	0.372 (DISCRT)	L 50	73		26	T										
Chemical Analysis																	
Heat Id	C	Mn	P	S	SI	Tot Al	Sol Al	Cu	Ni	Cr	Mo	Ch	V	Ti	B	IIW	ORGN
E6K162	.19	1.00	.015	.001	.24	.024	.023	.23	.12	.14	.04	.001	.004	.008	.0001	.42	USA

**Tested Pieces**

**Charpy Impact Tests**

**Chemical Analysis**

**PCES: 1, LBS: 2450**

**E6K162**

**5/31/17** PPI Q.C. HBZ-75 F.W.

**4/27/17**

**Justin Ward**  
SENIOR METALLURGIST - PRODUCT

**Cost Part #: 1344107**

**WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION**

**UOP RUSSELL - P.O. # 4500754097 - S/O # 5654-1 - V-402, COLD SEPARATOR - PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429**

P10#

**NUCOR**  
NUCOR CORPORATION  
NUCOR STEEL TEXAS

**Mill Certification**  
11/6/2014

MTR #: 0000063978  
8812 Hwy 79 W  
Jewett, TX 75846  
(903) 626-4461  
Fax: (903) 626-6290

Sold To: KLOECKNER METALS CORP  
500 COLONIAL CENTER PARKWAY  
SUITE 500  
ROSWELL, GA 30076-0000  
(678) 259-8817  
Fax: (678) 259-8894

Ship To: KLOECKNER METALS  
3837 SINGLETON BLVD  
DALLAS, TX 75212  
(214) 630-6959

Customer P.O.	6861815	Sales Order	209927.7
Product Group	Merchant Bar Quality	Part Number	3000050024004W0
Grade	A36/A529GR50/CSA44W/50W	Lot #	JW1410576901
Size	1/2" (.5000) Round	Heat #	JW14105769
Product	1/2" (.5000) Round 20' A36/A529-50/44W/50W	B.L. Number	J1-687279
Description	A36/A529-50/44W/50W	Load Number	J1-290957
Customer Spec		Customer Part #	MB1/2RND360240

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Roll Date: 7/14/2014 Melt Date: 7/9/2014 Qty Shipped LBS: 5,010 Qty Shipped Pcs: 375

ASTM A36/A36M-12, A709/709M-13 GR36, ASME SA36-10 Ed '11 Ad.  
ASME SA36-2010 EDITION-2011, ADDENDA  
ASTM A709/A709M-13 GR 36 [250]

C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb
0.15%	0.86%	0.013%	0.028%	0.22%	0.25%	0.16%	0.17%	0.050%	0.0188%	0.000%

Yield 1: 62,200psi Tensile 1: 76,500psi Elongation: 23% in 8"(% in 203.3mm)  
Yield 2: 61,100psi Tensile 2: 77,200psi Elongation 23% in 8"(% in 203.3mm)

Specification Comments: MEETS THE REQUIREMENTS OF: ASTM A36/A36M-08, A529/A529-05 GR50(345), A709/A709M-10 GR36(250); CSA G40.21-04 GR44W(300W)&GR50W(350W); AASHTO M270/270M-10 GR36(270); ASME SA36/SA36M-10 MEETS REPORTING REQUIREMENTS OF EN10204 SEC 3.1

Comments: E-mail: websales@nstexas.com

- All manufacturing processes of the steel, including melting, have been performed in the U.S.A.
- Mercury in any form has not been used in the production or testing of this product.
- Welding or weld repair was not performed on this material.
- This material conforms to the specifications described on this document and may not be reproduced, except in full, without written approval of Nucor Corporation.
- Results reported for ASTM E45 (Inclusion content) and ASTM E381 (Macro-etch) are provided as interpretation of ASTM procedures.

P/C  
JW  
3/21/15  
YAK-125  
PPI  
Q.C.  
F.W.

*Bhargava R Vantari*

Bhargava R Vantari  
Division Metallurgist

UOP RUSSELL -- P.O. # 4500754097 -- S/O # 5654-1 -- V-402, COLD SEPARATOR -- PROFESSIONAL PROJECTS, INC. 18115 TELGE RD CYPRESS TX, 77429  
ISR-1A, ISR-2 & ISR-3



**METALFAR PRODOTTI INDUSTRIALI SPA**  
 23861 CESANA BRIANZA (LC) - ITALY  
 VIA G. PARINI, 28  
 PHONE + 39 031 655441 - FAX +39 031 655149  
 quality.mff@farmas.com

**COMPANY WITH  
 MANAGEMENT SYSTEM  
 CERTIFIED BY DNV**  
 = ISO 9001 =  
 = ISO 14001 =

**INSPECTION CERTIFICATE EN 10204:2004 / 3.1** Nr. 2014-C\_MFF-08170 Data / Dated 29.11.2014

**ITEX PIPING PRODUCTS LLC**  
 13411 WEST ROAD  
 77041 HOUSTON, TEXAS  
 US

Ordine / PO: I-245434/NS  
 Item: 112  
 DDT / Delivery note: 2014-3E301-0004972  
 Packing List: 2014-3E401-0004431  
 Fattura / Invoice: 2014-3E401-0004431  
 Ns. rif. / Our ref.: 2014-3E201-0002513-0111

Dest. ITEX c/o NORTH SHORE STEEL-FFV  
 12945 MARKET STREET  
 77015 HOUSTON, TEXAS  
 US

Cod. colata Heat Code	Nr. colata Heat Nr	Quantità Quantity	Descrizione Description
	91436	15,00	BLIND 600 RF 1B* LF2CL1

Mat. in acc. a / Mat. in acc. to  
 ASTM/ASME A 350/SA 350 M - 14 ASME CODE SECT. II, PART A, ED. 2013  
 ASTM A350 LF2 CL1  
 NACE MR-0175/2009 ISO 15156  
 NACE MR-0103/2012  
 Q.A.S. IN ACCORD WITH PRESS EQUIPM. DIRECT. 97/23/EC (PED) ANNEX I, PARAGRAPH 4.3  
 CERT. 4687-2014-CE-ITA-ACCREDIA

Ann. mat. / Mat. remarks: FULLY KILLED STEEL AND FINE GRAIN PRACTICED

Elementi / Elements	C	Si	Mn	S	P	Cr	Ni	Mo	Ti	Cu	V	Nb	N
LADLE ANALYSIS	0,190	0,200	0,990	0,001	0,008	0,110	0,070	0,020	0,002	0,070	0,003	0,001	0,000
LADLE ANALYSIS	Al								0,391	0,355	0,273	0,130	--

CE LF=C+Mn/6+(Cr+Mo+V)/5+(Ni+Cu)/15    CE SF=C+Mn/6    F1=Cu+Ni+Cr+Mo+V    F2=Cr+Mo

Provotta Test specimen	Forma Shape	Snervamento > 0,2% Yield Strength > 0,2%	Snervamento > 1,0% Yield Strength > 1,0%	Rottura Tensile	Allungamento Elongation	Contrazione Reduction of area
Sez/Seet mm2    L. mm	1=O - 2=□	MPa	MPa	MPa	%	%
126,60    50,80	1    20	310,0	--	505,0	30,0	61,0

**DUREZZA / HARDNESS** HBW 152,0 - 154,0

**RESILIENZA / IMPACT TEST**

Tipo/Type	Provotta / Test Specimen	1-Joule	2-Joule	3-Joule	Media/Average
KV	10x10 mm	46	68	74	70,7

Tratt. Term. / Heat treatment: NORMALIZED AT 930° C - COOLED IN STILL AIR    ELECTRIC FURNACE

Dim In acc. a / Dim. acc. to: ASME/ANSI B16.5 -2013

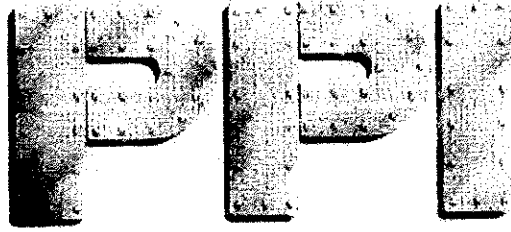
Finitura / Roughness: 125/250 MICROINCH AARH

Marcatura in acc. Marking in acc. to	Vis. & Dim.	SATISFACTORY	Origino Origin of Steel	EUROPEAN UNION
MSS SP25 Ed. 2013				

Note / Notes  
 100% MANUFACTURED IN ITALY  
 MANUFACTURING IN ACCORDANCE WITH ORDER AND SPECIFICATION

4/11/17  
 PPI  
 Q.C.  
 F.W.  
 XAN-89

<b>UFFICIO CONTROLLO QUALITA'</b> QUALITY CONTROL DEPARTMENT <i>S. Frigerio</i>	<b>ENTE UFFICIALE DI COLLAUDO</b> INSPECTION AUTHORITY	<b>MARCHIO PRODUZIONE</b> MANUFACTURER'S SYMBOL 
---	---	--



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

List of Contents

Item: V-402, COLD SEPARATOR

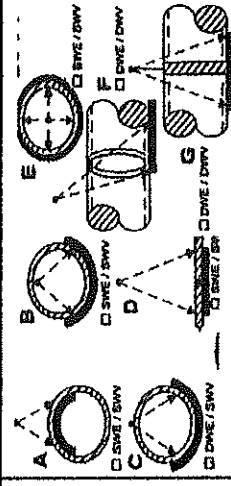
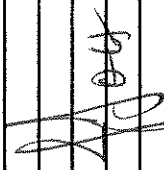
# **Non-Destructive Testing (NDT)**

<b>Pg. 1-5</b>	<b>Radiography Reports</b>
<b>Pg. 6</b>	<b>Magnetic Particle Test Report</b>
<b>Pg. 7</b>	<b>Ultrasonic Test Report</b>

A handwritten signature in black ink, located in the bottom right corner of the page. The signature is stylized and appears to be a name, possibly 'R. East'.



# Radiography Report

API Proj. No:		Client: PPI		Date: 7/15/17		PAGE 1 of 1	
Client Job# / SO#		Project Name: 78" x 2.5" Round Seam		Project Location: Cypress TX			
WFE #		PO #		Governing Spec.: SEC UTR DIV 2			
API Proc. No:		Radiation Source: IR 192		KV: N/A		MA: N/A	
Material:		Reinforcement ("): .125		Focal Spot Size ("): F100		Film (Plate) Load: <input checked="" type="checkbox"/> Single <input type="checkbox"/> Double	
Screens:		Front: .005"		Back: .005"		Film Size: 7.5" x 17"	
View / Location Markers		Pipe Size / Diameter		Pipe / Plate Thickness		Technique	
Weld #		F100C		WELDER ID		Film / Plate Type	
		D3/D4/D5/D7, 50, 80, 100, GP, HR, X		IQL / Penetrator		Reject (X)	
		F100C		Accept (I)		Porosity / Cluster Porosity	
		F100C		Crack		Slag or Inclusion	
		F100C		Inadequate Fusion		Inadequate Penetration	
		F100C		External Undercut		Internal Undercut	
		F100C		Burn Thru		Internal Concavity	
		F100C		High-Low / Mismatch		Film Artifact	
		F100C		Remarks / Comments / Line #			
C-1		2.5"		E		F100C	
2-3		98"		F		F100C	
3-4							
4-5							
5-6							
6-7							
7-8							
8-9							
9-10							
10-11							
11-12							
12-13							
13-14							
14-15							
15-16							
16-17							
17-18							
18-19							
19-20							
20-21							
							

RADIOGRAPHY PRODUCES TWO DIMENSIONAL IMAGES ONLY.  
THE DEPTH OF AND DEFECTS REPORTED ARE OF GOOD FAITH  
OPINIONS ONLY.

