

WATER AND WASTEWATER TREATMENT SOLUTIONS

# ASHBROOK WINKLEPRESS®

## **OPERATIONS & MAINTENANCE MANUAL**

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### Warranty

ASHBROOK CORPORATION, warrants for a period of twelve (12) months from the date of start-up, not to exceed eighteen (18) months from date of shipment, the new equipment of its own manufacture to be free from defects in materials and workmanship under normal use and service when used and maintained in accordance with instructions supplied by Ashbrook. Ashbrook's obligation under this warranty being limited to repairing or replacing, at its option, any part found to its satisfaction to be defective, provided that such part is, upon request, returned to Ashbrook's factory, freight prepaid. This warranty does not cover parts damaged by decomposition from chemical action or wear caused by abrasive materials, nor does it cover damage resulting from misuse, accident, neglect or from improper operation, maintenance, installation, modification or adjustment. This warranty does not cover parts required outside Ashbrook's factory without prior written approval. Ashbrook makes no warranty as to starting equipment, electrical apparatus or other material not of its manufacture, since the same are covered by warranties of the respective manufacturer thereof.

This warranty excludes consumable parts, specifically chicane blades, seal strips, and scraper blades. These items are warranted for a period of thirty days from startup. Start up for the purpose of this agreement shall be the date when the equipment is first placed into operation regardless of the status of the other items, i.e. sludge feed systems, polymer feed systems, conveyors, etc. at that time.

Ashbrook shall not be liable for consequential damages, whether or not caused by seller's negligence. Consequential damages for the purposes of this agreement shall include, but not be limited to, loss or use, income or profit, or loss of or damage to property occasioned by or arising out of the operation, use, installation, repair or replacement of the equipment or otherwise.

All parts repaired or replaced under this warranty will continue coverage on a pro-rated basis of the original contract.

## **Commencement of Warranty Period**

The warranty period as offered by Ashbrook for this project will begin on the date in which the end-user (Owner) receives first beneficial use of the equipment. This may or may not coincide with the final acceptance of the equipment.

### Five Year Warranty

### **Bearings:**

All roller bearings supporting the pressure, drive and guide rollers shall be warranted for a period of five (5) years against failure. This warranty shall include all parts and labor for repairing or replacing any bearing, which fails during this period proving that the Owner lubricated said bearing with the recommended lubricant.

## Three-Year Warranty

### Rollers and Roller Coatings:

All rollers and coatings shall be warranted for a period of three (3) years against failure of the roller coating or the rollers themselves. Ashbrook shall repair or replace, labor inclusive, any roller coating which fails during this period.

#### Frame and Component Coatings:

The frame work and hot dipped galvanized coating shall be warranted for a period of three (3) years against all manufacturing defects. Any defects or corrosion of components shall be repaired or replaced at no additional cost to the Owner. Corrosion that may occur at places where the frame has been drilled or welded in the field is not covered.

## **Limited Belt Warranty**

ASHBROOK CORPORATION warrants that the belts furnished with our slurry dewatering equipment are free from defects in material and workmanship. Should there be a defect in material or workmanship, Ashbrook will replace such defective belts on a pro-rated basis on a normal usage rate of 2,000 operating hours per belt. This warranty covers the belts only and does not include installation.

The life of a belt is primarily dependent upon the nature of the slurry and the experience and the competency of the operator. Therefore, this warranty does not cover belts damaged by decomposition from chemical action or wear caused by abrasive materials, nor does it cover damage resulting from nuisance, accident, neglect or from improper operation, maintenance, installation, modification or adjustment.



### 2.0 GENERAL INFORMATION

### 2.1 GENERAL MECHANICAL DESCRIPTION

### 2.1.1 INTRODUCTION.

The Ashbrook Winklepress<sup>®</sup> leads the dewatering market in percentage of cake solids and throughput. Ashbrook Manufactures the Winklepress<sup>®</sup> from quality materials with tough corrosion resistant coatings, which results in years of dependable service and minimal maintenance.

### 2.1.2 MECHANICAL DESCRIPTION.

For simplicity's sake, the Winklepress<sup>®</sup> is described in its various functional groups as indicated below.

A.	Main Frame	H.	Gravity Drain Section
В.	Rollers	I.	Wash Stations
C.	Bearings	J.	Scrapers
D.	Steering Assemblies	K.	Drive Train
E.	Tensioning Assemblies	L.	Dewatering Belts
F.	Hydraulic Power Unit	M.	In-Line Mixer
G.	Feed System		

A. <u>Main Frame</u>: A self-contained, steel structure consisting of structural beam and plate side frames and cross members supporting the inner workings. The frame resolves the dewatering pressures into vertical loads, which are transferred to the foundation. While the frame maintains the structural integrity of the machine, it relies on the foundation to hold the machine level and preserve the alignment.

The Winklepress® may be supplied with various options. The optional integral stainless steel drainage sump allows installation of the press on a level, clean floor secured with anchor bolts (supplied by others) and ready for connection to drain piping.

B. <u>Rollers:</u> Fabricated assemblies, typically of double end plate, stub shaft construction, which provide a bearing surface for the belts. The roller shafts (journals) are machined on

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both ends to accept the roller bearings. All rollers are coated externally for corrosion resistance. Perforated rollers are also coated internally. The rollers may be any of the following types:

- (1) <u>Dandy Roller</u>. Perforated roller with internal scoops to channel captured filtrate away from the sludge.
- (2) <u>Drive Roller</u>. typically covered with ¼" Buna-N rubber, used to pull the dewatering belts through the machine.
- (3) <u>Plain Roller</u>. Any non-perforated roller of varying diameter with the job specified covering, typically nylon. Used for steering and tensioning assemblies, as pressure rollers, nip rollers, or as idler rollers to change belt directions. Nip roller(s) function by placing additional pressure on the sludge at the end of the high zone. In some processes, this will increase the final cake solids.
- C. <u>Bearings:</u> Support the rollers on both ends and maintain parallel roller alignment. The cast iron bearing housing is split horizontally to allow access to the bearing without disturbing the bearing alignment. All bearing housings incorporate a button-head grease fitting for maintenance purposes. The steering bearings are cylindrical bore, cylindrical roller bearings. All other bearings are cylindrical bore, double row, and spherical roller bearings. The bearing shaft seal is a triple seal comprised of the labyrinth and elastomer face seal and quad ring. For additional moisture protection, the seal features a shaft-mounted splashguard.
- D. <u>Steering Assembly</u>: Monitors the position of the dewatering belts and makes adjustments to maintain belt track in the center of the machine. The Winklepress<sup>®</sup> has a steering assembly, comprised of a steering roller and a hydraulic positioning unit, for each belt. The assembly works by moving one end of the steering roller so that the steering roller is at a small angle to belt. The belt responds to this change in direction and moves back to the center of the machine. The components of the steering assembly are:
  - (1) <u>Hydraulic Positioning Unit:</u> The unit has a belt position-sensing paddle that is constantly in contact with the belt. This paddle rotates a steering valve that controls the hydraulic steering cylinder. As the cylinder responds, the steering roller position is altered. The stainless steel sensing paddle has a ceramic wear plate to protect the belt edge.
  - (2) <u>Steering Roller:</u> The steering roller is a plain roller with steering bearings. The bearing housings is attached to the swivel plate to accommodate the roller movement.
- E. <u>Tensioning Assembly:</u> Consists of hydraulic cylinders, a rack and pinion alignment system and two positions, four-way control valve. For optimum performance, both belts on the Winklepress<sup>®</sup> are tensioned individually, independently. The belts may be tensioned or retracted at the control valve on the belt press; however the amount of belt tension is regulated at pressure valve on the hydraulic power unit. The individual tensioning components are as follows:

- (1) <u>Hydraulic Cylinders:</u> Responds to changes in pressure from the hydraulic power unit and pushes or pulls on the rack (lower belt) or pinion (upper belt) to decrease/increase belt tension. There is one hydraulic cylinder on each end of both tensioning rollers.
- (2) <u>Rack and Pinion System:</u> Ensures perfect parallel alignment of the tensioning rollers. The bearing pedestals which support the tensioning roller bearings are attached to a freely rotating shaft, which spans the machine width. There is a pinion gear attached to each end of the shaft. The two pinions ride on two racks which are attached to the main frame in perfect alignment. This system will not allow one side to advance faster than the other side and maintains absolute alignment when the system is not moving. The lower belt tensioning works under the same principal except that the rack moves and the pinions and shaft are fixed in position and only allow to rotate, The system maintains equal belt tension across the entire width of the belt.
- (3) <u>Control Valve</u>: A two-position, four-way valve which regulates the flow of the hydraulic fluid to the hydraulic cylinders in the tensioning and steering assemblies. The hydraulic lines connecting the valve to the tensioning cylinders have independent shutoffs to isolate the individual belts.
- f. Hydraulic Power Unit. A self contained unit which provides all hydraulic power for operation of the steering and tensioning assemblies. The unit consists of a 20 gallon reservoir, with externally mounted oil level, temperature, and pressure gauges. The pressure gauge is dual scaled for hydraulic pressure in pounds per square inch (PSI) and belt tension in pounds per linear inch (PLI). An externally mounted motor powers the pressure compensated hydraulic pump. The hydraulic pressure is adjusted by regulating the pressure relief on the unit. Hydraulic oil is filtered through the externally mounted return filter and through an internal filter on the suction side of the pump. The reservoir is drain valve for maintenance purposes.

Depending upon the specific site installation, a multi stage hydraulic unit may be supplied. This unit contains one motor which drives one or more pumps. The additional pump(s) are used in conjunction with the flow splitting devices to provide independent belt tension circuits, belt steering as well as a separate circuit for the optional nip roller(s). The nip roller exerts additional pressure on the sludges at the end of the pressure zone

- g. <u>Feed Assembly.</u> Stainless steel chute which distributes the flocculated sludge across the belt to begin gravity dewatering. The feed chute has a standard ANSI flange for connecting to the sludge feed line.
- h. <u>Gravity Drain Section.</u> Consists of the drainage grids, the Ashbrook patented chicanes, the drainage trays and piping and the sludge restrainers. The components of the Gravity Drainage section are as follows:

- (1) <u>Drainage Grids:</u> Series of polyethylene strips arranged in a "V" pattern which support the dewatering belts. The strips are installed on stainless steel grid above the drainage trays. The polyethylene provides a low friction wear surface for the belts.
- (2) <u>Vertical Wedge</u>: A fixed grid attached to the frame and a moveable grid hanging from the frame, both fitted with polyethylene strips arranged in a "V" pattern. The wedge grids are oriented vertically with the larger opening at the top. The sludge flows from top to bottom and is de-watered by gravity and low pressure in this area as the sludge is mildly squeezed between both belts by the grids. For process flexibility, both the top and bottom openings are adjustable. Flexible seals at both sides of the belt in the wedge secure the sludge from being squeezed out from between the belts.
- (3) <u>Chicanes:</u> Ashbrook Corporation's patented plows that turn the sludge and provide clear openings for the free water to drain into the drain pans. The chicanes pivot independently on the support bar, which allow them to float directly on the belt and ride smoothly over the belt seam. This minimizes belt wear and prevents obstructions from blocking the sludge flow.
- (4) <u>Drainage Trays:</u> Assortment of stainless steel pans which collect the filtrate for piping to the machine sump. The piping is designed to be self-venting to provide maximum drainage flow.
- (5) <u>Sludge Restrainers:</u> Stainless steel guides that prevent sludge from running off the sides of the dewatering belts. The sludge restrainers are fitted with a neoprene strip at the bottom to maintain the seal between the belt and the sludge restrainer.
- i. <u>Wash Stations.</u> Two slotted stainless steel boxes containing the wash tube. The wash tube generates an overlapping spray pattern from the jet nozzles to blast embedded and surface particles from the belt. The wash tube has an internal brush for cleaning the nozzles while the machine is running. The wash station entry and exit slots are covered with neoprene seals to protect the belt and to prevent over-spray from the wash box. Each wash box is drained individually.
- j. <u>Scraper (Doctor) Blades</u>. Steel assemblies fitted with polyethylene blades, which remove the dewatered sludge cake from the dewatering belts. The scrapers are spring tensioned for pre-load adjustment. The proper tension is set at the factory and requires no field adjustment.
- k. <u>Drive Train.</u> Powers the Winklepress<sup>®</sup> by turning the drive rollers, which pull the dewatering, belts through the press. The drive train components are the two motor driven helical gear reducers connected in parallel to one variable frequency motor speed controller. See the Drive Section of this manual for more detailed information on the drive motors and gearboxes provided with this unit. The parallel wiring situation ensures adequate speed matching of the motors leading to properly matched roller rotation. The drive train receives its initial input from a variable speed drive unit. This allows the speed of belts to be varied from approximately one to six meters per minute. Belt speed will depend upon the type of dewatering process desired. The drive gearbox has its own splash lubrication system.