# OF WELDS RADIOGRAPHED	TRAVEL		TOTAL HOURS WORKED
	MILES R/T	HOURLY	
# OF RADIOGRAPHIC PERSONNEL	TO		SEE FIELD REPORT
Level II Radiographer:	Austin Wood		CLIENT: Robert Cornwall 7-17-17









# TGR INDUSTRIAL SERVICES

- Welding Specifications
- Welding Procedures
- Welder Qualifications
- Non Destructive Testing
- API-AWS-ASME-ANSI

## TGR INDUSTRIAL SERVICES

2815 Lilac \* Pasadena, Texas 77503  
 Phone 281-487-8800 \* Fax 281-998-0295

### ULTRASONIC INSPECTION REPORT

Customer/Client PPI PROFESSIONAL PROJECTS Project 5654  
 Date June 14, 2017 Location CYPRESS TX P.O. 5654.1  
 Instrument EPOCH Model 600

UTT Longitudinal Frequency 5 MHz Size .5" Type Britek  
 Angle 0 Shear Freq. 5 MHz Size .5" Type Britek Couplant Water/GTX Gel  
 Calibration IIW 97-5503 Reference Reflector .5" Procedure TGR AWS-UT-01 Code AWS Section/Rev. 0  
 AMP 80%  
 Screen Size 6" Surface Condition CLEANED AND PREP Cable Type/Length 5'/Micro dot

Remarks LAMINATION SCAN WAS CARRIED OUT ON AREAS LISTED BELOW

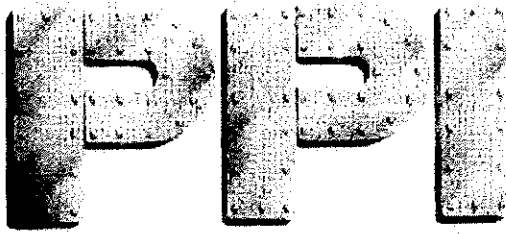
Weld Identification or Location	Angle	A Defect Level (db)	B Ref. Level (db)	C Defect Level (db)	Sound Path (ui)	Surface Dist. To Weld Ctr. Line	'X' Dist. (in.)	'Y' Dist. (in.)	Depth From 'A' Face (in.)	Length of Flaw (in.)	Matl. Thick (in.)	Accept	Reject
<b>5654/5654-1</b>													
D1	0	N/A	54.2								.875"	X	
D2	0	N/A	54.2								.875"	X	
E	0	N/A	54.2								.875"	X	
F1	0	N/A	54.2								.875"	X	
F2	0	N/A	54.2								.875"	X	
G1	0	N/A	54.2								.875"	X	
G2	0	N/A	54.2								.875"	X	
G3	0	N/A	54.2								.875"	X	
G4	0	N/A	54.2								.875"	X	
J	0	N/A	54.2								.875"	X	

Technician(s) Eric Fontenot NDT Level II Date 6/14/17 Hours .857

Client Signature Robert Camm Mileage 108 Travel Time 1hr Level III Approval \_\_\_\_\_ NO. 61417-F

6-14-17





**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

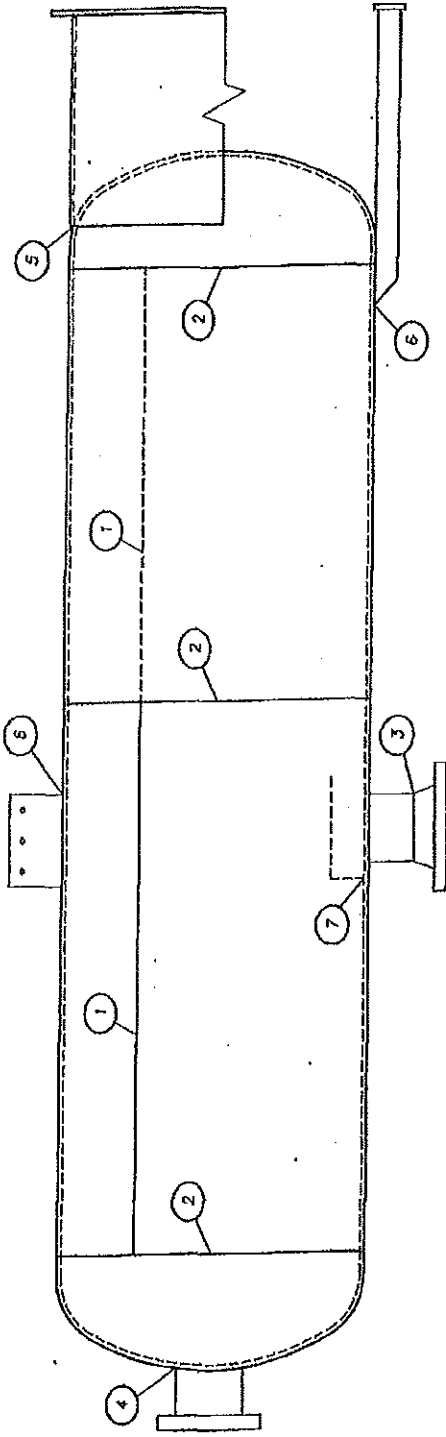
List of Contents

Item: V-402, COLD SEPARATOR

# **Welding**

<b>Pg. 1</b>	<b>Approved Weld Map</b>
<b>Pg. 2-6</b>	<b>WPS 149DCP Rev. 2</b>
<b>Pg. 7-11</b>	<b>WPS 151DCP Rev. 1</b>
<b>Pg. 12&amp;13</b>	<b>Eduardo Martinez Navejar (Dot.T)</b>
<b>Pg. 14&amp;15</b>	<b>Francisco Morales (E)</b>
<b>Pg. 16&amp;17</b>	<b>Emmanuel Cruz (I)</b>
<b>Pg. 18&amp;19</b>	<b>Roberto Alvarez (K)</b>
<b>Pg. 20&amp;21</b>	<b>Gerardo Perez (Q)</b>

A handwritten signature in black ink, located in the bottom right corner of the page. The signature is stylized and appears to be the name 'ROSE'.



**WELD MAP**

*[Handwritten Signature]*

**PPI** Professional Projects, Inc.

P.O. BOX 618 (118115 TELGE RD.) CYPRESS, TEXAS 77429

TITLE: 78" ID x 12'-0" s/s  
ITEM: V-402  
Cold Separator

CUSTOMER: UOP RUSSEL

CUSTOMER P.O. NO: 4500754097

PPI NO: 5654 DATE: 5/3/2017

DRAWING NO: S/O 5654-1

PWHT:	IMPACT TEST:	BASE METAL & THICKNESS	NOTES
Required	Required	SA-516-70N / 3.25"	
NO.	WELDMENT	WPS/PQR	NOTES
1	CAT A LONG SEAMS	151dcp/151-1dcp	
2	CAT B ROUND SEAMS	151dcp/151-1dcp	
3	CAT C FLANGE/PIPE/FORGING	149dcp/149-1dcp	
4	CAT D NOZZLE TO SHELL/HEAD	149dcp/149-1dcp	
5	SKIRT TO HEAD	151dcp/151-1dcp	
6	EXTERNAL ATTACHMENTS	149dcp/149-1dcp	
7	INTERNAL ATTACHMENTS	149dcp/149-1dcp	

EQUIP/TAG NUMBER

126-1103 126-1202  
 126-1203 126-1204

A - PROCEED

Authorization to proceed does not relieve Contractor/Supplier of its responsibility or liability under the Contract and or Purchase Order.  
 By Mario Ragma on Nov 27, 2015

"ALSO FOR SOUR SERVICE FABRICATION"

QW-482 SUGGESTED FORMAT FOR WELDING PROCEDURE SPECIFICATION (WPS)  
 (See QW-201.1, Section IX, ASME Boiler and Pressure Vessel Code)

Company Name:	Professional Projects, Inc.	By:	Seth B. Westbrook
Welding Procedure Specification No.	149 DCP	Date	3/07/13
Revision No.	2	Date	6/28/2013
Welding Process(es):	GMAW / FCAW	Type(s)	Semi-Automatic
(Automatic, Manual, Machine, or Semi-Auto)			

**JOINTS (QW-402)** Details

Joint Design: All Types: Groove & Fillet

Backing (Yes) FCAW (No) GMAW

Backing Material (Type) Base / Weld Metal SEE PRODUCTION DRAWINGS

(Refer to both backing and release.)

Metal	Nonfusing Metal	No permanent backing bars, rings, straps, etc. shall be used.
Nonmetallic	Other	

Sketches, Production Drawings, Weld Symbols or Written Description should show the general arrangement of the parts to be welded. Where applicable, the root spacing and the details of weld groove may be specified.

(At the option of the Mfg. sketches may be attached to illustrate joint design, weld layers and bead sequence, e.g. for notch toughness procedures, for multiple process procedures, etc.)

ROOT GAP 0" MIN. - 3/16" MAX.

PROFESSIONAL PROJECTS

DEC 02 2015

RECEIVED

**BASE METALS (QW-403)**

P-No. 1 Group No. \*\* 1 & 2 to P-No. 1 Group No. \*\* 1 & 2

OR

Specification type and grade SA-516-GR.70 Normalized

to Specification type and grade SA-516-GR.70 Normalized

OR

Chem. Analysis and Mech. Prop. \_\_\_\_\_

to Chem. Analysis and Mech. Prop. \_\_\_\_\_

Thickness Range:

Base Metal:	Groove	<u>.1875<sup>***</sup> - 8.00<sup>*</sup></u>	Fillet	<u>All</u>
Pipe Dia. Range:	Groove	<u>All</u>	Fillet	<u>All</u>

Other: \_\_\_\_\_

FILLER METALS (QW-404)	GMAW	FCAW
Spec. No. (SFA)	5.18	5.20
AWS No. (Class)	ER70S-2	E71T-1MjH4 (1.60% Mn Max.)
F-No.	6	6
A-No.	1	1
Size of Filler Metals	<u>.035" (Bare)</u>	<u>.045" (Flux Cored)</u>
Deposited Weld Metal	<u>.125"</u>	<u>1.625"</u>
Thickness Range:		
Groove	<u>.1375" Max.</u>	<u>8.00" Max.</u>
Fillet	<u>All</u>	<u>All</u>
Electrode-Flux (Class)	----	----
Flux Trade Name	----	<u>ESAB Dual Shield II 70T-12H4</u>
Consumable Insert	----	----
Other	<u>No Supplementary Filler Metal or Powdered Filler Metal Shall Be Used.</u>	

Each base metal-filler metal combination should be recorded individually.

\*\* WHEN IMPACT TESTING IS REQUIRED BASE MATERIAL TO BE P1 GROUP 2 AND MINIMUM THICKNESS QUALIFIED IS .825" WITH A MAXIMUM THICKNESS OF 8.00"

\*\* WPS may be used with base metal normalized conditions.

\*\* WPS may be used for Sour Service and all other welds that may be exposed to environments that may cause stress, corrosion and cracking

LEGEND

QW-482 (Back)

\*\* WHEN IMPACTS ARE REQUIRED  
 \*\*\* WITHOUT IMPACTS

WPS No. 148 DCP Rev. 2

<b>POSITIONS (QW-405)</b>		<b>POSTWELD HEAT TREATMENT (QW-407)</b>																																	
Position(s) of Groove	** 1G (Flat) / *** All Positions	Temperature Range	* 1150° F ± 25° F																																
Welding Progression:	Up: **XX Down: ----	Time Range	1 Hour per inch of thickness/1hr minimum																																
Position(s) of Fillet	** 1F, 2F / *** All Positions	Maximum hold time	1.75 hrs																																
<b>PREHEAT (QW-406)</b>		<b>GAS (QW-408)</b>																																	
Preheat Temp. Min.	* 175°F < 1"; 200°F > 1"	Shielding Gas(es)	Argon / CO <sup>2</sup>																																
Interpass Temp. Max.	300° F	Percent Composition (mixture)	75% Argon 25% CO <sup>2</sup>																																
Preheat Maintenance	None	Flow Rate	30-40 CFH																																
(Continuous or special heating where applicable should be recorded)		Gas Backing	None																																
		Trailing Shielding Gas Composition	None																																
<b>ELECTRICAL CHARACTERISTICS (QW-409)</b>																																			
Current AC or DC	Direct	Polarity	Reverse																																
Amps (Range)	Volts (Range)		**																																
(Amps and volts range should be recorded for each electrode size, position, and thickness, etc. This information may be listed in a tabular form similar to that shown below.)			GMAW																																
			120-190																																
			FCAW																																
			130-265																																
Tungsten Electrode Size and Type	-----																																		
Mode of Metal Transfer for GMAW	GMAW - Short Circuiling / FCAW - Spray Transfer																																		
Electrode Wire feed speed range	GMAW - 120-140 IPM / FCAW - 150-520 IPM																																		
<b>TECHNIQUE (QW-410)</b>																																			
String or Weave Bead	String																																		
Orifice or Gas Cup Size	GMAW: 1/2" / FCAW: 3/4"																																		
Initial and Interpass Cleaning (Brushing, Grinding, etc.)	Grind in bevel and 1" each side of joint. Grind, wire brush and scaling hammer between layers of weld metal. Surfaces shall be clean and free of paint, oil, dirt, scale, oxides and other detrimental material.																																		
Method of Back Gouging	Carbon-Arc and grind to sound metal to completely remove GMAW Root Pass.																																		
Oscillation	None																																		
Contact Tube to Work Distance	3/8" - 1.0"																																		
Multiple or Single Pass (per side)	Multiple																																		
Multiple or Single Electrodes	Single																																		
Travel Speed (Range)	GMAW: 6-10 IPM / FCAW: 12-14 IPM																																		
Peening	Is not allowed. A scaling hammer (flitterbug) is not considered peening.																																		
Other	No pass greater than 1/4" allowed Where required back weld using FCAW process.																																		
<table border="1"> <thead> <tr> <th rowspan="2">Weld Layers</th> <th rowspan="2">Process</th> <th colspan="2">Filler Metal</th> <th colspan="3">Current</th> <th rowspan="2">IPM Travel Speed Range</th> <th rowspan="2">Other (E.G., Remarks, Comments, Hot Wire Addition, Technique Torch Angle, etc.)</th> </tr> <tr> <th>Class</th> <th>Diameter</th> <th>Type Polarity</th> <th>Amp. Range</th> <th>Volt Range</th> </tr> </thead> <tbody> <tr> <td>Root</td> <td>GMAW</td> <td>ER70S-2</td> <td>.035"</td> <td>DC-Rev.</td> <td>120-190</td> <td>18-20</td> <td>6-10</td> <td>max 22,800 J/in</td> </tr> <tr> <td>2nd Completion</td> <td>FCAW</td> <td>E71T-1M/JH4</td> <td>.045"</td> <td>DC-Rev.</td> <td>130-265</td> <td>22-29</td> <td>12-14</td> <td>max 32,935 J/in</td> </tr> </tbody> </table>				Weld Layers	Process	Filler Metal		Current			IPM Travel Speed Range	Other (E.G., Remarks, Comments, Hot Wire Addition, Technique Torch Angle, etc.)	Class	Diameter	Type Polarity	Amp. Range	Volt Range	Root	GMAW	ER70S-2	.035"	DC-Rev.	120-190	18-20	6-10	max 22,800 J/in	2nd Completion	FCAW	E71T-1M/JH4	.045"	DC-Rev.	130-265	22-29	12-14	max 32,935 J/in
Weld Layers	Process	Filler Metal				Current			IPM Travel Speed Range	Other (E.G., Remarks, Comments, Hot Wire Addition, Technique Torch Angle, etc.)																									
		Class	Diameter	Type Polarity	Amp. Range	Volt Range																													
Root	GMAW	ER70S-2	.035"	DC-Rev.	120-190	18-20	6-10	max 22,800 J/in																											
2nd Completion	FCAW	E71T-1M/JH4	.045"	DC-Rev.	130-265	22-29	12-14	max 32,935 J/in																											

\* FOR SOUR SERVICE MINIMUM PREHEAT TO BE 200° F & PWHT WILL BE AT 1175° F ± 25° F

**Professional Projects, Inc.**  
 18116 Telge Road, Cypress, TX 77428  
**ASME - Procedure Qualification Record (PQR) - QW-483**  
 Weld Office WPS

PQR record number Date	149-1 DCP 4/25/2012	Revision 0	WPS record number Company name Welding standard	149 DCP Professional Projects, Inc. ASME section IX	Revision 0
---------------------------	------------------------	------------	---	---	------------

BASE METALS (QW-403)	Product form	Specification (type or grade)	P no.	Qp no.	Sha	Shc	Thick.	(in.)	Th.	(in.)
Welded test	Plate	SA-516 (70) N	1	2	-	-	1.750	-	-	-
and tested.	With PWHT, With Impacts, With hardness									
Notes										

POST WELD HEAT TREATMENT (QW-107)		Time	(hr)	1.75	Type	Stress relief
Temperature	(°F)	1150				
Heating rate	(°F/hr)	230		Flame		
Cooling rate	(°F/hr)	250		Flame		
Notes	Controlled heating and cooling from 850°F					

JOINTS (QW-402)		Joint design	Single-V groove	Yes; weld metal	
Backing		None			
Reinforcers		None			
Groove angle	(deg)	60			
Root opening	(in.)	1 3/4			
Root face	(in.)	1/8			

WELDING PROCESSES	QIAW Semi-automatic	FOAW Semi-automatic
Welding process		
Type		

FILLER METALS (QW-404)	QIAW Semi-automatic	FOAW Semi-automatic
EFA specification	E-10	E-20
AWS classification	ER10S-2	E71T-12H-RH
Filler metal F-number	0	6
Weld metal A-number	1	11
Filler metal (chemical) composition	solid wire	flux coated
Filler metal trade name	not recorded	not recorded
Filler metal size (in.)	.035	.045
Deposited thickness (in.)	.125	1.825
Maximum pass thickness (in.)	.125	.125
Weld deposit chemistry	carbon steel	carbon steel
Supplemental filler metal	none	none
Supplemental filler metal vol. (in.)	none	none

POSITION (QW-406)	QIAW Semi-automatic	FOAW Semi-automatic
Position	0	10
Weld progression	-	-

PREHEAT (QW-408)	QIAW Semi-automatic	FOAW Semi-automatic
Preheat temperature (°F)	300	200
Maximum interpass temperature (°F)	300	300

GAS (QW-409)		QIAW Semi-automatic	FOAW Semi-automatic
Shielding gas:	Type	75% Argon, 25% CO2	75% Argon, 25% CO2
	Flow rate (cfr)	40	40
	Flow rate (cfr)	None	None
Torching gas:	Type	None	None
	Flow rate (cfr)	-	-
Backlog gas:	Type	None	None
	Flow rate (cfr)	-	-

ELECTRICAL (QW-409)		QIAW Semi-automatic	FOAW Semi-automatic
Filler metal size (in.)		.035	.045
Amps		182	227
Volts		23	26
Torch speed (in./min)		10	16
Maximum heat input (Btu/in)		25.118	23.835
Current polarity		DCEP (reverse polarity)	DCEP (reverse polarity)
Wire feed speed (in./min)		280	360
Arc transfer mode		Short circuiting	Spray

TECHNIQUE (QW-410)		QIAW Semi-automatic	FOAW Semi-automatic
Shield or weave		Stringer	Stringer
Orifice/arc cup size (in.)		3/4	3/4
O.T.W.D.		3/4	3/4
Multiple passes per side		Single pass	Multiple passes
Peening		Not used	Not used
Interpass cleaning		Bushing and Grinding	Bushing and Grinding
Back gouging method		None	None

**Professional Projects, Inc.**  
 18116 Telge Road, Cypress, TX 77429  
**ASME - Procedure Qualification Record (PQR) - Test results (PWHT)**  
 WeldOffice WPS

PQR record number Date	149-1 DCP 4/25/2013	Revision 0	WPS record number Company name Welding standard	149 DCP Professional Projects, Inc. ASME Section IX	Revision 0
---------------------------	------------------------	------------	---	---	------------

TENSILE TESTS (QW-150)						
Specimen number	Width (in.)	Thickness (in.)	Area (in <sup>2</sup> )	Ultimate (tensile) load (lb)	Ultimate unit stress (ksi)	Type of failure and location
T-1	.746	.021	0.0216	49100	76500	Ductile-BM
T-2	.749	.021	0.0223	44900	76000	Ductile-BM
T-3	.740	.021	0.0111	46500	76000	Ductile-BM
T-4	.743	.025	0.0331	45700	76500	Ductile-BM

GUIDED BEND TESTS (QW-160)			
Type of test	Acceptance criteria	Result	Comments
4 transverse cold bends per QW-161.1 and QW-162.2	QW-163	Acceptable	see ASME IX - QW-161.1

TOUGHNESS TESTS (QW-170)								
Specimen number	Notch location	Notch type	Specimen size (in.) x (in.)	Test temperature (°F)	(ft lb)	Impact values (ft lb-in)	(J)	Drop weight break
	Weld Metal	V-notch	0.254 x 0.254	-50	33-40-47	20-20-40	29-42-44	
	Weld Metal H/T	V-notch	0.254 x 0.254	-50	18-37-68	20-30-50	17-31-58	
	HAZ	V-notch	0.254 x 0.254	-50	70-30-89	40-30-40	20-50-78	