- l. <u>Dewatering Belts.</u> Polyester woven mesh joined by a stainless steel clip form an endless band.
- m. <u>In-Line Mixer.</u> Self-cleaning variable orifice venturi mixer used to condition the sludge prior to dewatering. The mixing energy may be varied independently of the flocculation by moving the mixer arm and counterweight. This independent adjustment results in he lowest polymer usage of any belt press on the market.

### 2.2 GENERAL PROCESS DESCRIPTION

### 2.2.1 INTRODUCTION.

Ashbrook's dewatering equipment is designed for use in municipal, industrial or specialized applications where removal of a liquid (usually water) from a solid-liquid suspension, slurry, is desirable. The Winklepress® Belt Filter Press does this through the use of two porous belts, which allow both gravity and pressurized dewatering. In the gravity stage, the sludge is allowed to thicken and most of the filtrate, water, is removed. During the pressure filtration stage, the sludge is also exposed to shear forces, which greatly increase filtration. The filtrate removed is captured and piped to the base of the machine. This water which has a very low solids content due to the superior capture rate of the Winklepress®, is often drained back to the head of the plant. In some instances, the filtrate may be recycled as belt wash water. The discharge of the machine is a friable cake with a greatly increased solids content.

### 2.2.2 DEWATERING PROCESS

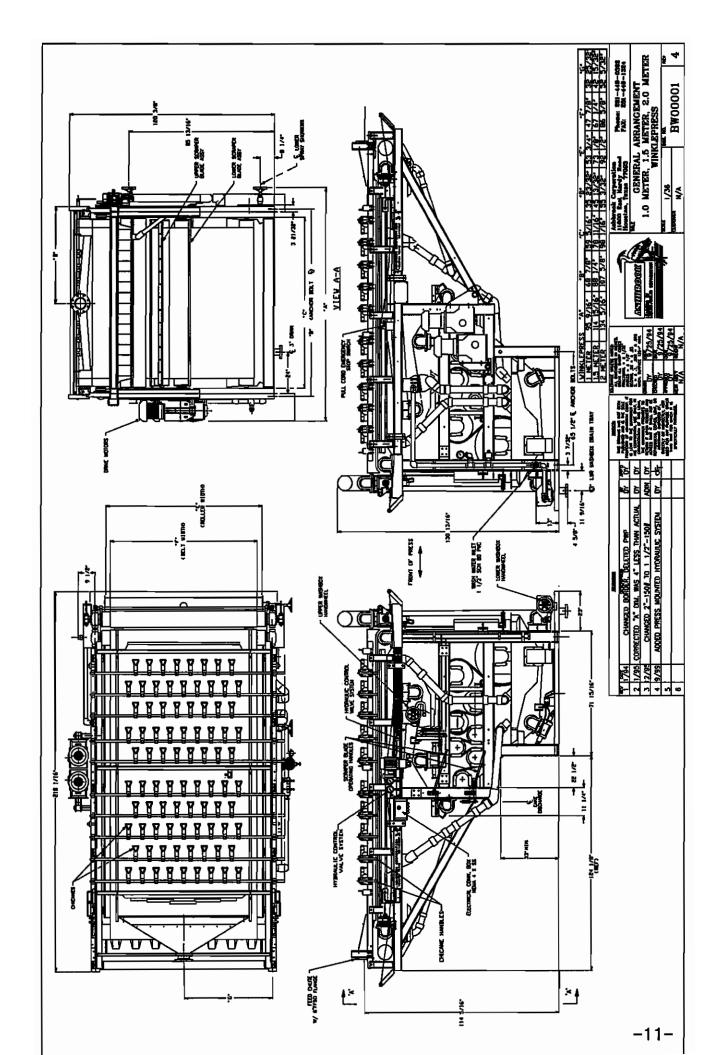
Prior to filtration, the sludge must be conditioned to cause solid particle agglomeration or clumping. This process, called flocculation is accomplished by injecting a polyelectrolyte, or polymer, into the slurry. Since most slurries are charged, it is important to select the proper type of polymer to neutralize the charge. As the nature of flocculated sludge controls to some extent the dewatering characteristics of that slurry, polymers of varying charge, strength, and molecular weight should be tested. The Ashbrook laboratory can assist by analyzing individual slurries and recommending the optimum polymer and dosage. Along with the type of polymer, mixing energy and retention time play a major role in the flocculation process. For this reason, the Ashbrook system of polymer injection and in-line mixing is designed for maximum flexibility. Ashbrook typically supplies one in-line variable orifice mixer and polymer injection ring per machine. We recommend that three polymer injection locations in the sludge feed line be established. The locations should be selected to allow 15, 30 and 45 seconds retention time before the polymer sludge mixer enters the Winklepress<sup>®</sup>. These locations allow the mixer/polymer injection ring to be relocated easily should more or less retention time be required for optimum dewatering. To remix flocculated sludge is counter-productive, so the unused locations should be fitted with spool pieces of nominal size.

The flocculated sludge is discharged from the feed line onto the Winklepress® through an inlet distributor. This inlet spreads the sludge across the entire machine width to allow optimum gravity dewatering. The sludge from the feed pipe hits a disc shape baffle before it discharges onto the sludge feed box. The baffle dissipates the sludge feed energy. An adjustable spreader door controls the sludge level in the feed box. The sludge distributes to the gravity belt uniformly through the bottom opening between the spreader door and belt by a constant head across the width of the belt. The depth of sludge in the feed box area shall be 2.5-4.5", which can be adjusted by turning the spreader adjustment

arm to increase or decrease the opening of that spreader door. Cautions shall be taken to prevent the sludge from overflowing or running dry in the feed box area. During the dewatering process, sludge is conveyed on a porous weave belt. The belt allows the free water to pass through where it is captured by drain pans and piped to the machine base. The sludge is prevented from running off of the sides of the Winklepress® by sludge restrainers and rubber seals. As the sludge is moved through the gravity section, it is turned over by Ashbrook's patented Chicanes. These plow-like devices greatly increase the gravity dewatering by clearing places for the water to drain as they turn the sludge mass. At the end of the gravity section, the sludge is loosely structured cake ready for the pressure dewatering.

The vertical wedge section uses the natural effects of gradually increasing pressure imposed by gravity on the depth and weight of sludge, this zone further reduces the volume of suspension in preparation of pressing. At this point the two belts begin to converge compressing the sludge. The first roller encountered in this stage is Ashbrook's Dandy Roller. This perforated roller has internal scoops to channel captured filtrate away from the sludge. As the belts travel past the Dandy Roller, they take an S-shaped path around rollers of progressively decreasing diameter. This increases both the pressure and the shear-action to the sludge. The group of smaller diameter rollers is the high-pressure section of the dewatering process. The shear-action, in this section, turns the sludge mass within the belts exposing the wet inner cake to the belts and expelling the free water. At the end of these rollers the belts separate and the sludge cake is discharged from the machine.

The belts continue past scrapers that remove any residual cake and prepare the belts for cleaning. The belts are washed in separate wash stations that remove any particles that may have embedded in the porous belt. The belts must be continually cleaned to prevent belt binding and a loss of dewatering ability. The clean belts exit the wash stations to begin the process again.





### 3.0 RECEIVING

Thoroughly inspect the equipment before accepting shipment from the transportation company. If any item on the Bill of Lading is damaged or missing, ensure an annotation is made on the Freight Bill or Express Receipt. If any concealed damage is discovered after unloading, notify the transportation company and request an inspection.

Ashbrook inventoried and packaged the spare parts required for your order prior to shipment. To ensure inventory accuracy, we request the packaged labeled "Spare Parts" not to be opened until the Ashbrook Service Technician arrives. If the box is opened prior to arrival, Ashbrook will not assume liability for any missing parts.

Ashbrook will assist your efforts to collect claims for loss or damage in transit. Should there be any loss or damages please notify Ashbrook within three (3) working days of delivery. Ashbrook's assistance does not relieve the transportation company of any responsibility for reimbursement on your claim and in no instance assumes liability on the part of Ashbrook for the claim.

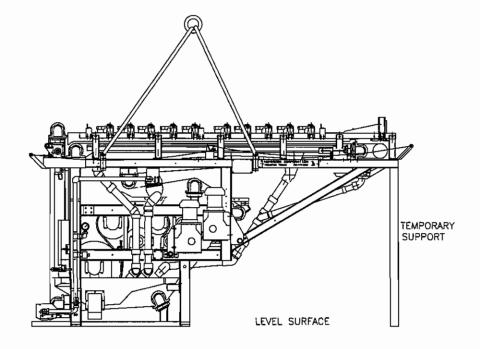
Claims for loss or damage in transit do not alter the payment terms for your order and payment should not be withheld or delayed because of a claim.



### 4.0 HANDLING INSTRUCTIONS

The press should be lifted using 2 spreader beams to avoid putting a horizontal force on top of the frame slide plates. If spreader beams are not available then insert a 4x4 timber of a length equal to the distance between the side plates between the frame side as near the lifting points as possible. Use four chains or cables of 8 foot minimum length to attach to the lifting points on the frame lifting lugs.

- 4.1 Care must be taken that the lifting forces are transmitted vertically to the frame lifting lugs only. Do not lift by any other point on the press.
- 4.2 Precautions must be taken to prevent overload to the machine or the lifting equipment due to acceleration, deceleration or shock forces. The machine must be lowered carefully to rest on a level surface with its weight evenly distributed on the supports.
- 4.3 Loose ship items such as the belts, in line mixer, booster pumps, etc. will be consolidated and crated for shipment. All crates should be lifted from the bottom only using a fork lift or slings.





### **5.0 STORAGE**

Ashbrook recommends indoor storage for all items, however we recognize this may not be possible. If limited indoor storage is available, we recommend storing the electric control panel, the crate of spare parts, the hydraulic power unit and drive motors, if shipped loose, indoors. Additionally the following steps should be taken for all storage locations.

- 5.1 Store the press in a level position supported on wooden dunnage.
- 5.2 Completely cover the press with a well secured waterproof tarpaulin in an area free of extreme temperatures, moisture, shock and vibrations.
- 5.3 Do not store items on top of the press.
- 5.4 Periodically inspect the roller spindles, gears, etc. for rust. Keep these items well lubricated to prevent rusting.
- 5.5 Bearings are greased when they leave the factory. No additional greasing is necessary for storage.
- 5.6 The gearboxes are shipped completely filled with oil. No additional oil is required for storage. However, they must be drained to the proper level before starting.
- 5.7 The hydraulic power unit and drive motor (if shipped loose) should be stored in a clean, dry area protected from extreme temperatures, moisture, shock, and vibration.
- 5.8 Rotate all rollers two or three revolutions by hand every thirty- (30) days.
- 5.9 The box labeled "Spare Parts" should be stored indoors and not opened until the Ashbrook service representative comes for the start up.

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### **6.0 INSTALLATION INSTRUCTIONS**

6.1 GENERAL: The proper design and construction of the foundation, sump, piping, pumps and other ancillary equipment operated with the Winklepress<sup>®</sup> is the responsibility of the owner, engineer or contractor unless arranged otherwise at the time of purchase. These instructions are intended as a guide based on sites with configurations similar to those recommended by Ashbrook. Since they are general, some modifications may be required to solve your unique requirements. Should assistance be required, please contact Ashbrook's Engineering or Service Department.

## 6.2 INSTALLING THE WINKLEPRESS®:

- 6.2.1 Study applicable plans to verify location of press. Confirm the machine orientation in this manual matches the hook up locations in the plans including wash water, electric, sludge feed, and polymer.
- 6.2.2 Verify cast in place anchor bolt locations from the General Arrangement Drawings. If anchor bolts are expansion anchors, they will be installed after press is set on piers.
- 6.2.3 Lift press according to Handling Instructions and carefully set it in place.