HARDNESS TEST						
Type (Scale)	Distance (from surface)	6A-518 (70) H	HAZ	Weld	HAZ	6A-510 (70) H
Vickers (HV) 10Kg	1/16" from surface	140	107-103	220-198-185	183-173	160
Vickers (HV) 10Kg	Mid wall		102	211	167	
Vickers (HV) 10Kg	1/16" above surface	165	104-108	221-215	203-190	180

OTHER TESTS			
Type of test	Acceptance criteria	Result	Comments
Weld Metal Chemistry		Acceptable	see page 3

CERTIFICATION				
Welder name	ID Number	Stamp number	Mechanical testing by Laboratory test number Test file number Tests conducted by	Dynabac Laboratories, Inc. MT13-282 Jesus Vazquez

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Dynabac Laboratories, Inc.	Professional Projects, Inc.		
Name	Signature	Name	Signature
Ready Hurray		Keith B. Westbrook	
Date		Date	
4/26/2013		4/26/2013	

Professional Projects, Inc.  
18116 Teige Road, Cypress, TX 77428  
ASME - Additional Information (PQR)  
WeldOffice WPS

PQR record number Date	14F-1 DCP 4/25/2013	Revision #	WPS record number Company name Writing standard	14F DCP Professional Projects, Inc. ASME Section IX	Revision #
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C Mn Si S P Cr Ni Mo V Al Cu Ti Zr Nb B  
.05 1.26 .72 .001 .02 .03 .04 .01 .01 .02 .14 .03 .005 .01 .0007

"ALSO FOR SOUR SERVICE FABRICATION"

**QW-482 SUGGESTED FORMAT FOR WELDING PROCEDURE SPECIFICATION (WPS)**  
 (See QW-201.1, Section IX, ASME Boiler and Pressure Vessel Code)

Company Name: Professional Projects, Inc. By: Seth B. Westbrook  
 Welding Procedure Specification No. 151 DCP Date 3/07/13 Supporting PQR No.(s) 151-1 DCP  
 Revision No. 1 Date 5/28/2013  
 Welding Process(es): GMAW / FCAW / SAW Type(s) Semi-Automatic / Machine  
 (Automatic, Manual, Machine, or Semi-Auto)

**JOINTS (QW-402)** Details

Joint Design: All Types: Groove & Fillet  
 Backing (Yes) FCAW, SAW (No) GMAW  
 Backing Material (Type) Base / Weld Metal SEE PRODUCTION DRAWINGS  
 (Refer to both backing and retainers.)

Metal Nonfusing Metal  
 Nonmetallic Other . No permanent backing bars, rings, straps, etc. shall be used.

Sketches, Production Drawings, Weld Symbols or Written Description should show the general arrangement of the parts to be welded. Where applicable, the root spacing and the details of weld groove may be specified.

(At the option of the Mfr. sketches may be attached to illustrate joint design, weld layers and bead sequence, e.g. for notch toughness procedures, for multiple process procedures, etc.)

ROOT GAP 0" MIN. - 3/16" MAX.

PROFESSIONAL PROJECTS  
 DEC 02 2015  
 RECEIVED

**BASE METALS (QW-403)**

P-No. 1 Group No. \*\* 1 & 2 to P-No. 1 Group No. \*\* 1 & 2  
 OR  
 Specification type and grade SA-516-GR.70 Normalized  
 to Specification type and grade SA-516-GR.70 Normalized  
 OR  
 Chem. Analysis and Mech. Prop. \_\_\_\_\_  
 to Chem. Analysis and Mech. Prop. \_\_\_\_\_

Thickness Range:  
 Base Metal: Groove .1875<sup>\*\*\*</sup> - 8.00<sup>\*</sup> Fillet All  
 Pipe Dia. Range: Groove All Fillet All  
 Other: \_\_\_\_\_

FILLER METALS (QW-404)	GMAW	FCAW	SAW
Spec. No. (SFA)	5.18	5.20	5.17
AWS No. (Class)	ER70S-2	E71T-1M/JH4 (1.60% Mn)	EH14K
F-No.	6	6	6
A-No.	1	1	1
Size of Filler Metals	.035" (Bare)	.045" (FLUX CORED)	3/32", 1/8"
Deposited Weld Metal	.125"	.250"	1.375"
Thickness Range:			
Groove	.1375" Max.	.500" Max.	8.00" Max.
Fillet	All	All	All
Electrode-Flux (Class)	----	----	ESAB Spool Arc 71
Flux Trade Name	----	Dual Shield II 70T-12H4	ESAB OK Flux 10.62
Consumable Insert	----	----	----
Other	No Supplementary Filler Metal or Powdered Filler Metal Shall Be Used.		

Each base metal-filler metal combination should be recorded individually. SAW: No Recrushed Slag Used.

\*\* WHEN IMPACT TESTING IS REQUIRED BASE MATERIAL TO BE P1 GROUP 2 AND MINIMUM THICKNESS QUALIFIED IS .625"  
 \*\* base metal is in the normalized condition

**FLUOR.**  
 A - PROCEED  
 Authorization to proceed does not relieve Contractor/Supplier of its responsibility or liability under the Contract and/or Purchase Order.  
 By Mario Ragma on Nov 27, 2015

FLUOR A7DJ  
 IOC, NO. REC'D: 02-DEC-2015  
 A7DJ-FAR-4-0207-00003-3A  
 QWP/PLAG NUMBER  
 126-1163 126-1202  
 126-1203 126-1204

126-1205 126-1206  
 126-1212 27-1213-02  
 27-1228-04

\*\* WHEN IMPACTS ARE REQUIRED  
 \*\*\* WITHOUT IMPACTS

QW-482 (Back)

WPS No. 151 DCP Rev. 1

POSITIONS (QW-405) **1G (Flat)		POSTWELD HEAT TREATMENT (QW-407)	
Position(s) of Groove	*** SAW 1G ; GMAW / FCAW All Positions	Temperature Range	1175°F ± 25 degrees
Welding Progression:	Up: FCAW/GMAW Down: ---	Time Range	1.75 hr min (1 hr min per in for sour service 1hr min less than 1" thick)
Position(s) of Fillet	** 1F, 2F / *** SAW 1F, 2F GMAW / FCAW All Positions	GAS (QW-408)	GMAW / FCAW Processes Only
PREHEAT (QW-406)		Shielding Gas(es)	ARGON / CO <sup>2</sup>
Preheat Temp. Min.	*175°F < 1" / 200° > 1"	Percent Composition (mixture)	75% Aron 25% CO <sup>2</sup>
Interpass Temp. Max.	350°	Flow Rate	30-40 CFH
Preheat Maintenance	None	Gas Backing	None
(Continuous or special heating where applicable should be recorded)		Trailing Shielding Gas Composition	None

ELECTRICAL CHARACTERISTICS (QW-409)			
Current AC or DC	Direct	Polarity	Reverse
Amps (Range)	*	Volts (Range)	**
(Amps and volts range should be recorded for each electrode size, position, and thickness, etc. This information may be listed in a tabular form similar to that shown below.)			
		GMAW	GMAW
		115-125	18-20
		FCAW	FCAW
		130-265	22-29
		SAW	SAW
		400-700	28-35
Tungsten Electrode Size and Type	(Pure Tungsten, 2% Thoriated, etc.)		
Mode of Metal Transfer for GMAW	GMAW - Short Circuiting / FCAW - Spray Transfer		
Electrode Wire feed speed range	(Spray arc, short circuiting arc, etc.) GMAW - 120-140 IPM / FCAW - 150-520 IPM / SAW - 60-80 IPM		

TECHNIQUE (QW-410)	
String or Weave Bead	String
Orifice or Gas Cup Size	GMAW - 1/2" / FCAW - 3/4" / SAW - 3/4"
Initial and Interpass Cleaning (Brushing, Grinding, etc.)	Grind in bevel and 1/2" each side of joint. Grind, wire brush and scaling hammer between layers of weld metal. Surfaces shall be clean and free of paint, oil, scale and other detrimental materials
Method of Back Gouging	Carbon-Arc to remove GMAW Root Pass completely and grind to sound metal.
Oscillation	None
Contact Tube to Work Distance	GMAW & FCAW 3/8" - 1" / SAW 1" - 1-1/2"
Multiple or Single Pass (per side)	Multiple
Multiple or Single Electrodes	Single
Travel Speed (Range)	GMAW: 6-9 IPM / FCAW: 12-14 IPM / SAW: 16-20 IPM
Peening	Is not allowed. A scaling hammer (jitterbug) is not considered peening.
Other	No pass greater than 3/8" allowed Where required back weld using FCAW process.

Weld Layers	Process	Filler Metal		Current			IPM Travel Speed Range	Other (E.g., Remarks, Comments, Hot Wire Addition, Technique Torch Angle, etc.)
		Class	Diameter	Type	Amp. Range	Volt Range		
ROOT	GMAW	ER70S-2	.035"	DC-REV.	120-130	20-22	6-9	max 19,066 J/in
Hot Pass	FCAW	E71T-1MJH4	.045"	DC-REV.	130-265	22-29	12-14	max 32,935 J/in
3rd	SAW	EM14K	1/8"	DC-REV.	400-700	28-39	16-20	max 81,900 J/in
Completion 1 Side	SAW	EM14K	3/32"	DC-REV.	400-600	28-39	14-18	max 78,000 J/in
Backweld	FCAW	E71T-1MJH4	.045"	DC-REV.	130-265	22-29	12-14	max 32,935 J/in

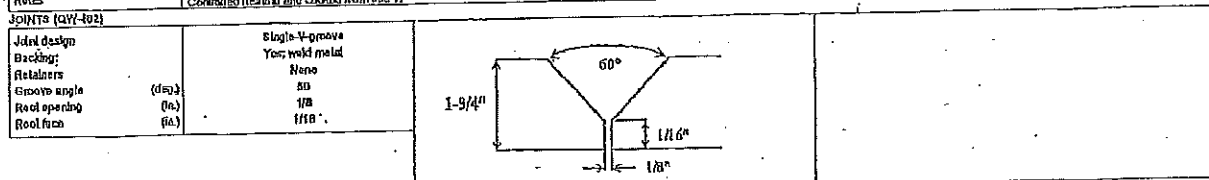
\* FOR SOUR SERVICE MINIMUM PREHEAT TO BE 200 °F

**Professional Projects, Inc.**  
 18115 Telge Road, Cypress, TX 77429  
**ASME - Procedure Qualification Record (PQR) - QW-483**  
 Weld Office WPS

PQR record number Date	161-DCP 4/28/2013	Revision 0	WPS record number Company name Welding standard	161 DCP Professional Projects, Inc. ASME Section IX	Revision 0
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BARE METALS (QW-103)		Product form	Specification (type or grade)	P no.	Grp. no.	Size	Sch.	Thick.	(in.)	Th.	(in.)
Welded to:		Plate	SA-516 (70) N SA-516 (70) N	1 1	2 2	- -	- -	1.750 1.750	- -	- -	- -
and tested Notes	W/A PWHT, With impacts, With hardness										

POST WELD HEAT TREATMENT (QW-107)		Temp	(°F)	Time	(hrs)	1.75	Temp	Type	Stress relief
Temperature	(°F)	3150							
Heating rate	(°F/hr)	220							
Cooling rate	(°F/hr)	280							
Notes	Controlled heating and cooling from 800°F								



WELDING PROCESSES		GTAW	FCM	SAW
Welding process		Gas metal arc	Shielded metal arc	Automatic
Type				
<b>FILLER METALS (QW-104)</b>				
BFA specification		E-30	E-30	E-30
AWA classification		E70S-2	E70T-2M-3H	E70T-2M-3H
Filler metal F-number		1	11	1
Weld metal F-number		1	11	1
Filler metal nominal composition		solid wire	flux cored	solid wire
Filler metal trade name		not recorded	not recorded	ESAB Spool Arc 71
Filler metal size	(in)	.035	.035	1/8
Deposited thickness	(in)	.125	.250	1.375
Maximum pass thickness	(in)	.125	.125	.250
Weld deposit chemistry		carbon steel	carbon steel	carbon steel
Flux AWS specification		-	-	E-30
Flux AWS classification		-	-	F-7A
Flux nominal composition		-	-	borated flux
Flux trade name		-	-	ESAB OK Flux 10.62
Flux type		-	-	Neutral flux
Flux from reworked stock		-	-	no
Supplemental filler metal		none	none	none
Supplemental filler metal vol.	(%)	none	none	none
<b>POSITION (QW-105)</b>				
Position		1G	1G	1G
Weld progression		-	-	-
<b>PREHEAT (QW-106)</b>				
Preheat temperature	(°F)	200	200	200
Maximum interpass temperature	(°F)	350	350	350
<b>GAS (QW-108)</b>				
Shielding gas	Type	75% Argon, 25% CO2	75% Argon, 25% CO2	-
	Flow rate	40	40	-
Trailing gas	Type	None	None	-
	Flow rate	-	-	-
Backing gas	Type	None	None	-
	Flow rate	-	-	-
<b>ELECTRICAL (QW-109)</b>				
Filler metal size	(in)	.035	.035	1/8
Amps		162	227	500
Volt		23	28	29
Travel speed	(in/min)	10	13.635	72.8161
Maximum heat input	(Btu/in)	26.110	23.635	10.62
Current polarity		DCEP (reverse polarity)	DCEP (reverse polarity)	DCEP (reverse polarity)
Wire feed type		-	-	Gas wire
Wire feed speed	(in/min)	250	380	87
Arc transfer mode		Shield-circuiting	Spray	-
<b>TECHNIQUE (QW-110)</b>				
String or weave		Stringer	Stringer	Stringer
Offset cup size	(in)	3/4	3/4	1.0
Offset		3/4	3/4	None
Condition		-	-	Single electrode
Multiple electrodes		-	-	50
Electrode angle	(deg)	Single pass	Multiple passes	Multiple passes
Multiple passes per side		-	-	Multiple layer
Multiple or single layer		Not used	Not used	Not used
Preheat		Brushing and grinding	Brushing and grinding	Brushing and grinding
Interpass cleaning		Grinding	None	None
Back gouging method		-	-	-

**Professional Projects, Inc.**  
 10115 Telge Road, Cypress, TX 77429  
**ASME - Procedure Qualification Record (PQR) - Test results (PWHT)**  
 WeldOffice.WPS

PQR record number Date	151-DCP 4/28/2013	Revision 0	WPS record number Company name Welding standard	151 DCP Professional Projects, Inc. ASME Section IX	Revision 0
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TENSILE TESTS (QW-150)							Reduced section
Specimen number	Width (in.)	Thickness (in.)	Area (in <sup>2</sup> )	Ultimate total load (lb)	Ultimate wall stress (psi)	Type of failure and location	
T-1A	.763	.821	0.6162	49600	80290	Ductile-BH	
T-1B	.764	.790	0.6002	46100	77000	Ductile-BH	
T-2A	.764	.807	0.6085	46800	80000	Ductile-BH	
T-2B	.763	.808	0.6060	46800	77800	Ductile-BH	

Comments				
GUIDED BEND TESTS (QW-160)		Acceptance criteria	Result	Comments
4 transverse side bends per QW-101.1 and QW-102.2		QW-103	Acceptable	see - ASME IX - QW-151.1

Comments								
TOUGHNESS TESTS (QW-170)								
Specimen number	Notch location	Notch type	Specimen size (in.) x (in.)	Test temperature (°F)	Impact values (ft-lb)	Impact values (J)	Impact values (ft-lb)	Drop weight break
	Weld Metal	V-notch	0.394 x 0.394	-50	100-84-108	60-40-70	83-71-90	
	Weld Metal HAZ	V-notch	0.394 x 0.394	-50	88-105-79	75-75-60	88-91-85	
	HAZ	V-notch	0.394 x 0.394	-50	69-73-20	40-30-10	63-68-28	

Comments						
HARDNESS TEST						
Type (Scale)	Distance from surface	SA-516 (70) H	HAZ	Weld	HAZ	SA-516 (70) H
Vickers (HV) 100g	1/16" from surface	161	170-176	189-220-203	185-208	148
Vickers (HV) 100g	1/8" HAZ		178	174	171	
Vickers (HV) 100g	1/16" above surface	182	174-187	237-240	180-185	164

Comments			
OTHER TESTS			
Type of test	Acceptance criteria	Result	Comments
Weld Metal Chemistry		Acceptable	see page 3

Comments				
CERTIFICATION				
Welder's name	ID Number	Stamp number	Mechanical testing by Laboratory test number Test ID number Tests conducted by	Dynamic Laboratories, Inc. 64713-263 Jesus Vazquez

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Dynamic Laboratories, Inc.		Professional Projects, Inc.		
Name	Signature	Name	Signature	
Randy Maxey		Seth B. Desbrouck		
Date		Date		
4/28/2013		4/27/2013		

**Professional Projects, Inc.**  
 18115 Telge Road, Cypress, TX 77429  
**ASME - Additional Information (PQR)**  
 WeldOffice WPS

<small>PQR record number</small>	151-1 DCP	<small>Revision 0</small>	<small>WPS record number</small>	151 DCP	<small>Revision 0</small>
<small>Data</small>	4/28/2013		<small>Company name</small>	Professional Projects, Inc.	
			<small>Welding standard</small>	ASME Section IX	

C	Mn	Si	S	P	Cr	Ni	Mo	V	Al	Cu	Ti	Zr	Nb	B
.01	1.26	.70	.002	.01	.03	.04	.01	.01	.02	.14	.03	.005	.01	.00063

**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Eduardo Martinez Navejar Clock No. \_\_\_\_\_ Stamp No. Dot.T

Using WPS No. 149 DCP Rev. 2 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification GMAW / FCAW	Qualification Ranges GMAW / FCAW
Process	Semi-Auto	Semi-Auto
Process Type	Without / With	Without / With
Backing [metal, weld metal, flux, etc. (QW-402)]	P1 to P1	P1 to P1
Material Spec. (QW-403)		
Thickness		.1875" - 8.00"
Groove	-----	All
Fillet	-----	
Diameter		2 7/8" OD & Over
Groove	All	All
Fillet	All	
Filler Metal (QW-404)		
Spec. No.	5.18 / 5.20	5.18 / 5.20
Class	ER70S-2/E71T-1MJH4	ER70S-2/E71T-1MJH4
F-No.	6 / 6	6 / 6
Deposited Weld Metal Thickness	GMAW= .125"	GMAW= .1375" Max.
Groove	FCAW= 1.625"	FCAW= 8.00" Max.
Fillet	1G (Flat)	1G (Flat)
Position (QW-405)	Uphill/Downhill	Uphill/Downhill
Weld Progression (QW-410)	75% Argon / 25% CO <sup>2</sup>	75% Argon / 25% CO <sup>2</sup>
Gas Type (QW-408)		
Gas Backing	<u>N/A</u>	
Electrical Characteristics (QW-409)		
Current	DC	DC
Polarity	Reverse	Reverse

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

Other: **Visual Examination - Satisfactory**

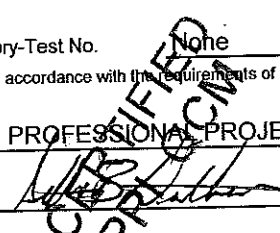
Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 6/24/2012

By: \_\_\_\_\_



(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)  
NOTE: Any essential variables in addition to those above shall be recorded.

**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)**

(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)

Welder Name Eduardo Martinez Navejar Clock No. \_\_\_\_\_ Stamp No. Dot.T

Using WPS No. 151DCP Rev. 1 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values	With /	Qualification Ranges
	Used in Qualification		GMAW / FCAW / SAW
Process	GMAW / FCAW / SAW		GMAW / FCAW / SAW
Process Type	Semi-Auto / Auto		Semi-Auto / Auto
Backing [metal, weld metal, flux, etc. (QW-402)]	Without / With / With		Without / With / With
Material Spec. (QW-403)	P1 to P1		P1 to P1
Thickness	.750"		.1875" - 1.50"
Groove	-----		All
Fillet	-----		
Diameter	-----		2-7/8" & Over
Groove	-----		All
Fillet	-----		
Filler Metal (QW-404)	5.18 / 5.20 / 5.17		5.18 / 5.20 / 5.17
Spec. No.	ER70S-2 / E71T-1 / EM13K		ER70S-2 / E71T-1 / EM13K
Class	6 / 6 / 6		6 / 6 / 6
F-No.	GMAW= .125"		GMAW= .1375" Max.
Deposited Weld Metal Thickness	FCAW= .3125"		FCAW= .625 Max.
	SAW= .4375"		SAW= .875" Max
	1G		1G
Position (QW-405)	Uphill/Downhill/Downhill		Downhill
Weld Progression (QW-410)	75% Argon / 25% CO <sup>2</sup>		75% Argon / 25% CO <sup>2</sup>
Gas Typ (QW-408)			
Gas Backing	N/A		
Electrical Characteristics (QW-409)			
Current	DC		DC
Polarity	Reverse		Reverse

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

**Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. \_\_\_\_\_

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 6/20/2012 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