## CAUTION: Ensure lifting safety is observed during all hoisting operations

- 6.2.4 Loosely secure anchor bolts. If expansion anchors are to be used:
  - a. Mark their locations while Winklepress® is in place.
  - b. Remove Winklepress<sup>®</sup> following Handling Instructions.
  - c. Drill and install expansion bolts.

*Note:* Drilling the anchor bolts while the Winklepress<sup>®</sup> is in place could damage the frame's protective coating or cause alignment problems.

- d. Replace the Winklepress® following Handling Instructions.
- e. Loosely secure the anchor bolts.
- 6.2.5 Level the Winklepress®:
  - a. Using a precision level, check across the frame to ensure

the machine is level.

b. Shim the Winklepress® around the anchor bolts until all of the above rollers are level.

*Note:* Do NOT shim any roller. Shimming the roller could cause premature bearing failure or belt alignment problems and void the Ashbrook warranty.

c. Tighten the anchor bolts.

6.2.6 Verify rollers remained level by checking the same rollers again. Check machine for level lengthwise by taking an elevation at the four corners.

6.2.7 Relevel the machine as required.

6.2.8 Grout the machine as applicable using a non-shrink, nonetallic grout.

6.3 Connect Wash Water: Water should be provided to the wash boxes at 85 psi and the following flow rates: One Meter, 40 gpm; One and One-Half Meter, 60 gpm; Two Meter, 80 gpm. If the water pressure or flow is not sufficient for the above requirements, then a booster pump is required. The wash water connection will be a 1.5 inch diameter Schedule 80 PVC unless otherwise specified. Ashbrook recommends a ball valve be installed prior to any booster pump required and a pressure gauge be installed prior to the press to verify pressure requirements.

6.4 Connect Sludge Feed Line: The sludge feed line will be connected to the Winklepress<sup>®</sup> feed box as shown on the General Arrangement Drawing in this manual. Use a flexible connection to allow for adjustment of the feed box. The feed box is supplied with a standard ANSI 150 lb. raised face flange unless otherwise specified. The 2.0 meter and the 1.5 meter Winklepress<sup>®</sup> have a six inch diameter feed chute inlet, and the 1.0 meter Winklepress<sup>®</sup> has a four inch diameter feed chute will be supplied (standard, unless otherwise noted). Ensuring the sludge is fed evenly across the belt width is critical to the performance and maintenance of the belt press. Because of this, Ashbrook recommends eight feet of straight feed piping prior to the feed box. Additionally, sharp turns in the feed line should be avoided by using long radius elbows.

6.5 Install In Line Mixer: The Ashbrook In Line Mixer should be installed initially at the location that will allow 30 seconds retention time or as recommended by Ashbrook's Process Engineers. Ensure the directional arrow on the mixer points in the direction of the sludge flow. The polymer injection ring should be installed between the inlet flange of the mixer and the sludge feed pipe. Connect the injection ring to the splitter manifold via four lengths of clear hose. Connect the splitter manifold to the polymer system according to the polymer system manufacturer's instructions.

6.6 Electrical Hook-Ups: Electrical interconnection of the Winklepress® is always through a dedicated control panel. It is often the case that all required motor starters and or drives are integrated with the operating logic into a single panel. In this case, it will only be necessary to perform all interconnection wiring between the press and the panel as described by the terminal strip diagrams found in the as built control panel drawings. It is also possible that the control panel may contain only operating logic and all starters

are at a motor control center or that other equipment must be interlocked with this panel. Once again, the as built drawings will provide interconnection guidance. On the WinklepressWPN®, all control wiring is terminated in the junction box on the machine. To complete the installation, the following connections are required:

**WARNING**: Electrical connections should only be attempted by a qualified electrician. All electrical work must be in compliance with NEC, NEMA, OSHA and other local codes. Serious personal injury, fatalities or equipment damage could result from improper electrical connections.

- 6.6.1 Winklepress® Junction Box: The machine is shipped pre-wired. The installing contractor is responsible for interconnecting the junction box and the control panel as indicated on the as-built electrical drawings. Be certain to seal the conduit entry point to the junction box to prevent water entry. The conduit entry should always be in the bottom of the junction box when possible.
- 6.6.2 <u>Winklepress® Drive Unit:</u> Consult the Drive Section of this manual for the electrical requirements of the specific drive motor provided. The connection will be made at the junction boxes on the machine's drive motors.
- 6.6.3 <u>Hydraulic Power Unit</u>: The motor is a 230/460 volt, 60 Hz, 3 phase, 1.0 horsepower unit unless otherwise indicated in the hydraulic unit section of this manual. Electrical connection will be at the motor junction box. The connection information is on the inside cover of this box. The hydraulic unit will also have a low pressure switch which has been pre wired to the press junction box.



### 7.0 MECHANICAL START-UP PROCEDURES:

**7.1 GENERAL:** Prior to attempting dewatering for the first time, the Winklepress<sup>®</sup> must be inspected and prepared for operation. This section addresses the procedures, which will prepare the machine for operation.

### 7.2 MECHANICAL CHECKOUT:

- 7.2.1 Visually inspect anchor bolts and verify they are tightened.
- 7.2.2 Verify the machine is level.
- 7.2.3 Inspect the rollers:
  - (a) Verify rollers are level across the machine width.
  - (b) Check for cleanliness. Remove any construction materials, packing materials, dirt, grease, etc.
  - (c) Turn each roller by hand two or three revolutions.

### Note: The seals should drag slightly and the drive rollers should not turn.

- (d) If any roller turns roughly or sticks, inspect the roller for external obstructions. If no obstructions exist, disassemble the bearing housings and inspect the bearings. If damaged, notify Ashbrook for repair or replacement.
- (e) Inspect the roller coatings. All coatings should be intact.

### 7.2.4 Inspect the gravity drainage grids:

- (a) Grids should be level and free from any sharp edges or protrusions.
- (b) Grids should be free of embedded materials and all bolt heads should be well below plastic wear surface.
- (c) Sludge restrainers should be in place and the rubber seal should be intact. Remove any sharp edges. Rubber seals will wear with use. As they wear, adjust them to maintain adequate sealing and if necessary replace them.
- (d) Chicanes blades should be resting on the grids. No metal portion of the chicane assembly should be touching the grids.
- (e) Verify the scrapers pivot freely and that the plastic blades are not chipped, cracked, or broken.

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- 7.2.5 Inspect wash boxes and verify rubber seals are in place:
  - (a) The rubber seals located at the wash boxes will wear with use. As they wear, adjust them to maintain adequate sealing and if necessary replace them.

### **7.3 ELECTRICAL CHECK OUT:**

**WARNING:** A qualified electrician should only check electrical connections. Failure to follow federal, state or local codes could cause severe personal injuries, fatalities or severe equipment damage.

7.3.1 Hydraulic Power Unit: Bump the motor circuit to ensure motor is turning in the correct direction.

**Caution:** Ensure unit is filled with hydraulic fluid. Severe equipment damage could result if unit is operated without oil.

7.3.2 Drive Unit Inspection: Bump the drive unit circuit to ensure drive rollers turn in the correct directions.

**Caution:** Ensure gearbox is drained to operating level before operating drive unit. Damage to the drive unit could occur if unit is operated before being drained to the correct level.

7.3.3 Wash Water Booster Pump: Bump the motor circuit to ensure motor is turning in the correct direction.

**Caution:** Ensure pump is primed or is self-priming. The pump could be damaged if operated without being primed.

- 7.3.4 Electrical Sensors: Inspect all sensors to ensure they shut down the appropriate machine functions. Depending on your particular installation, some of the following machine sensors and alarms may not be present. However, they are included as an indication of the full capability of the machine. When triggered, the sensors will cause the Winklepress® to have a total or a partial shut down as indicated below:
- (a) Total Shut Down: All machine functions, sludge and polymer feed systems, hydraulic power unit and wash water system are stopped if not in the Bypass Mode. This results from the following alarm conditions:
  - (1) Belt Breakage: proximity switch, which detects a broken belt.

- (2) Belt Misalignment: two limit switches, which detect gross misalignment of the belts on either side.
- (3) Low Wash Water Pressure: a pressure switch, which detects water pressure below the owner specified setting, typically 60 psig.
- (4) Hydraulic Temperature: a temperature switch that detects hydraulic fluid temperature above 175°F at the hydraulic power unit.
- (5) Hydraulic Pressure: pressure switches which detect hydraulic pressure too low to maintain drive traction and belt alignment.
- (6) Emergency Stop: a push button on the machine and other optional location(s) to manually stop all functions.
- (7) Emergency Trip Cord: a pull cord circling the machine, which functions as an emergency stop.
- (b) Partial Shut Down: shuts down sludge and polymer feed and continues to operate the belt drive, hydraulic power unit and wash water system for a period of one hour. This results from:
  - (1) High Sludge Level: a level sensor which detects sludge about to overflow the edge of restrainers in the gravity section.
  - (2) Lack of Cake: a level sensor, which detects a lack of sludge in the gravity section.

Caution: Alarms and sensors are on the machine to protect personnel and the equipment.

Operating the machine with sensors not functioning properly places the operator and equipment in danger.

### 7.4 HYDRAULIC SYSTEM CHECK OUT:

- 7.4.1 Verify all hydraulic lines between hydraulic power unit and the Winklepress® are in place.
- 7.4.2 Put the control valves on the Winklepress® in the retract position.
- 7.4.3 Energize the hydraulic power unit. The pump may take up to 90 seconds to reach full pressure, which will register on the pressure gauge.

Note: If the pump has not picked up pressure within 90 seconds, turn off pump motor and check for correct pump rotation and fluid level.

- 7.4.4 With the pump operating, turn the regulator knob on the pump to adjust the lower belt tension. Observe the gauge for the lower belt and set pressure to around 350 psi.
- 7.4.5 Adjust the upper belt tension by turning the knob of the valve in the end of the manifold block. Observe the gauge for the upper belt and set the pressure to around 300 psi. By design, the upper belt tension pressure cannot be set higher than the lower belt tension.
- 7.4.6 Push in both control valve knobs on the manifold to extend the belt tensioning cylinders. (Pressure may be varied according to cake solids requirements)
- 7.4.7 Check the belt press hydraulic power unit for leaks. Repair if required.
- 7.4.8 Cycle both rollers through the tension/retract cycle several times to ensure they function correctly and to purge air from the system.

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- 7.4.9 Inspect steering sensing paddle for damage, and freedom of movement. If its movement is stiff notify the Ashbrook Service Department.
- 7.4.10 Manipulate the valve by manually moving the sensing paddle off center in one direction. The hydraulic positioning unit should move fully in one direction in response to the sensing paddle. Move the paddle off center in the other direction and note the movement of the hydraulic positioning unit in the other direction.
- 7.4.11 If equipped with the Nip Roller option, verify that both cylinders are operating correctly and uniformly to move the nip roller toward the bottom pressure roller. There must be a uniform space of 3/8 inch between the nip roller and the bottom pressure roller. The hydraulic pressure for the nip roller should be initially set at 100psi. The normal operating pressure range for the nip roller is from 100 to 350 psi.

### 7.5 WASH WATER: Inspect the following items:

- 7.5.1 Verify the wash water is being delivered to the wash boxes at 85 psig or higher and at the correct flow rates. If a booster pump is installed, ensure pump is functioning correctly.
- 7.5.2 Verify all valves in the water line are open.
- 7.5.3 Verify hand wheels on both wash tubes are fully closed. Rotate completely in the counter clockwise direction and then back fully in the clockwise direction. This action rotates the brush inside the wash tube and cleans the spray nozzles.

**NOTE**: Do NOT over tighten hand wheel. This could damage the internal seals causing a loss of wash water pressure. Should water continue to drain from the bypass hose it is likely that gravel or trash is preventing the valve from closing. In this case repeat the opening and closing cycle of the valve to clear it.

7.6 DEWATERING BELT INSTALLATION: The dewatering belt is one of the most easily damaged items on the Winklepress<sup>®</sup>. Because of this, it is important to know how to handle the belt prior to attempting installation.

### 7.6.1 Handling and Storage:

- (a) Always store belts in their protective wrappers or containers standing on end.
- (b) Do not smash, stack or store items on the rolled belts.
- (c) Do not allow the belt to become kinked or folded.
- (d) Keep foreign substances off the belts as much as possible.
- (e) Never attempt to dewater sludge with a new belt before performing the run-in on the press as described in Section 7.7.

7.6.2 <u>Belt Safety:</u> Installing belts on a new machine where there are no belts being replaced is a job that requires two people working together using much care and patience.

WARNING: ATTEMPTING TO USE THE PRESS BELT DRIVE TO INSTALL A NEW BELT IS EXTREMELY DANGEROUS. DO NOT ENERGIZE THE DRIVES TO TRY TO MAKE THE BELT INSTALLATION GO FASTER. TO DO SO CAN RESULT IN SERIOUS INJURY OR DEATH. LOCK OUT THE DRIVE WHEN INSTALLING BELTS ON A NEW MACHINE.

The first belts to be installed on the Winklepress<sup>®</sup> MUST BE fed by hand. Two people working together can work the belt around the rollers by pulling the slack from one roller to the next. But, when old belts are being replaced it is acceptable to part the old belt and attach the new belt to the old at the clipper seam and then use the press drive at low speed to pull in the new belt while the old belt is fed out. (See SK001935)

In either case, keep your hands away from the belts where they go around rollers or through wash boxes and other pinch points.

To ensure safe operation observe the following:

- (a) Stop Switches: Ensure location and operation of the stop switches for the drive and hydraulic unit are known and that all switches function properly
- (b) Remember, even though the belt moves slowly it can catch clothing, hands, jewelry, etc. Remove jewelry and fasten clothes to protect yourself.
- (c) The hydraulic system also moves slowly, but with bone crushing force. DO NOT ever place body parts between the moving machine parts.

### 7.6.3 Belt Installation: READ THE PROCEEDING SECTION FIRST!

- (a) Lift the chicanes off the grid bars by rotating their lifting handles and raise the sludge restrainers to make clearance between the seals and the grid bars.
- (b) Loosen the upper and lowers wash box seal panels and retract to make a larger opening.
- (c) Unwrap the belts and record the serial numbers on the Belt Record Sheet.
- (d) Remove the joining wire from the belt seam.
- (e) Position the belts at the wedge end of the machine.

**Note:** The smooth (flattened) side of the belt faces the sludge. Turn the rough side toward the rollers. The Ashbrook warranty does not cover belts that have been installed improperly.

(f) Feed the lower belt over the top of the tensioning roller down through the wedge, and under the perforated dandy roller.

- (g) Ensure the belt is feeding squarely. Any kink, crease or wrinkle in the belt must be avoided or the belt could be damaged when placed in service under tension.
- (h) After straightening the belt, continue the belt through the pressure rollers, through the lower wash box and down around the lower steering roller.
- (i) At this point it is allowed to energize the drive momentarily to bring the belt through the machine so the ends can be joined at the wedge end of the machine where the belt is vertical.
- (j) Observe the safety precautions above and lock out the drive once the belt is in position for seaming.
- (k) Join the two ends of the belt and thread the splice wire through the loops. Ensure the thread wire does not miss any loops and catches each loop alternately. Ensure the belt edges are in line and do not form a step at the joint.
- (l) Bend the wire into a loop and feed it back into the belt loops. Cut off the excess wire.
- (m) Begin feeding the upper belt over the upper tensioning roller over the gravity grids and down through the wedge and under the perforated dandy roller.
- (n) Work the belt through the pressure section by pulling the slack from roller to roller.
- (o) Pass the belt through the upper wash box and under the upper steering roller.
- (p) Pull the upper belt up around the upper tensioning roller to the gravity deck.
- (q) Pull the other end of the belt up to where the ends come together on top of the upper tensioning roller; where it will be accessible for seaming.
- (r) Join the two ends of the belt and thread the splice wire through the loops.

  Ensure the thread wire does not miss any loops and catches each loop alternately. Ensure the belt edges are in line and do not form a step at the joint.
- (s) Bend the wire into a loop and feed it back into the belt loops. Cut off any excess wire.
- (t) Readjust the wash box seals, the restrainers and rotate the chicanes down onto the belt.

7.7 Run-In Period: A new belt should always be broken in at low speed for about 30 minutes prior to being loaded with sludge. This ensures that the new belt will track properly and pre-stretches the belt. Always monitor the machine closely during this time.

The process for belt run in is:

### **NOTE:** Never attempt dewatering until the new belt has been pre-stretched.

- 7.7.1 Adjust the tensioning pressure to 30 pli on both belts.
- 7.7.2 Start the belt wash water flow and energize the belt drive.
- 7.7.3 Follow the chart below to increase the belt tension during the break in cycle.

TIME PERIOD	BELT TENSION
First Hour	30 pli
Second Hour	40 pli
Third Hour	50 pli
Fourth Hour	40 pli

- 7.7.4 Set the belt tension to the desired setting for running the process stream. Generally, both belts will be operated at the same pli setting, not the same hydraulic pressure (psi). Tighten the jam nut on the pressure adjusting knobs when the desired belt tension has been set to prevent accidental changes due to vibration or other influence.
- 7.7.5 Adjust the steering sensing paddle by moving the valve mounting bracket so the dewatering belt tracks on in the center of the machine.

**Note:** Fine adjustment of the steering circuit is best done with the belts moving.

**CAUTION**: Use extreme caution when working around the moving belt. Avoid loose clothing that might become caught in the belt.

7.7.6 Proceed to Process Start Up:



### **8.0 PROCESS START UP:**

8.1 General: Knowing how to correctly and safely operate the belt press is important to accomplish optimum dewatering performance and minimum operating costs. After the Winklepress® is on line, operators can begin to adjust the following: sludge feed rate, polymer, feed rate and concentration, mixing energy, belt speed, and belt tension. The procedures for process start up and optimization are covered in the following section.

### 8.2 Process Variables:

8.2.1 Sludge Feed: The sludge flow rate can be determined by the desired solids loading, the amount of feed solids per hour per meter of belt width (lbs/hr/m) and the feed slurry solids concentration (%). See Formula 8.1 for the formula. The feed solids should be characterized to determine inorganic (ash) content, biosolids content and solids chemistry. For a quick reference the following sludge hydraulic limits are applicable for most of the municipal and industrial sludges:

#### Sludge Type

### Hydraulic Limit (GPM/Meter)

Primary, 100% domestic.	80-100
Secondary, 100% domestic	
Brewery waste from extended air	60-90
Paper, 100% primary, virgin fibers	100-200
Paper, 100% primary, secondary fibers	150-250
Alum	60-90
Blend of Primary, Secondary	60-90
Anaerobically digested	60-90

8.2.2 <u>Polymer</u>: Polymers are water-soluble long-chain organic molecules, which function in several ways to coagulate and flocculate solid particles. Sludge dewatering on a belt filter press is made possible to a great extent through the addition of a polyelectrolyte or polymer to the sludge. The primary duty of the polymer is to cause the sludge solids to flocculate. To do this, the polymer must neutralize the sludge charge, cause a rapid desorption of the sludge particles which unbinds surface water and cause the sludge particles to agglomerate along the polymer chains. To accomplish the optimum dewatering, it is important to select the proper polymer type, molecular weight charge density and electrical properties. The most common types of polymers used in the dewatering market today are the following:

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### 1. Forms of Polymers:

• Dry Polymers (95-100% active)

Dry polymers are manufactured as powder, granules, beads, or flakes. Dry polymers have a high active content. Dry polymer have proven to be very effective for biosolids conditioning, however, solution making of dry polymers is more difficult than that of liquids and emulsions.

Emulsion/Dispersion Polymers (20-67% active)

Emulsions are dispersions of polymer particles in hydrocarbon oil. They are high molecular weight polymers with high solids. Emulsions are pourable, clear to white milky liquids with viscosity ranging from 300-5,000 centipoise. Emulsions are stored in drums or tanks and transported with pumps, therefore, many operators prefer emulsions to dry polymers.

Mannich Polymers (3-7% active)

Mannich polymers have a high molecular weight and very high viscosity, typically ranging from 45,000-60,000 cps. The pH of Mannich polymers can be as high as 12. Mannich polymers are usually less expensive and have a relatively short shelf life.

Liquid Polymers (10-60% active)

There is a wide range of liquid polymer types available. Liquid polymers have low to medium molecular weight, viscosity ranging from 1 to 6,000 cps. The pH of liquid polymers is generally neutral to acidic. Shelf life can be from two months to one year depending on the manufacturer.

Regardless of the type of polymer selected, the plant personnel should verify that the polymer system specified can handle the type of polymer selected for the application. The recommended final polymer solution concentration ranges to condition the slurry are the following:

- Dry Polymers (0.05-0.5% by wt.)
- Emulsion/Dispersion Polymers (0.1-0.5% by vol.)
- Mannich Polymers (1-3% by vol.)

To avoid polymer activity degredation problems, solution storage times of organic polymers should be limited to 4-6 hours. Higher solution strengths are less susceptible to polymer degredation than low concentrations. Some polymers, especially higher molecular weight polymers, need "aging" time to develop full product activity in application.

NOTE: If the polymer solution is prepared at concentrations that are considerably higher than the solution concentrations recommended then polymer dewatering costs will increase because the polymer cannot be dispersed efficiently into the slurry. Polymer overdosing will deteriorate the sludge dewatering process as well.

- 2. <u>Polymer Charge:</u> A polymer should be chosen which neutralizes the sludge charge, and works within the pH range of the treatment plant's process. The three basic types of polymer (relating to charge) are:
  - Cationic: a positively charged polymer used with negatively charged sludges. This is the most common polymer for conditioning wastewater biosolids.
  - Non-ionic: a neutrally charged polymer used for some biosolids either independently or in conjuction with cationic polymers
  - Anionic: a negatively charged polymer used for some biosolids and positively charged sludge's such as alum sludge either independently or in conjunction with cationinc polymers.

### 3. Molecular Weights of Polymers:

Polymer is composed of many monomer units joined together. Molecular weight of a polymer is a rough indication of the length of the polymer chain that holds the charged sites apart. Molecular weight affects polymer solubility, viscosity and charge density in aqueous solution.

Molecular Weight Range	Description of MW
10,000,000 and higher	"Very high"
1,000,000 to 10,000,000	"High"
200,000 to 1,000,000	"Medium"
100,000 to 200,000	"Low"
50,000 to 100,000	"Very low"
Less than 50,000	"Very very low"

Low and very low molecular weight polymers are very water-soluble. They are usually described as "primary coagulants" and sometimes are used as the first part of a two-polymer program where very high charge density is required to "break" the suspension. Most of the sludge conditioning polymers fall into "medium" "high" and very "high" ranges. Higher molecular weight polymers have a broader dosage range.

4. <u>Polymer Dosage</u>: For a given type of sludge, polymer dosage is generally solids dependent, the lower the percent solids the higher the chemical dosage required. Polymer should be injected into the sludge at the minimum amount required for dewatering. All excess polymers are wasted and goes down the drain with filtrate. This is not cost or process effective. See the process diagnostic chart at the end of this section. It is furnished to help the plant operators determine if too little or too much polymer is being used.

Typical Polymer Dosage for Belt Filter Press Process

Sludge Type	Polymer Dosage (lbs/T d.s.)
Raw primary	4-8
Primary plus waste activated	6-10
Waste activated	8-16
Anaerobically digested waste activated	12-18
Anaerobically digested 50% primary plus	
50% waste actvated	10-16
Aerobically digested	10-16

Polymer selection and dosage should be determined by jar and bench-scale simulation test.

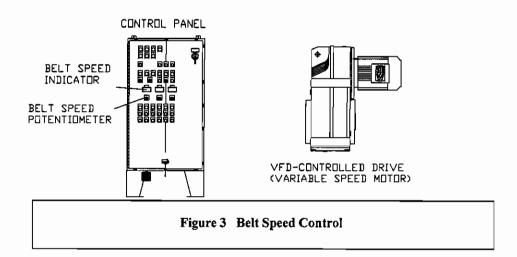
**8.2.3** Mixing Energy: This is the energy required to instantaneously mix the polymer with the suspended solids of the slurry. The optimum mixing energy is usually determined on site by adjusting the throat opening inside the variable orifice mixer. For example, to increase the mixing energy, reduce the throat opening of the mixer by increasing the adjustable counterweight and turn up the adjustable bolt on the valve stop handle to allow the weight arm to move further down. Too little or too much mixing energy results on less than optimum floc formation that adversely affects dewatering action. The diagram at the end of this section illustrates the detrimental effects of these conditions.