\* No Consumable inserts

**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Francisco Morales Clock No. \_\_\_\_\_ Stamp No. E

Using WPS No. 149 DCP Rev. 2 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	Qualification Ranges
Process	GMAW / FCAW	GMAW / FCAW
Process Type	Semi-Auto	Semi-Auto
Backing [metal, weld metal, flux, etc. (QW-402)]	Without / With	Without / With
Material Spec. (QW-403)	P1 to P1	P1 to P1
Thickness		
Groove	-----	.1875" - 8.00"
Fillet	-----	All
Diameter		
Groove	All	2 7/8" OD & Over
Fillet	All	All
Filler Metal (QW-404)		
Spec. No.	5.18 / 5.20	5.18 / 5.20
Class	ER70S-2/E71T-1MJH4	ER70S-2/E71T-1MJH4
F-No.	6 / 6	6 / 6
Deposited Weld Metal Thickness	GMAW= .125"	GMAW= .1375" Max.
Groove _____ Fillet _____	FCAW= 1.625"	FCAW= 8.00" Max.
Position (QW-405)	1G (Flat)	1G (Flat)
Weld Progression (QW-410)	Uphill/Downhill	Uphill/Downhill
Gas Type (QW-408)	75% Argon / 25% CO <sup>2</sup>	75% Argon / 25% CO <sup>2</sup>
Gas Backing <u>N/A</u>		
Electrical Characteristics (QW-409)		
Current	DC	DC
Polarity	Reverse	Reverse

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

Other: **Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 3/13/2017 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)**

**(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Francisco Morales Clock No. \_\_\_\_\_ Stamp No. E

Using WPS No. 151DCP Rev. 1 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	With /	Qualification Ranges
Process	<u>GMAW / FCAW / SAW</u>		<u>GMAW / FCAW / SAW</u>
Process Type	<u>Semi-Auto / Auto</u>		<u>Semi-Auto / Auto</u>
Backing (metal, weld metal, flux, etc. (QW-402))	<u>Without / With / With</u>	<u>With /</u>	<u>Without / With / With</u>
Material Spec. (QW-403)	<u>P1 to P1</u>		<u>P1 to P1</u>
Thickness			
Groove	<u>.750"</u>		<u>.1875" - 1.50"</u>
Fillet	<u>-----</u>		<u>All</u>
Diameter			
Groove	<u>-----</u>		<u>2-7/8" &amp; Over</u>
Fillet	<u>-----</u>		<u>All</u>
Filler Metal (QW-404)			
Spec. No.	<u>5.18 / 5.20 / 5.17</u>		<u>5.18 / 5.20 / 5.17</u>
Class	<u>ER70S-2 / E71T-1 / EM13K</u>		<u>ER70S-2 / E71T-1 / EM13K</u>
F-No.	<u>6 / 6 / 6</u>		<u>6 / 6 / 6</u>
Deposited Weld Metal Thickness			
Groove _____ Fillet _____	<u>GMAW= .125"</u> <u>FCAW= .3125"</u> <u>SAW= .4375"</u>		<u>GMAW= .1375" Max.</u> <u>FCAW= .625 Max.</u> <u>SAW= .875" Max</u>
Position (QW-405)	<u>1G</u>		<u>1G</u>
Weld Progression (QW-410)	<u>Uphill/Downhill/Downhill</u>		<u>Downhill</u>
Gas Typ (QW-408)	<u>75% Argon / 25% CO<sup>2</sup></u>		<u>75% Argon / 25% CO<sup>2</sup></u>
Gas Backing <u>N/A</u>			
Electrical Characteristics (QW-409)			
Current	<u>DC</u>		<u>DC</u>
Polarity	<u>Reverse</u>		<u>Reverse</u>

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

**Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

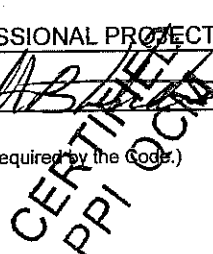
Organization: PROFESSIONAL PROJECTS, INC.

Date: 5/25/2016 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

\* No Consumable Inserts



**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name <u>Emmanuel Cruz</u>	Clock No. _____	Stamp No. <u>1</u>
Using WPS No. <u>149 DCP</u>	Rev. <u>2</u>	Date <u>5/28/2013</u>
the above welder is qualified for the following ranges		
<b>Variable</b>	<b>Record Actual Values Used in Qualification</b>	<b>Qualification Ranges</b>
Process	<u>GMAW / FCAW</u>	<u>GMAW / FCAW</u>
Process Type	<u>Semi-Auto</u>	<u>Semi-Auto</u>
Backing [metal, weld metal, flux, etc. (QW-402)]	<u>Without / With</u>	<u>Without / With</u>
Material Spec. (QW-403)	<u>P1 to P1</u>	<u>P1 to P1</u>
Thickness	_____	<u>.1875" - 8.00"</u>
Groove	_____	<u>All</u>
Fillet	_____	_____
Diameter	_____	_____
Groove	<u>All</u>	<u>2 7/8" OD &amp; Over</u>
Fillet	<u>All</u>	<u>All</u>
Filler Metal (QW-404)	_____	_____
Spec. No.	<u>5.18 / 5.20</u>	<u>5.18 / 5.20</u>
Class	<u>ER70S-2/E71T-1MJH4</u>	<u>ER70S-2/E71T-1MJH4</u>
F-No.	<u>6 / 6</u>	<u>6 / 6</u>
Deposited Weld Metal Thickness	<u>GMAW= .125"</u>	<u>GMAW= .1375" Max.</u>
Groove _____ Fillet _____	<u>FCAW= 1.625"</u>	<u>FCAW= 8.00" Max.</u>
Position (QW-405)	<u>1G (Flat)</u>	<u>1G (Flat)</u>
Weld Progression (QW-410)	<u>Uphill/Downhill</u>	<u>Uphill/Downhill</u>
Gas Type (QW-408)	<u>75% Argon / 25% CO<sup>2</sup></u>	<u>75% Argon / 25% CO<sup>2</sup></u>
Gas Backing <u>N/A</u>	_____	_____
Electrical Characteristics (QW-409)	_____	_____
Current	<u>DC</u>	<u>DC</u>
Polarity	<u>Reverse</u>	<u>Reverse</u>

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

Other: **Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

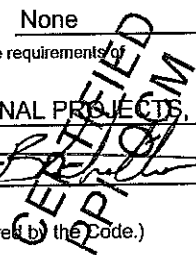
We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 6/23/2013 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the code.)

NOTE: Any essential variables in addition to those above shall be recorded.



**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Emmanuel Cruz Clock No. \_\_\_\_\_ Stamp No. 1

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Using WPS No. 151DCP Rev. 1 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	With /	Qualification Ranges
Process	<u>GMAW / FCAW / SAW</u>		<u>GMAW / FCAW / SAW</u>
Process Type	<u>Semi-Auto / Auto</u>		<u>Semi-Auto / Auto</u>
Backing (metal, weld metal, flux, etc. (QW-402))	<u>Without / With / With</u>	<u>With /</u>	<u>Without / With / With</u>
Material Spec. (QW-403)	<u>P1 to P1</u>		<u>P1 to P1</u>
Thickness			
Groove	<u>.750"</u>		<u>.1875" - 1.50"</u>
Fillet	<u>-----</u>		<u>All</u>
Diameter			
Groove	<u>-----</u>		<u>2-7/8" &amp; Over</u>
Fillet	<u>-----</u>		<u>All</u>
Filler Metal (QW-404)			
Spec. No.	<u>5.18 / 5.20 / 5.17</u>		<u>5.18 / 5.20 / 5.17</u>
Class	<u>ER70S-2 / E71T-1 / EM13K</u>		<u>ER70S-2 / E71T-1 / EM13K</u>
F-No.	<u>6 / 6 / 6</u>		<u>6 / 6 / 6</u>
Deposited Weld Metal Thickness			
Groove _____ Fillet _____	<u>GMAW= .125"</u>		<u>GMAW= .1375" Max.</u>
	<u>FCAW= .3125"</u>		<u>FCAW= .625 Max.</u>
	<u>SAW= .4375"</u>		<u>SAW= .875" Max</u>
Position (QW-405)	<u>1G</u>		<u>1G</u>
Weld Progression (QW-410)	<u>Uphill/Downhill/Downhill</u>		<u>Downhill</u>
Gas Typ (QW-408)	<u>75% Argon / 25% CO<sup>2</sup></u>		<u>75% Argon / 25% CO<sup>2</sup></u>
Gas Backing <u>N/A</u>			
Electrical Characteristics (QW-409)			
Current	<u>DC</u>		<u>DC</u>
Polarity	<u>Reverse</u>		<u>Reverse</u>

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

**Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

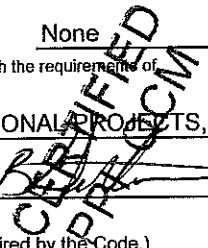
Organization: PROFESSIONAL PROJECTS, INC.

Date: 7/3/2016 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

\* No Consumable Inserts



**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Roberto Alvarez Clock No. \_\_\_\_\_ Stamp No. K

Using WPS No. 149 DCP Rev. 2 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	Qualification Ranges
Process	GMAW / FCAW	GMAW / FCAW
Process Type	Semi-Auto	Semi-Auto
Backing [metal, weld metal, flux, etc. (QW-402)]	Without / With	Without / With
Material Spec. (QW-403)	P1 to P1	P1 to P1
Thickness		.1875" - 8.00"
Groove	-----	All
Fillet	-----	
Diameter		2 7/8" OD & Over
Groove	All	All
Fillet	All	
Filler Metal (QW-404)		
Spec. No.	5.18 / 5.20	5.18 / 5.20
Class	ER70S-2/E71T-1MJH4	ER70S-2/E71T-1MJH4
F-No.	6 / 6	6 / 6
Deposited Weld Metal Thickness	GMAW= .125"	GMAW= .1375" Max.
Groove _____ Fillet _____	FCAW= 1.625"	FCAW= 8.00" Max.
Position (QW-405)	1G (Flat)	1G (Flat)
Weld Progression (QW-410)	Uphill/Downhill	Uphill/Downhill
Gas Type (QW-408)	75% Argon / 25% CO <sup>2</sup>	75% Argon / 25% CO <sup>2</sup>
Gas Backing <u>N/A</u>		
Electrical Characteristics (QW-409)		
Current	DC	DC
Polarity	Reverse	Reverse

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

Other: **Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 3/13/2017 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)  
NOTE: Any essential variables in addition to those above shall be recorded.

**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)**

**(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Roberto Alvarez Clock No. \_\_\_\_\_ Stamp No. K

Using WPS No. 151DCP Rev. 2 Date 2/12/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	With /	Qualification Ranges
Process	<u>GMAW / FCAW / SAW</u>		<u>GMAW / FCAW / SAW</u>
Process Type	<u>Semi-Auto / Auto</u>		<u>Semi-Auto / Auto</u>
Backing [metal, weld metal, flux, etc. (QW-402)]	<u>Without / With / With</u>	<u>With /</u>	<u>Without / With / With</u>
Material Spec. (QW-403)	<u>P1 to P1</u>		<u>P1 to P1</u>
Thickness			
Groove	<u>.750"</u>		<u>.1875" - 1.50"</u>
Fillet	<u>-----</u>		<u>All</u>
Diameter			
Groove	<u>-----</u>		<u>2-7/8" &amp; Over</u>
Fillet	<u>-----</u>		<u>All</u>
Filler Metal (QW-404)			
Spec. No.	<u>5.18 / 5.20 / 5.17</u>		<u>5.18 / 5.20 / 5.17</u>
Class	<u>ER70S-2 / E71T-1 / EM13K</u>		<u>ER70S-2 / E71T-1 / EM13K</u>
F-No.	<u>6 / 6 / 6</u>		<u>6 / 6 / 6</u>
Deposited Weld Metal Thickness			
Groove _____ Fillet _____	<u>GMAW= .125"</u>		<u>GMAW= .1375" Max.</u>
	<u>FCAW= .3125"</u>		<u>FCAW= .625 Max.</u>
	<u>SAW= .4375"</u>		<u>SAW= .875" Max</u>
Position (QW-405)	<u>1G</u>		<u>1G</u>
Weld Progression (QW-410)	<u>Uphill/Downhill/Downhill</u>		<u>Downhill</u>
Gas Typ (QW-408)	<u>75% Argon / 25% CO<sup>2</sup></u>		<u>75% Argon / 25% CO<sup>2</sup></u>
Gas Backing <u>N/A</u>			
Electrical Characteristics (QW-409)			
Current	<u>DC</u>		<u>DC</u>
Polarity	<u>Reverse</u>		<u>Reverse</u>

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

**Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

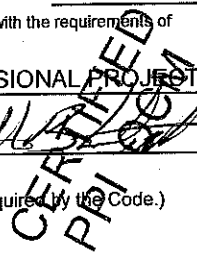
Organization: PROFESSIONAL PROJECTS, INC.

Date: 2/12/2013 By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

\* No Consumable Inserts



**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)  
(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Gerardo Perez Clock No. \_\_\_\_\_ Stamp No. Q

Using WPS No. 149 DCP Rev. 2 Date 5/28/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	Qualification Ranges
Process	GMAW / FCAW	GMAW / FCAW
Process Type	Semi-Auto	Semi-Auto
Backing [metal, weld metal, flux, etc. (QW-402)]	Without / With	Without / With
Material Spec. (QW-403)	P1 to P1	P1 to P1
Thickness		
Groove	-----	.1875" - 8.00"
Fillet	-----	All
Diameter		
Groove	All	2 7/8" OD & Over
Fillet	All	All
Filler Metal (QW-404)		
Spec. No.	5.18 / 5.20	5.18 / 5.20
Class	ER70S-2/E71T-1MJH4	ER70S-2/E71T-1MJH4
F-No.	6 / 6	6 / 6
Deposited Weld Metal Thickness	GMAW= .125"	GMAW= .1375" Max.
Groove _____ Fillet _____	FCAW= 1.625"	FCAW= 8.00" Max.
Position (QW-405)	1G (Flat)	1G (Flat)
Weld Progression (QW-410)	Uphill/Downhill	Uphill/Downhill
Gas Type (QW-408)	75% Argon / 25% CO <sup>2</sup>	75% Argon / 25% CO <sup>2</sup>
Gas Backing <u>N/A</u>		
Electrical Characteristics (QW-409)		
Current	DC	DC
Polarity	Reverse	Reverse

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory
Side Bend per QW462.2	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

Other: **Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

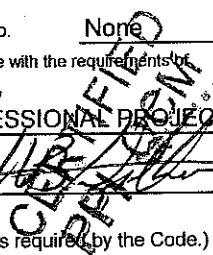
We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

Date: 5/29/2013

By: \_\_\_\_\_

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)  
NOTE: Any essential variables in addition to those above shall be recorded.



**QW-484 SUGGESTED FORMAT FOR MANUFACTURER'S RECORD OF WELDER OR WELDING  
OPERATOR QUALIFICATION TEST (WPQ)**

**(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)**

Welder Name Gerardo Perez Clock No. \_\_\_\_\_ Stamp No. Q

Using WPS No. 151DCP Rev. 1 Date 2/12/2013

the above welder is qualified for the following ranges

Variable	Record Actual Values Used in Qualification	With /	Qualification Ranges
Process	<u>GMAW / FCAW / SAW</u>		<u>GMAW / FCAW / SAW</u>
Process Type	<u>Semi-Auto / Auto</u>		<u>Semi-Auto / Auto</u>
Backing [metal, weld metal, flux, etc. (QW-402)]	<u>Without / With / With</u>	<u>With /</u>	<u>Without / With / With</u>
Material Spec. (QW-403)	<u>P1 to P1</u>		<u>P1 to P1</u>
Thickness			
Groove	<u>.750"</u>		<u>.1875" - 1.50"</u>
Fillet	<u>-----</u>		<u>All</u>
Diameter			
Groove	<u>-----</u>		<u>2-7/8" &amp; Over</u>
Fillet	<u>-----</u>		<u>All</u>
Filler Metal (QW-404)			
Spec. No.	<u>5.18 / 5.20 / 5.17</u>		<u>5.18 / 5.20 / 5.17</u>
Class	<u>ER70S-2 / E71T-1 / EM13K</u>		<u>ER70S-2 / E71T-1 / EM13K</u>
F-No.	<u>6 / 6 / 6</u>		<u>6 / 6 / 6</u>
Deposited Weld Metal Thickness			
Groove _____ Fillet _____	<u>GMAW= .125"</u> <u>FCAW= .3125"</u> <u>SAW= .4375"</u>		<u>GMAW= .1375" Max.</u> <u>FCAW= .625 Max.</u> <u>SAW= .875" Max</u>
Position (QW-405)	<u>1G</u>		<u>1G</u>
Weld Progression (QW-410)	<u>Uphill/Downhill/Downhill</u>		<u>Downhill</u>
Gas Typ (QW-408)	<u>75% Argon / 25% CO<sup>2</sup></u>		<u>75% Argon / 25% CO<sup>2</sup></u>
Gas Backing <u>N/A</u>			
Electrical Characteristics (QW-409)			
Current	<u>DC</u>		<u>DC</u>
Polarity	<u>Reverse</u>		<u>Reverse</u>

**Guided Bend Test Results QW462.2(a), QW462.3(a), QW462.3(b)**

Type and Figure No.	Results
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory
Side Bends per QW462.2(a)	Satisfactory

**Radiographic Test Results (QW304 & QW305)**

For alternative qualification of groove welds by radiography

Radiographic Results: \_\_\_\_\_

**Fillet Weld Test Results [See QW462.4(a), QW462.4(b)]**

Fracture Test (Describe the location, nature and size of any crack or tearing of the specimen) \_\_\_\_\_

Length and Per Cent of Defects \_\_\_\_\_ inches \_\_\_\_\_ %

Marco Test-Fusion \_\_\_\_\_

Appearance-Fillet Size (leg) \_\_\_\_\_ in. X \_\_\_\_\_ in. Convexity \_\_\_\_\_ in. or Concavity \_\_\_\_\_ in.

**Visual Examination - Satisfactory**

Test Conducted by: Professional Projects, Inc. Laboratory-Test No. None

We certify that the statement in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

Organization: PROFESSIONAL PROJECTS, INC.

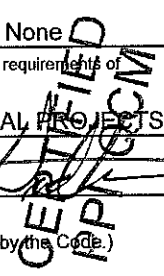
Date: 2/12/2013

By: *[Signature]*

(Details of record of tests are illustrative only and may be modified to conform to the type and number of tests required by the Code.)

NOTE: Any essential variables in addition to those above shall be recorded.

\* No Consumable Inserts





**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

List of Contents

Item: V-402, COLD SEPARATOR

# **Pressure Testing**

**Pg. 1**

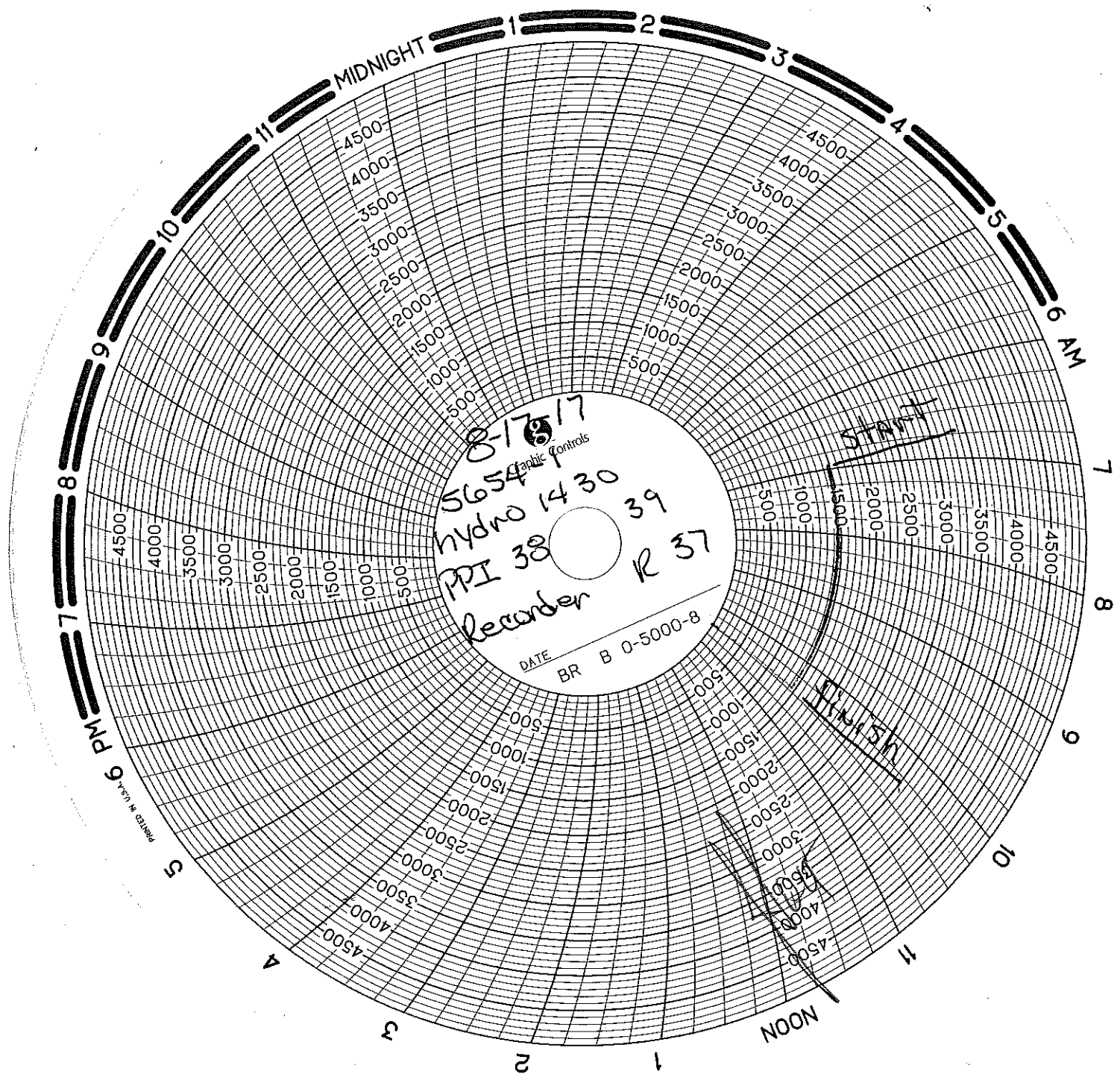
**Hydrostatic Pressure Chart**

**Pg. 2-4**

**Gauge Calibration Sheets**

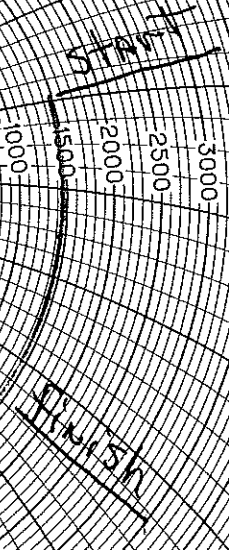
(PPI GAUGES: PPI-38, PPI-39 & RECORDER: R-37)

A handwritten signature in black ink, located in the lower right quadrant of the page. The signature is stylized and appears to be a name followed by a date, possibly 'J. [unclear] 1994'.