**8.2.4** Retention Time: This is the time required for the polymer reacting with the biosolids/residuals suspended in the slurry to complete the flocculation process. Most dewatering applications require 15-20 seconds to complete the flocculation process. With too little time, it generates small pin flocs. Both of these lead to reduced dewatering. For ideal dewatering, small strong flocs are desired. If room permits the pipeline design should include three spool locations that can accommodate the variable orifice mixer in order to change the retention time, if necessary, to improve the dewatering process. See the diagram at the end of this section. The spool pieces should be placed at 15, 30, and 45 seconds away from the belt filter press inlet at maximum flow.

## 8.3 Winklepress® Adjustments:

**8.3.1** Belt Speed: There are two basic considerations with belt speed. The slower the belt speed, the greater the effects of the pressure section that translates into increased cake dryness. This works because as the belt slows, the cake trapped between the belts is allowed to thicken which increases the shear-action produced by the pressure rollers. Conversely, the faster the belt speed, the greater the process throughput (assuming sludge feed rate is increased). The belt speed should be slowly adjusted until the optimal balance between process throughput and cake dryness is achieved. The belt speed range is 1 to 5 1/2 m/min. There are two VFD controlled belt

drives the belt speed can be adjusted by a belt drive speed potentiometer located on the control panel



- **8.3.2** Belt Tension: The belt tension should be set at 350 psig initially by adjusting the pressure valve on the hydraulic power unit. Since the sludges vary from plant to plant, the optimum pressure should be determined once the belt press is operating. An increase in the belt tension will increase the cake compression forces at the pressure rollers resulting in a dryer cake. However, it could cause the negative effect of belt blinding or pushing solids through the belts, which will result in an unacceptable amount of solids, lost to the filtrate. High belt tension will also decrease belt life. Ideally the pressure should be just below the point where the solids start adhering to the belt.
- **8.3.3.** Belt Type: The opening size weave of the belt and belt material determine the dewatering characteristics of that belt. The initial belt supplied by Ashbrook with your machine as been selected based on our experience with processes similar to your own. The information on the belt supplied with this machine is in Section 10 of this manual. Each belt and connecting splice are designed for a minimum tensile strength equal to five times the normal maximum dynamic tension to which the belt shall be subjected. The splice is designed to fail before the belt and is constructed of type 316stainless steel.
- **8.4 Upstream Variables:** There are other items upstream of the belt press that can affect the performance of the press. The information here is to illustrate some of the variables that may affect the overall dewater ability of the plant slurry:
  - **8.4.1** Slurry Pump Selection: For sludge dewatering applications, the use of positive displacement pumps is recommended. The preferred pumps for these applications include the following: Progressive Cavity,

Rotary Lobe, and Gear pumps. These pumps allow even flow of the slurry along the pipeline to allow good dispersion of the polymer with the suspended solids of the slurry and a constant pressure drop across the variable orifice mixer.

**8.4.2** Slurry Characteristics: Slurry characteristics shall be considered in sludge dewatering process.

#### 1. Solids Concentration

Solids concentration level influences the selection of a slurry condition program. Increasing feed solids concentration will cause lower polymer conditioning requirement. It is extremely important that the characteristics of the slurry being dewatered remain relatively constant in order to maintain good process control of the belt filter press. For example, if the feed solids concentration increases by 30% (i.e. from 2% to 2.6%), one of the following variables has to be adjusted in order to keep the press running satisfactorily:

- Polymer Dosage
- Belt Speed
- Slurry Flow Rate (to maintain constant solids loading)

#### 2. Biological Sludge Content

Usually biological sludges have high cationic polymer requirement. When dewatering waste activated biosolids, it is critical to understand that the specific resistance for activated sludge increases when the biological process is experiencing short mean cell residence time, low dissolve oxygen, low temperature and high F/M (food to microbe ratio) to control the population of filamentous bacteria in the aeration basin(s) to prevent poor belt filter press performance. Blooms of filamentous bacteria increase the polymer dosage; reduce the solids loading, and the cake solids during the dewatering process because water is stored inside the cells of the bacteria. Higher polymer requirements usually result from high dissolved solids in sludge.

#### 3. Inorganic (Ash) Content

Usually higher ash content yields higher dry cake solids. Biological sludges have ash contents ranging 15-35%. Ash contents of digested biological sludge can increase to 30-50%. Higher ashes contents are occasionally encountered from lime stabilized sludges or chemical treatment waste sludges. In these cases it is not unusual to have an anionic or nonionic conditioning program work best with the sludge.

#### Sludge Storage Time

Extended storage of raw primary and waste biological sludges before polymer conditioning increases conditioning requirements. Aeration improves the sludge dewatering characteristics.

- **8.4.3** Washwater Characteristics: The washwater used to clean the belts needs to have the following quality to prevent poor performance of the belt filter press:
- The total suspended solids (TSS) concentration should be ≤ 50 mg/l
- The total dissolved solids (TDS) concentration should be ≤ 1,000mg/l
- The pH of water should be 6-8
- The temperature should be 10-50°C.
- The washwater pressure should be ≥ 85 psig

Occasionally if the TSS concentration reaches 200 mg/l, the unit can operate marginally if the nozzles in the spray tubes are cleaned frequently with the wire brushes (these are actuated by opening and closing the manual valve). If the washwater pressure drops considerably, the solids that are embedded in the belts during the filtration process cannot be dislodged, causing belt blinding after a certain period of time.

- 8.5 Process Calculations: To evaluate the Winklepress ® performance, it is important to understand the basic calculations involved. The governing process variables of the dewatering process are the following:
  - Solids Loading (lbs/hr processed, dry basis)
  - Cake Solids (%TS, % total solids in the cake)
  - Polymer Dose (lbs of dry or neat polymer/ton of dry solids dewatered)
  - Capture (% of dry solids of the feed retained in the cake after the dewatering process)
    - **8.5.1** <u>Cake Solids</u>: This is determined by conducting a total solids test (see Standard Methods For the Examination of Water and Wastewater19<sup>th</sup> edition)
    - **8.5.2.** Solids Loading Rate: The amount of solids loading dewatered in the press is determined by the following equation:

### Formula 8.1:

 $SL = \underbrace{SFR \times BDS \times STSC \times 60}_{BW}$ 

where, SL = solids loading (lbs/hr)

SFR = slurry flow rate (gpm)

BDS = bulk density of the slurry

STSC = slurry total solids concentration (%TS)

BW=belt width (m)

60=conversion factor (min/hr.)

In order to determine the solids loading, the slurry flow rate (usually measured by a magnetic flow meter or a calibration tank), the total solids concentration of the slurry and belt width must be known.

### 8.5.3 Polymer Concentration:

a. Liquid Polymer:

### Formula 8.2

Percent Concentration = (Gallons Polymer/Gallons Water) x 100%

Example: Determine polymer percent concentration using 2.5 gallons polymer and 1000 gallons of water

Percent Concentration: 2.5/1000 = 0.0025 Multiply by 100% to convert to percentage  $0.0025 \times 100\% = .25\%$ 

b. Dry Polymer:

### Formula 8.3

Percent Concentration = [Pounds Polymer/(Gallons Water x 8.34)] x 100%

Example: Determine polymer concentration using 10 pounds dry polymer and 1000 gallons water.

Convert 1,000 gallons of water to pounds - 1 gallon = 8.34 pounds  $1,000 \times 8.34 = 8340$  pounds

Polymer Concentration:

10/8340 = 1.19

To convert to percent concentration, multiply by 100%  $1.19 \times 100\% = 0.12\%$ 

**8.5.4** <u>Polymer Usage</u>: The polymer dose required for the dewatering process is determined by the following equation:

### Formula 8.4

 $PD = (PSFR \times PSC \times PSBD \times 2000) \div (SFR \times BDS \times STSC)$ 

where, PD = polymer dose (dry or neat lbs/ton dry solids)

PSFR = polymer solution flow rate to variable orifice mixer (gpm)

PSC = polymer solution concentration (% wt. for dry polymers, % vol. for emulsion/dispersion and mannich polymers)

PSBD = polymer solution bulk density (usually 8.34 lbs/gal)

SFR, BDS, STSC = as described previously

**8.5.5** <u>Capture Rate</u>: The capture of the dewatering process is determined by the following equation:

#### Formula 8.5

### CR = 100 [(CS/FS)] [(FS-FTS)/CS-FTS)]

where, CR = capture rate (%)
CS = cake solids (%TS)
FS = feed solids (%TS)
FTS = filtrate solids (%TSS)

### 8.6 Process Start Up:

8.6.1 Start wash water.

8.6.2 Start hydraulic power unit and set pressure at 350 psig.

**8.6.3** Ensure hydraulic control valves are in tension position and belt is tensioned.

**8.6.4** Start belt drive and run for approximately two minutes to pre-wet the belt. The belt speed should be approximately fifty percent of its maximum.

**8.6.5** Start the polymer pump; make sure that the polymer system is operational and is providing the adequate flow rate and polymer solution concentration (Calibrate the polymer system to provide the appropriate polymer dose (lbs/ton) for the biosolids/residuals loading specified.

8.6.6 Start sludge pump, after allowing the polymer solution to flow for a period of 30 seconds. Adjust the flow rate per the specifications (conduct a total feed solids concentration test prior to pumping the biosolids/residuals to the press) to determine the flow rate required to match the solids loading specified. Look on top of the gravity zone of the press to determine if the polymer solution flow rate being fed to the variable orifice mixer is sufficient to flocculate the biosolids/residuals effectively (adjust the polymer pump until this condition is achieved). Adjust the belt speed to prevent thickened biosolids/residuals from overflowing the gravity zone.

The operational belt speed range recommended for the press is between 1-3 m/min (3.3-10 fpm). The optimum belt speed depends upon the type of biosolids/residuals being dewatered and the expected performance of the press.

**8.6.7** Adjust side sludge restrainers until most solids are retained inside the restrainers. Water seeping under the seals is common and will not hurt the

dewatering process. Most of the presses have AUTO MODE operation option on its control panel. The press can be start up automatically or manually.

For the automatic start up, place the mode Select HAND/OFF/AUTO selector in the Auto position, the Auto pilot light illuminates. Press the AUTO START push-button, the press starts up following the above procedure automatically. The operator need to adjust the potentiometer dials of sludge pump, polymer pump, hydraulic pressure, belt speed to the optimum settings before the start up. Those settings need to adjust accordingly after the start up to reach the optimum performance.

For the manual to start up, place the Mode Select HAND/OFF/AUTO selector in the HAND position, then start the press follow the start up procedure.

To start up the press without AUTO MODE operation option, press the push buttons and follow the start up procedure.

8.7 Process Adjustments: Because the dewatering process is dependent on numerous variables, it is important to understand how changes in the process will affect the end result. All of the process variables have an optimum point depending on the other variables. Because of this, Ashbrook recommends adjusting the process slowly by changing one variable at a time and logging the results. A suggested order for adjusting the process is:

- **8.7.1** Adjust sludge feed rate to achieve the throughput desired.
- **8.7.2** Adjust polymer flow for proper flocculation.
- **8.7.3** Adjust belt speed.
- **8.7.4** Adjust the wedge plate.
- **8.7.5** Fine-tune the performance by adjusting the belt tension, mixer, and chicanes, etc.

**8.8 House Keeping and Clean Up:** Refer to the detailed information in the Daily Operation Section of this manual for the house keeping and clean up required prior to shutting down the machine.

NOTE: Never shut down the press with sludge between the belts.

**8.9 Process Trouble Shooting**: There are several circumstances that can cause poor dewatering performance in a belt filter press:

- Low Cake Solids
- Low Capture
- · Low Solids Loading

# **8.9.1** <u>Low Cake Solids:</u> When this instance occurs, the following corrective measures are recommended:

#### 1) Adjust belt speed

Measure the current belt speed and the cake thickness. If the belt speed is greater than 3 m/min and the cake thickness is less than 3/8", reduce the belt speed in 10% increments allowing enough time before cake samples are taken to determine if the reduced belt speeds improve the cake solids concentration.

#### 2) Adjust the polymer dose

Sometimes, the slurry solids concentration can increase creating a starved polymer condition. This can be resolved by increasing the polymer solution flow rate to the variable orifice mixer. Take samples to determine if changes in polymer dose settings improve cake solids concentration.

#### 3) Adjust the mixing energy

If the slurry characteristics vary, it may require an increase or a decrease in mixing energy by adjusting the throat of the variable orifice mixer (see diagram at the end of this section). Take samples to determine if changes in mixer settings improve cake solids concentration.

#### 4) Adjust hydraulic pressure

Increase the hydraulic pressure in 50 psig increments (do not exceed hydraulic pressures of 550 psig, 750 psig, and 1,000 psig for the 1.0-m, 1.5-m, and 2.0-m unit respectively to prevent irreversible belt damage). Caution has to be taken when this procedure is executed to prevent blinding the belts with solids.

# **8.9.2** <u>Low Capture:</u> when this instance occurs, the following corrective measures are recommended:

#### 1) Adjust belt speed:

Measure the current belt speed. If the belt speed is greater than 3 m/min, reduce the belt speed in 10% increments allowing enough time before filtrate samples are taken to determine if the reduced belt speeds improve the capture.

#### 2) Adjust polymer dose:

Sometimes, the slurry solids concentration can increase creating a starved polymer condition, allowing extra solids to pass through the belts. This can be resolved by increasing the polymer solution flow rate to the variable orifice mixer. Take samples to determine

if changes in polymer dose settings improve cake solids concentration.

#### 3) Adjust doctor blades:

Check the doctor blades to make sure they are touching the surface of the belts. If there is a small gap, extra solids will remain on the belts, which will enter the wash boxes, and show up in the filtrate. If the blades are worn out, contact the Ashbrook Retrofit and Spares Parts Department to order new ones.

# 4) Inspect slurry restrainer seals in the gravity zone and the wedge zone:

Verify that the slurry restrainer seals in the gravity zone do not allow the slurry to pass underneath them. Otherwise, the slurry will fall into the filtrate pan in the gravity zone causing an increase of the suspended solids concentration in the filtrate. In addition, the restraining seals in the wedge zone should not allow any thickened slurry to exit from the edges of the wedge; if they are loose, adjust the external wall of the wedge zone until the seals prevent thickened slurry from migrating to the filtrate stream.

**8.9.3** <u>Low Throughput:</u> When this instance occurs, the press cannot meet the hydraulic or solids throughput requirements. The following corrective measures are recommended:

#### 1) Verify the slurry solids concentration

2) Inspect the slurry pipeline upstream of the belt filter press is free of obstruction and debris. If the slurry solids concentration is decreased, the solids loading to the press will be decreased by the same amount. Adjust the slurry flow rate to make up for the reduced solids concentration.

#### **8.10 PROCESS DIAGNOSTIC CHART**

#### **Insufficient Polymer**

Sludge squeezing from the belts Large weak flocs Poor gravity dewatering Gravity section overflows Poor capture rates Wet cake

#### **Insufficient Mixing**

Large clumpy flocs
Filtrate in sludge inlet is cloudy
High filtrate solids
Low cake dryness
Cake sticks to belts

#### **Excessive Polymer**

Foaming at sludge inlet
Sludge feels "slimy"
Filtrate is foamy and slimy
Puddling in the gravity section
High polymer bills
Cake sticks on belts at discharge

#### **Excessive Mixing**

Sheared flocs
Poor gravity drainage
High filtrate solids
Sludge squeezes from belts

#### Proper Polymer Dosing & Sludge Polymer Mixing

Small strong Flocs
Clear Filtrate
Little or no foaming
Good drainage in the gravity section
Plowed rows of loosely structured cake at the end of the gravity section
Cake discharge falling freely
Dry cakes
High throughput

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#### 8.11 WINKLEPRESS PROCESS TROUBLESHOOTING CHART

Problem	Probable Cause	Recommended Solution
1) Wet Cakes	a. Sludge rate too high	a. Lower sludge loading
	b. Belt speed too fast	b. Reduce belt speed
	c. Improperly dosed polymer	c. Adjust polymer rate
	d. Incorrect polymer for application	d. Screen for optimum polymer. Arrange on site jar test with your poly representative
	e. Incorrect belt tension f. Incorrect polymer/sludge mixing action	e. Increase belt tension f. Adjusting mixing action at in-line polymer mixer g. Check plant process for
	g. Plant process upset	trouble
2) Puddling or ponding in the gravity section	a. Incorrect polymer dosage	a. Adjust polymer feed rate
	b. Incorrect polymer/sludge mixing action	b. Adjust mixing action at in-line polymer mixer
	c. Inadequate polymer concentration	c. Try various concentrations. Use post dilution H <sub>2</sub> O if available
	d. Belt not cleaning properly	d. Check if belt is blinded Operate brush in wash tube
3) Low Capture rate (Solids recovery)	a. Incorrect polymer dosage	a. Use jar test to determine optimum dose
(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	b. Sludge solids squeezing from between belts	b. Reduce sludge pumping rate or increase polymer feed rate
	c. Belt tension (pli) too high	c. Reduce tension accordingly
4) Sludge squeezing from between belts into sump	<ul> <li>a. Insufficient polymer</li> <li>b. Large weak flocculation</li> <li>of sludge particles in the gravity section</li> <li>c. Sludge loading or belt speed incorrect</li> </ul>	a. Increase accordingly b. Increase mixing action at sludge/poly mixer to decrease floc size c. Decrease sludge flow or increase belt speed
5) Uneven cake dryness at machine discharge	a. Poorly distributed sludge at machine inlet	a. Use the level baffle and belt speed to properly distribute the sludge across the entire effective belt width

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# 2 SLUDGE DEWATERING LOG SHEET

	POLYMER COST/TON/DS				er Ø 1 Artika va			
	POLYMER USAGE (LBS/TON/DS)							
	POLYMER CONC. (%)							
	POLYMER FLOW RATE (GPM)							
KTURE: YPE: :OST/LB:	CAVE POLYMER THICKNESS FLOW INCH) RATE (GPM)							
SLUDGE MIXTURE: POLYMER TYPE: POLYMER COST/LB: BELT TYPE: LAB PHONE:	CAPTURE RATE (%)							
	CAKE SOLIDS (%)							
	FILTRATE SOLIDS (MG/L)							
	TOTAL FILTRATE FLOW RATE (GPM)							
PRESS NUMBER: TEST DATE: TEST DURATION: RUN#: SLUDGE TYPE:	WASH WATER (GPM)							
PRESS NUMBEI TEST DATE: TEST DURATIO RUN#: SLUDGE TYPE:	WASH WATER (PSI)							
	SLUDGE TEMP. °F							
	SLUDGE PH				-			
	SOLIDS LOADING (LB/HR)							
	SLUDGE FLOW RATE (GPM)							
	BELT TENSION (PLI)							
	BELT SPEED (MMIN)							
ISTOMER: FE: TY, STATE: ANT PHONE: TPE & SIZE ESS:	JE TIME / MPLE NO							



#### ASHBROOK WINKLEPRESS®

#### 9.0 DAILY OPERATION PROCEDURES:

- <u>9.1 General</u>: These procedures cover the routine operation of the Winklepress<sup>®</sup> and should be used as a model for a plant's customized procedures.
- <u>9.2 Pre-Operation</u>: This covers the steps, which should be followed prior to starting any of the belt press functions. These steps help ensure the safety of the operators as well as the equipment.

#### 9.2.1 Pre-Start Inspection:

- (a) Verify no foreign objects are on the belt or in an area that will interfere with the belt press operation.
- (b) Ensure chicanes are positioned on belt.
- (c) Verify tensioning control valve is in the tension position and that the belt is ready for tensioning.
- (d) Ensure all feed pumps are ready for operation and all valves are open.
- (e) Ensure the scraper blades are in position against the belts.
- (f) Verify panel and machine have not been locked-out due to a prior alarm or maintenance condition.
- (g) Inspect hydraulic power unit and verify the oil level is adequate for operation.
- 9.2.2 <u>Start-Up</u>: The sequence detailed is for a completely manual start up. Depending on the installation, the electrical controls may have the capacity to completely automate the start up. However, it is important to know the manual start up process to evaluate the effectiveness of the control system.
  - (a) Start belt wash system.
  - (b) Start hydraulic system and allow two minutes for belts to completely tension.
  - (c) Start belt drive system and allow the belts to be completely pre wetted prior to adding sludge.
  - (d) Start sludge and polymer feed pumps.
- <u>9.3 Operation</u>: The routine practice of inspecting the belt press during the operation phase will minimize down time. The inspection instructions are divided into mechanical

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and process checklists for the aid of the operators and mechanics.

#### 9.3.1 Mechanical Inspection:

- (a) Ensure feed assembly is evenly loading the belt.
- (b) Ensure chicanes are turning sludge mass and inspect them for wear. Replace chicanes as required.
- (c) Ensure edge restrainer seals are contacting the belt and seals are not worn. Replace or adjust seals as required.
- (d) Ensure doctor blades are functioning correctly. Inspect blades for wear and replace as required.
- (e) Inspect gravity drainage grids for wear. Replace wiper bars before belt contacts metal support grids.
- (f) Ensure belt wash system is completely cleaning belt. Look for streaking or striping on the belt. If present, rotate the wash water hand wheel fully counter clockwise and then fully clockwise to clean the spray nozzles.
- (g) Inspect wash box seals for wear. Replace as required.
- (h) Inspect dewatering belts for wear. Repair holes per maintenance instructions. Repair or replace broken belt seam wires.
- (i) Ensure steering sensing paddles are in contact with the belts and correcting belt steering as required.
- (j) Ensure there are no leaks from any of the systems.
- (k) Inspect roller coatings for wear and ensure flingers are in place.
- (1) Ensure all electrical controls are functional.

#### 9.3.2 Process Inspection:

- (a) Adjust sludge feed rate for process throughput requirements.
- (b) Adjust polymer feed rate until flocculation is correct.
- (c) Adjust belt speed and tension for above conditions.
- (d) Ensure mixing energy is in the correct range.
- (e) Adjust belt tension and nip roller pressure if available as required for optimum dewatering.
- <u>9.4 Normal Shut Down & Clean Up</u>: The key to minimal down time and reduced maintenance costs is housekeeping. If the belt press is inspected and maintained daily it can be counted on for years of service. The following guideline should be used for daily machine shut down and cleaning:
  - **9.4.1** Shut down the sludge and polymer feed systems.
  - 9.4.2 Allow the belt wash station to run for 45 minutes without any sludge or polymer feeding onto the belt press. During this time period:

Name of the Control o

- (a) Lift the chicanes off the belt.
- (b) Wash down the Winklepress® from top to bottom using a water hose.
- (c) Rotate the scraper blades away from the belt and hose down the scraper assembly, especially behind and under the blades.
- (d) Wash out the drain pans.
- (e) When the machine is completely washed down and free from sludge, return the chicanes and scrapers to their operating position. Clean the wash water spray tube by rotating the wash water hand wheel completely in the counter clockwise direction and then completely in the clockwise direction.
- 9.4.3 Shut down the belt wash water system.
- 9.4.4 Shut down the drive unit.
- 9.4.5 Move the tension control valve on Winklepress® to the retract position. Allow the belt to completely retract to clean and oil the cylinder rods.
- 9.4.6 Shut down the hydraulic power unit.
- 9.4.7 Move the tension valve to the tension position.
- **9.5 Emergency Shut Down:** The machine could be stopped without going through the normal shut down sequence due to a mechanical failure or other emergency. While the machine will not be damaged due to this type of shutdown, the life of components could be shortened by not cleaning the belt press. If the machine is shut down because of an emergency, the following steps should be taken:
  - **9.5.1** Identify the problem and estimate the down time.
  - 9.5.2 If the machine will be down for more than one shift then:
    - (a) Wash the machine down to prevent sludge from drying on both belts. The area where both belts are in contact with the sludge (pressure section) should be given extra effort.
    - (b) If possible, relax the belt tension.
    - (c) Correct the emergency condition.
    - (d) Start hydraulic power unit and reduce belt tension to 25 pli by adjusting the pressure control valve on the hydraulic power unit.
    - (e) Place the tension valve in the tension position and allow the belt to tension.

**CAUTION:** Starting the belt drive at full tension with cake between the belts places unnecessary stress on the belts, belt drive motor, and rollers. This could lead to premature mechanical failure.