8-17-17  
5654  
Hydro 1430  
PPI 38  
Recorder R 37

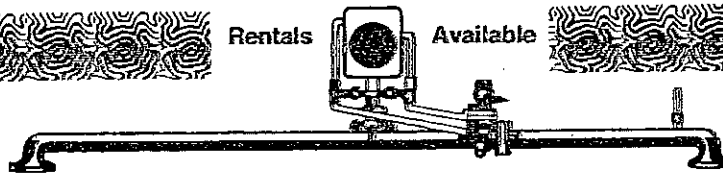
DATE  
BR B 0-5000-8



MADE IN U.S.A.

Rentals

Available



# JOHNNY'S GAUGE & METER REPAIRS

(713) 695-1038 • 718 DUNWOODY  
HOUSTON, TEXAS 77076-1914

## CALIBRATION CERTIFICATE

CUSTOMER Professional Projects, Inc.  
P.O. Box 618  
Cypress, Texas 77410

DATE CALIBRATED 2-01-2017  
OUR INVOICE NO. 4898  
CUSTOMER'S P. O. NO. \_\_\_\_\_

INDICATED RANGE 0-3,000# ACCURACY  $\pm$  0.5 % SERIAL NO. PPI-38

TYPE OF INSTRUMENT CALIBRATED 4<sup>1/2</sup>" McDaniel Pressure Gauge

TYPE OF STANDARD USED TO CALIBRATE Crosby Deadweight Tester  
S/N-39037

ALL STANDARDS DIRECTLY TRACEABLE TO  
NATIONAL INSTITUTE OF STANDARDS & TECHNOLOGIES TEST NO. 2.6/172409 & 6.6/139577

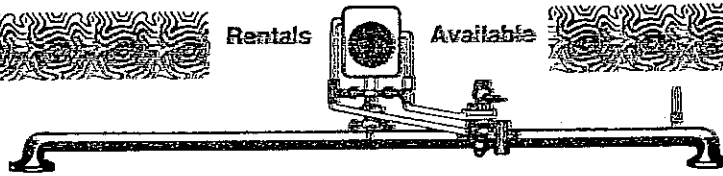
ROOM TEMPERATURE AT TEST 74 ° F

DATE OF CALIBRATION DUE 2-01-2018

INSPECTOR Fred Sull

Rentals

Available



# JOHNNY'S GAUGE & METER REPAIRS

(713) 695-1038 • 718 DUNWOODY

HOUSTON, TEXAS 77076-1914

## CALIBRATION CERTIFICATE

CUSTOMER Professional Projects, Inc.

P.O. Box 618

Cypress, Texas 77410

DATE CALIBRATED 4-27-2017

OUR INVOICE NO. 5193

CUSTOMER'S P. O. NO. \_\_\_\_\_

INDICATED RANGE 0-3,000# ACCURACY  $\pm$  0.5 % SERIAL NO. PPI-39

TYPE OF INSTRUMENT CALIBRATED 4 1/2" McDaniel Pressure Gauge

TYPE OF STANDARD USED TO CALIBRATE Crosby Deadweight Tester

S/N 39037

ALL STANDARDS DIRECTLY TRACEABLE TO

NATIONAL INSTITUTE OF STANDARDS & TECHNOLOGIES TEST NO. 2.6/172409 & 6.6/139577

ROOM TEMPERATURE AT TEST 74° F

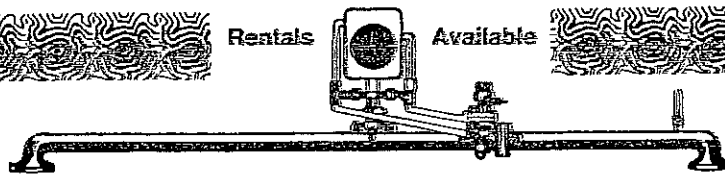
DATE OF CALIBRATION DUE 4-27-2018

INSPECTOR

*Fred Snel*

Rentals

Available



# JOHNNY'S GAUGE & METER REPAIRS

(713) 695-1038 • 718 DUNWOODY

HOUSTON, TEXAS 77076-1914

## CALIBRATION CERTIFICATE

CUSTOMER Professional Projects, Inc.  
P.O. Box 618  
Cypress, Texas 77410

DATE CALIBRATED 4-27-2017  
OUR INVOICE NO. 5193  
CUSTOMER'S P. O. NO. \_\_\_\_\_

INDICATED RANGE 0-5,000# ACCURACY  $\pm$  1.0 % SERIAL NO. R-37

TYPE OF INSTRUMENT CALIBRATED 8" Heco Pressure Recorder

TYPE OF STANDARD USED TO CALIBRATE Crosby Deadweight Tester  
S/N-39037

ALL STANDARDS DIRECTLY TRACEABLE TO  
NATIONAL INSTITUTE OF STANDARDS & TECHNOLOGIES TEST NO. 2.6/172409 & 6.6/139577

ROOM TEMPERATURE AT TEST 74 °F

DATE OF CALIBRATION DUE 4-27-2018

INSPECTOR

*Fred Sull*



**Professional Projects Inc.**

18115 Telge Rd. Cypress, TX 77429

## **5654-1 Databook**

List of Contents

Item: V-402, COLD SEPARATOR

# **Miscellaneous Certificates/ Reports**

<b>Pg. 1</b>	<b>Nameplate Photocopy</b>
<b>Pg. 2&amp;3</b>	<b>PWHT Calibration Sheet &amp; Chart</b>
<b>Pg. 4</b>	<b>Paint Report</b>

A handwritten signature in black ink, appearing to read 'J. Q. A. T.', is located in the bottom right corner of the page.

NB 3170

CERTIFIED BY



PPI PROFESSIONAL PROJECTS INC.

CYPRESS TEXAS

U  
W  
RT-1  
HT

MA 1100  
PSI AT  
TEMP -50  
YEAR 2017

PSI AT 150 °F  
PSI AT - °F  
°F AT 1100 PSI  
MFG. SER. NO. 5654-1

HEAD MAT SA-516-70N  
SHELL MAT SA-516-70N  
HYDR. TEMP 1430  
EST. WT 40,667 LBS

THK. 2.2262"  
2.5"  
.0625"

ITEM: V-402, COLD SEPARATOR

P.O.: 4500754097



W H LABORATORIES

8450 Rayson • Houston, Texas 77080 • 713/895-7504 • FAX 713/895-8906

Company: Tex-Fab, Inc.

Date: 03-15-2017

Lab Report #: 17-0314-16

Attention: Jay Johnson

P.O. #: \_\_\_\_\_

**TEMPERATURE MEASURING DEVICE CALIBRATION**  
**IN ACCORDANCE WITH WHL WORK INSTRUCTION CAL-103**

The chart recorder included in this report has been calibrated in accordance with ASTM and traceable to NIST using an Analogic Digi Cal II potentiometer S/N 7977, calibration due 04-27-2017.

Model and/or Make: 0-2000°F Honeywell

Serial, Identification # or Set #: 0848Y879399200001 #3

Date Calibrated: 03-15-2017 Next Due Date: 03-15-2018

Standard Temperature Reading °F	Instrument Reading °F		Deviation °F		After Calibration °F		Deviation °F	
	Chart	LED	Chart	LED	Chart	LED	Chart	LED
200	200	200	0	0	200	200	0	0
400	400	399	0	-1	400	399	0	-1
600	600	598	0	-2	600	598	0	-2
800	800	799	0	-1	800	799	0	-1
1000	1000	1000	0	0	1000	1000	0	0
1200	1200	1198	0	-2	1200	1198	0	-2
1400	1400	1400	0	0	1400	1400	0	0
1600	1600	1602	0	+2	1600	1602	0	+2
1800	1800	1800	0	0	1800	1800	0	0
2000	2000	1999	0	-1	2000	1999	0	-1

Comments: Satisfactory. Accurate to within ± 1% of full scale.

Date: 03-15-2017

Approved by: *Howard E. Heinsohn*

Howard E. Heinsohn



# CY-FAIR COATINGS, INC.

P.O. Box 1440  
Tomball, TX 77377-1440

Phone: (281) 351-7427  
Fax: (281) 378-4378

## Paint Report

Cy-Fair Job Number: 17262

Equipment Description: PPI S/O 5654-1 Item: V-402, COLD SEPARATOR

P.O.# 5654-9 Area: All External Surfaces

Surface Preparation: Spec. SSPC-SP- 6 Surface Condition Mill Scale

Date	Time	Temp. (f)	Rel. Humidity	Dew Point (f)
8/21/2017	9:45AM	89	64%	75

Anchor Pattern: 2.2 to 2.5 Measured by: Press-O-Film

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.2X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.5 X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.3 X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm

Coating Application: No moisture on surface and a minimum of 5 deg. F above dew point per Cy-Fair Coatings Procedure, Inc. C-001 Rev. 4.

AT	RH	DP	ST	Date	Type	Manufacturer and product	Batch / Lot number	DFT	Measured by
91	55%	73	93	8/21/2017	FAST CURE EPOXY	SHERWIN WILLIAMS MACROPOXY 646	A: XM1957MU	4.0	MikroTest Elektro- Physik
							B: XM2027VN	6.0	
Time: 14:35PM				1st					
95	46%	71	96	8/23/2017	FAST CURE EPOXY	SHERWIN WILLIAMS MACROPOXY 646	A: XM1957MU	4.0	MikroTest Elektro- Physik
							B: XM2027VN	6.0	
Time: 15:35PM				2nd					
93	48%	71	94	8/24/2017	ALPHATIC ACRYLIC POLYURETHANE	SHERWIN WILLIAMS HI- SOLIDS POLYURETHANE	A: XM0877RX	3.0	MikroTest Elektro- Physik
							B: MQ0587RK	4.0	
Time: 16:30PM				3rd					

Remarks: COLOR: STUCTURAL GRAY # 4031

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.4 X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.3 X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm

**Testex PRESS-O-FILM™ HT**  
www.testextape.com  
5654-1  
**2.2 X-Coarse**  
1.5 to 4.5 mil  
38 to 115 µm  
Made in USA  
115 µm