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- (f) Start wash water and allow belt to pre-wet.
- (g) Start belt drive. If belt is not clean, allow the machine to run for 45 minutes to complete a belt wash down cycle.
- (h) Increase the belt tension to the normal setting.
- (i) Start the sludge and polymer feed systems and begins operation of the press.
- **9.5.3** If possible, relax the belts by placing the control valve in the retract position.
- 9.5.4 Correct the emergency condition.
- 9.5.5 Start the hydraulic power unit and reduce the pressure to 15 pli.
- **9.5.6** Place the hydraulic control valve in the tension position and allow the belt to tension.
- 9.5.7 Start the belt wash system and allow the belt to pre-wet.
- 9.5.8 Start the belt drive.
- 9.5.9 Increase hydraulic pressure to normal setting (25 pli).
- 9.5.10 Start sludge and polymer feed systems.
- **9.5.11** Continue dewatering process as normal.

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## ASHBROOK WINKLEPRESS®

#### 10.0 MAINTENANCE PROCEDURES

**10.1 GENERAL:** Maintenance instructions will be divided into the same functional groups as indicated in the General Mechanical Description of this manual. Drawings, cut sheets or schematics, if applicable, will be indicated in the appropriate section. The intervals indicated are based on a normal work or operating schedule of forty hours per week.

#### 10.2 DAILY MAINTENANCE ITEMS:

- 10.2.1 Clean belts by running belt drive and wash system without sludge or polymer for a minimum period of 45 minutes.
- 10.2.2 Clean spray nozzles on wash boxes.
- 10.2.3 Check fluid level in hydraulic unit. Fill as required.
- 10.2.4 Manually extend and retract the tension cylinders to clean and oil the rods. This will greatly extend the life of the seals.
- 10.2.5 Cycle the steering cylinder in both directions by holding the steering paddle first one way and then the other. This will clean and oil the rods and greatly extend the life of the seals.
- 10.2.6 Inspect alarm sensors.
- 10.2.7 Check emergency trip cord by manually tripping and resetting.

#### **10.3 WEEKLY MAINTENANCE ITEMS:**

- 10.3.1 Inspect wear items specifically chicanes, scraper blade, gravity drainage grids, dewatering belts, rubber seals on the sludge restrainers and the wash stations. Replace as required.
- 10.3.2 Inspect frame and roller coatings for wear.
- 10.3.3 Inspect belt guides and wiper bars for cleanliness/wear. Clean as required.
- 10.3.4. Check for any loose bolts.

#### 10.4 MONTHLY MAINTENANCE ITEMS:

- 10.4.1 Verify daily and weekly items have been completed
- 10.4.2 Clean belts with a soap/bleach mixture. To prepare the soap/bleach mixture, use 1-cup detergent and 3-cups bleach to mix with 5 gallons water. The soap can be any laundry type liquid detergent and the bleach can be any generic brand bleach containing 5.25% sodium hypochlorite. The water can be tap water. Use power wash system to spray the soap/bleach mixture on belt surface for cleaning. The spray pressure shall be about 1,000 psig and not to exceed 2,000 psig.

10.4.3 Check belt seam wires for breaks. Replace if broken.

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#### 10.5 <u>SEMI-ANNUALLY MAINTENANCE ITEMS</u>:

- 10.5.1 Verify monthly items have been completed.
- 10.5.2 Clean hydraulic filter screen.
- 10.5.3 Check oil level in drive unit gearbox and lubricate bearings. See lubrication schedule in Section 13.
- 10.5.4 Inspect polymer mixer/injection ring assembly and clean as required. (See Section 10.17.2)
- 10.5.5 Lubricate the hydraulic pump motor bearings.
- 10.5.6 Replace belt seam wires.

#### 10.6 **FRAME**:

#### 10.6.1 Inspection Items:

- a. Inspect frame and anchor bolts and tighten as required.
- b. Inspect frame coating and repair corrosion as required.

#### 10.6.2 Coating Repair Procedures: (Galvanized Frame only)

Note: The frame may be under warranty. Contact Ashbrook before repairing the frame.

- a. Clean corroded area with wire brush until base metal is exposed.
- b. Coat area with spray or liquid galvanizing solution.

#### 10.6.3 Hot Dip Galvanizing Process Description

All carbon steel surfaces shall be hot dipped galvanized in accordance with ASTM A123/A 123M-97a, with a minimum coating of Grade 100.

The general procedure is as follows:

- 1. The components to be galvanized are first dipped in a 180 degree F caustic bath to remove any lacquers, oils or other foreign material from the steel.
- 2. The components are pickled in a hydrochloric acid solution to remove any residual mill scale and aid in zinc adherence.
- 3. If corrosion exists on any of the parts after acid dipping, the parts are sandblasted to white metal where required.
- 4. The components are submerged in an 850 degree F zinc bath for not more than 5 minutes. The zinc bath uses a sal ammoniac surface froth for fluxing the components.
- 5. The components are removed from the zinc bath and checked for zinc thickness build-up. Acceptable zinc thickness is between 4 and 7 mils.
- 6. The galvanized surface shall be cleaned of all runs, sags, excessive deposits and other deformities.

#### 10.7 <u>ROLLERS</u>:

#### 10.7.1 Inspection Items:

- a. Inspect roller coating for damages.
- b. Minor chips and scratches can be repaired using a touch up kit.
- c. Contact Ashbrook for re-coating worn out coatings.

#### 10.7.2 <u>Drawings:</u>

SK001606 - Roller Assembly

#### **10.8 BEARINGS**:

10.8.1 Bearing Cut Sheets: See attached

10.8.2 Pillow block Dimensional Data: See attached

- a. Spherical Roller Bearing Dimensional Data
- b. Cylindrical Roller Bearing Dimensional Data

#### 10.8.2 Inspection Items:

- a. Ensure grease is visible on bearing/shaft seal.
- b. Check bolts.
- c. Ensure roller flinger is in place.

#### 10.8.3 <u>Lubrication Procedures</u>:

*Note*: Lubricate bearings every six months with 3 to 5 ounces of grease per bearing. Use only the lubricants contained in the lubrication cross reference in this manual. Failure to lubricate the bearings will invalidate the bearing warranty.

- a. Attach grease gun to button grease fitting.
- b. Inject three to five ounces of grease. Grease should be seen.
- c. Disconnect grease gun and continue with remaining bearings.
- d. Repeat until all bearings are lubricated.

#### **Bearing Specifications**

All rollers shall be supported by a greasable-type, high capacity "E" design roller bearings, equipped with a metal cages, in sealed, splash proof, horizontal split case, pillow block housing. These bearings shall be pressed fit to the roller shaft. Bearings supporting the steering rollers shall be non-self-aligning cylindrical roller bearings in pivot mounted pillow block housings. All other rollers shall be supported by self-aligning spherical roller bearings mounted in fixed pillow block housings.

The L10 life shall be based on the summation of all forces applied to the bearings, including, but not limited to, roller mass forces and belt tension on the rollers. The belt tension forces exerted on the pressure zone rollers shall include a belt tension of 50 pli at a belt speed of 5 meters per minute. Certified calculations, based on the AFBMA/ISO capacity formula, showing that all bearings comply with the specified requirements for minimum L10 bearing life, at maximum loadings, shall be submitted to the engineer as set forth in the contract documents.

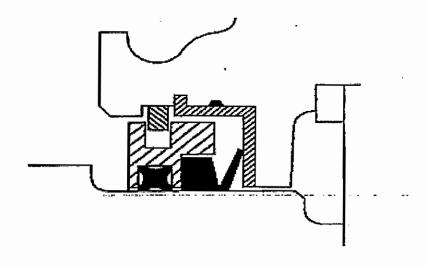
Bearing housings shall be class 30 cast iron with four stainless steel mounting bolts and four stainless steel cap bolts. The outer side of the housing shall be solid, without end caps or filler plugs. The housings shall be designed with an integrally cast water trough which, when shrouded be a shaft mounted water flinger, shall divert water from the bearing seal area. The housing shall be coated as specified herein.

The bearing seal in the pillow block housing shall be of non-metallic construction with a carrier/flinger, which rotates with the roller shaft. A static sealing arrangement between the carrier/flinger and the shaft shall be a triple rubber seal, constructed in a manner that prevents relative rotation between that seal and the shaft. A dynamic sealing arrangement between the carrier/flinger and the bearing housing shall consist of a primary dynamic contact seal of ozone resistant rubber which shall seal by rotational contact with a machined housing surface. A secondary dynamic seal shall be a labyrinth seal between the carrier/flinger and the bearing housing which utilizes a non-metallic retaining ring to hold the seal assembly in position within the housing.

Bearing lubrication shall be performed through a monel or type 316 stainless button head grease fitting mounted on the bearing housing. All bearings shall be outboard (externally mounted) and shall be greaseable while the unit is in operation Lubrication shall not be required more than once every six months.

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#### IMPROVED TRIPLE-TECT SEAL DESIGN

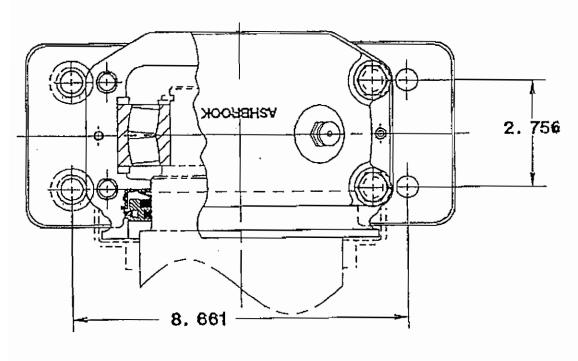


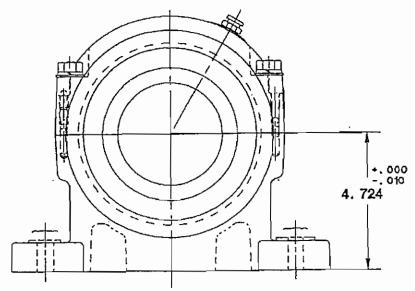
#### **FEATURES:**

- ❖ HOUSING SEAL IS PATENTABLE TRIPLE-TECT DESIGN
- COMBINATION NON-METAL LABYRINTH SEAL. DYNAMIC FACE RUBBING LIP SEAL. AND STATIC SHAFT SEAL.
- DYNAMIC LIP SEALS AGAINST STAINLESS STEEL RING AND WILL NOT DAMAGE THE SHAFT.
- SEAL ASSEMBLY CONTAINS OZONE RESISTANT STATIC AND DYNAMIC SEALS WITH WEATHER RESISTANT NYLON LABYRINTH CARRIER/FLINGER
- ❖ FACE CONTACT SEAL IS REPLACEABLE WITHOUT REMOVING BEARING FROM SHAFT OR HOUSING FROM FRAME.

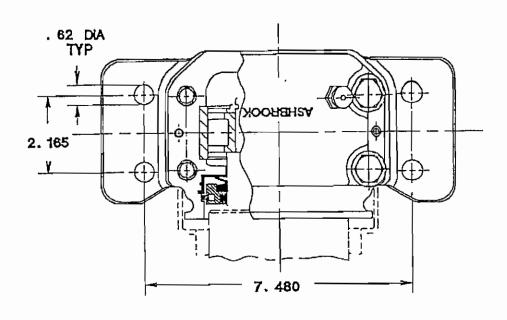
#### **BENEFITS:**

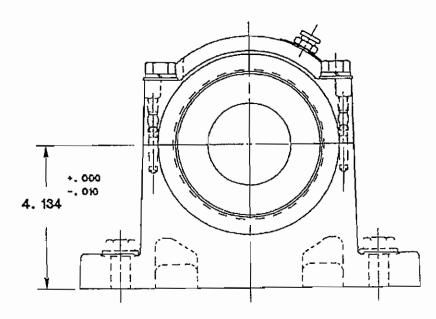
- ❖ ALLOWING FOR GREASE PURGING WITHOUT EXCESSIVE PRESSURE BUILD UP IN HOUSING
- ALLOWS FOR BEARING MISALIGNMENT AND EXPANSION
- ❖ SEALS STATICALLY ALONG SHAFT-SEAL ROTATES WITH SHAFT
- ❖ SEAL CONTACT WILL NOT DAMAGE SHAFT
- ❖ NO CORROSION OR WEAR ON SHAFT UNDER SEAL SURFACE
- ❖ PROVIDES SUPERIOR SEALING\_ACTION IN WET ENVIRONMENTS
- HOUSING SEAL RING PROVIDES CONTINUOUS SEALING SURFACE AND PREVENTS POTENTIAL SEAL LIP DAMAGE DURING INSTALLATION
- ❖ SEAL ASSEMBLY HAS BEEN LIFE TESTED AND MET ALL DESIGN CRITERIA



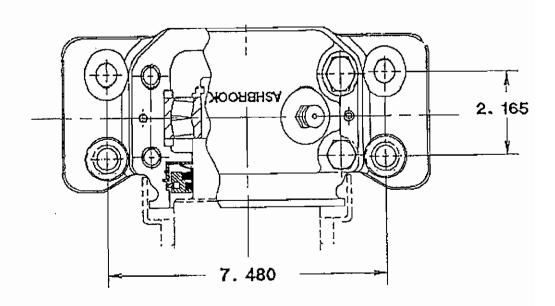


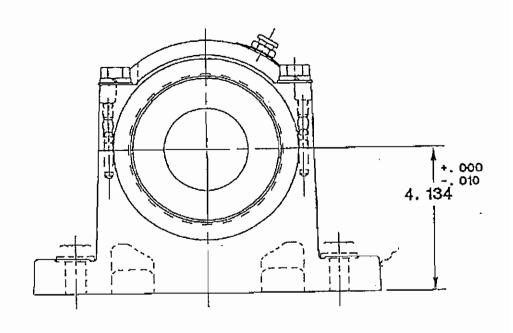
90MM CLOSED END PILLOW BLOCK CAD3232





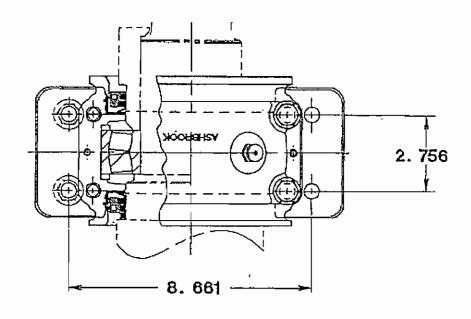
#### 60MM TRACKING ROLL PILLOW BLOCK- EXPANSION

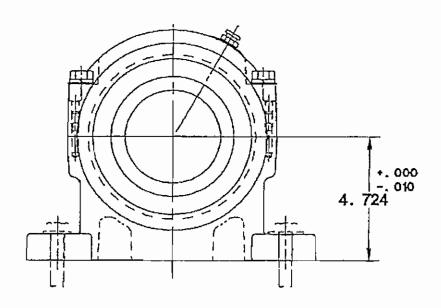




#### 60MM CLOSED END PILLOW BLOCK

CAD3231

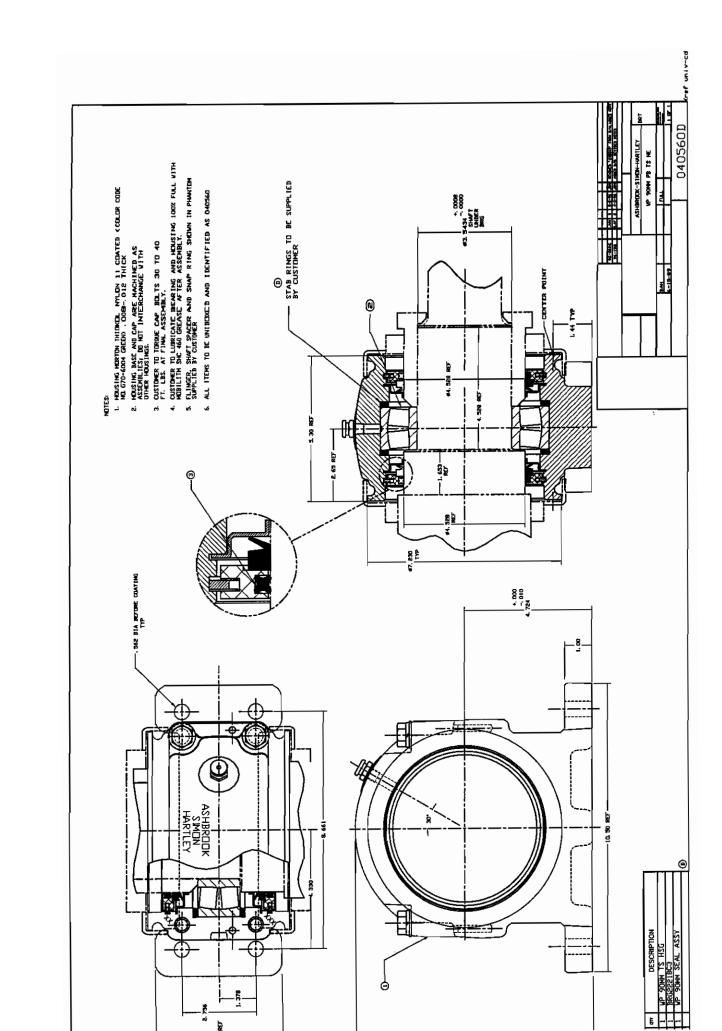


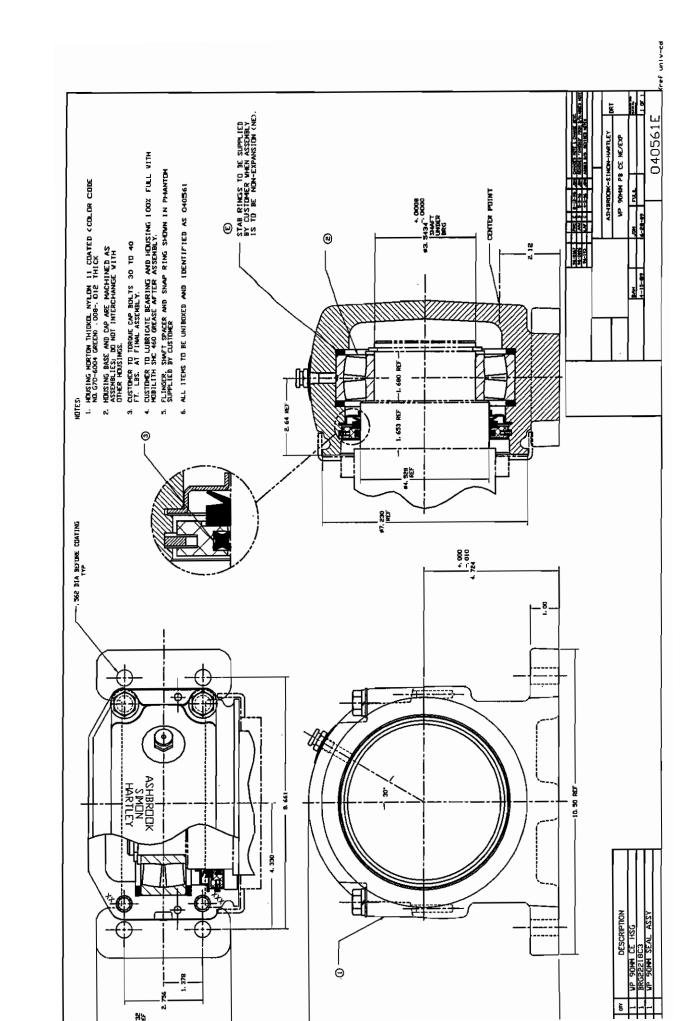


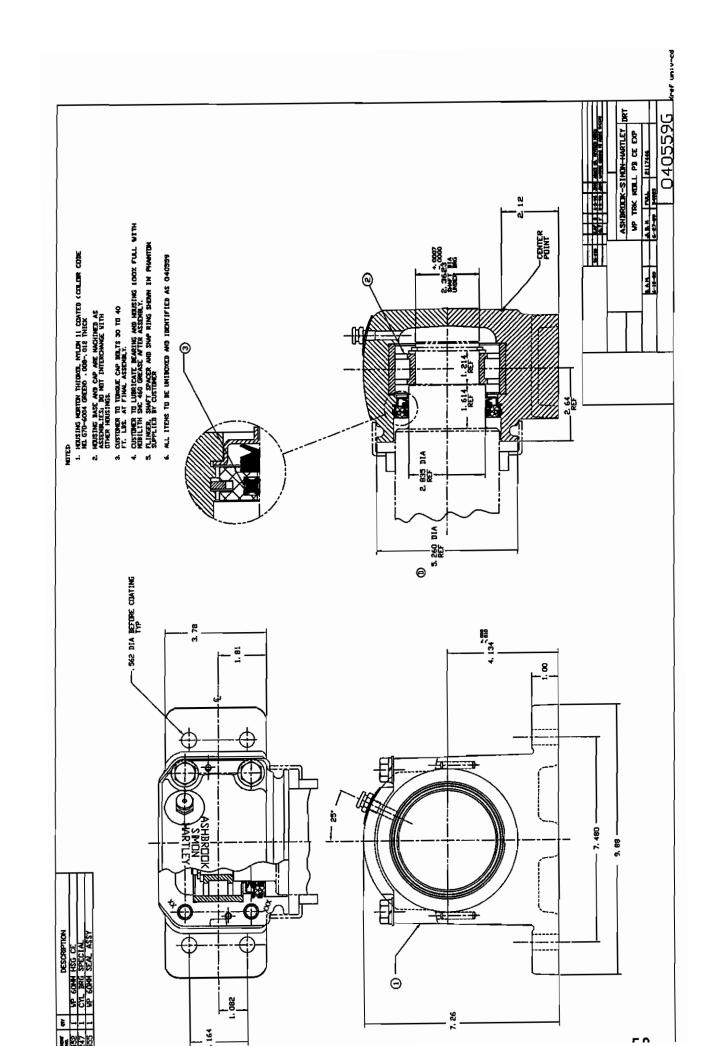
## 90MM THRU BORE PILLOW BLOCK

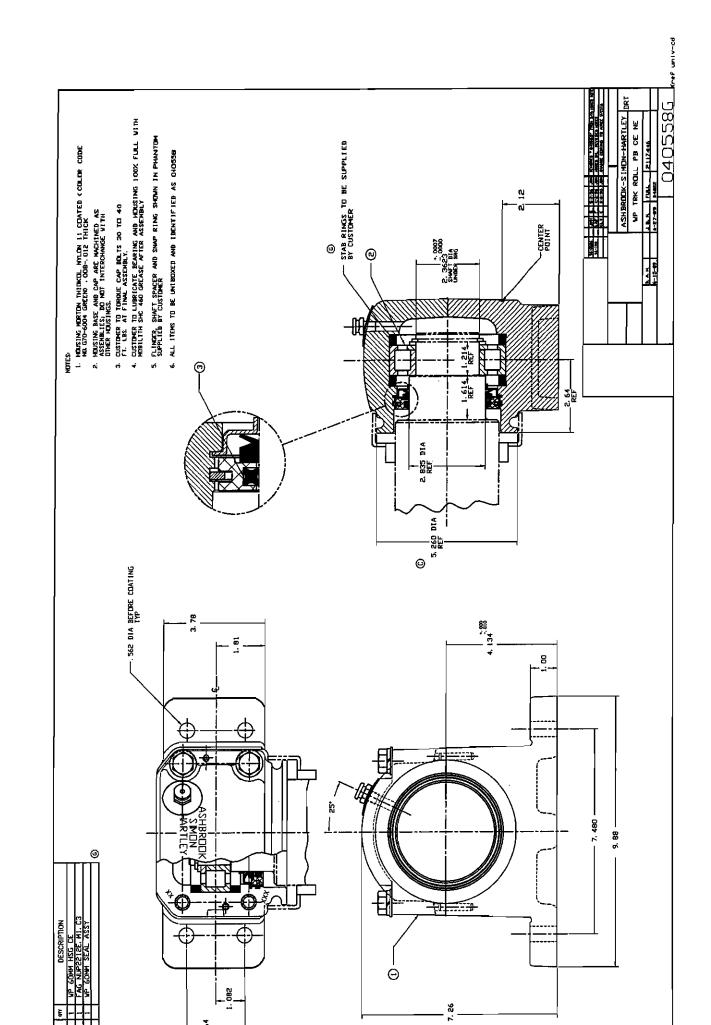
# WINKLEPRESS . 62 DIA TYP 2. 165 7. 480 +.000 4. 134

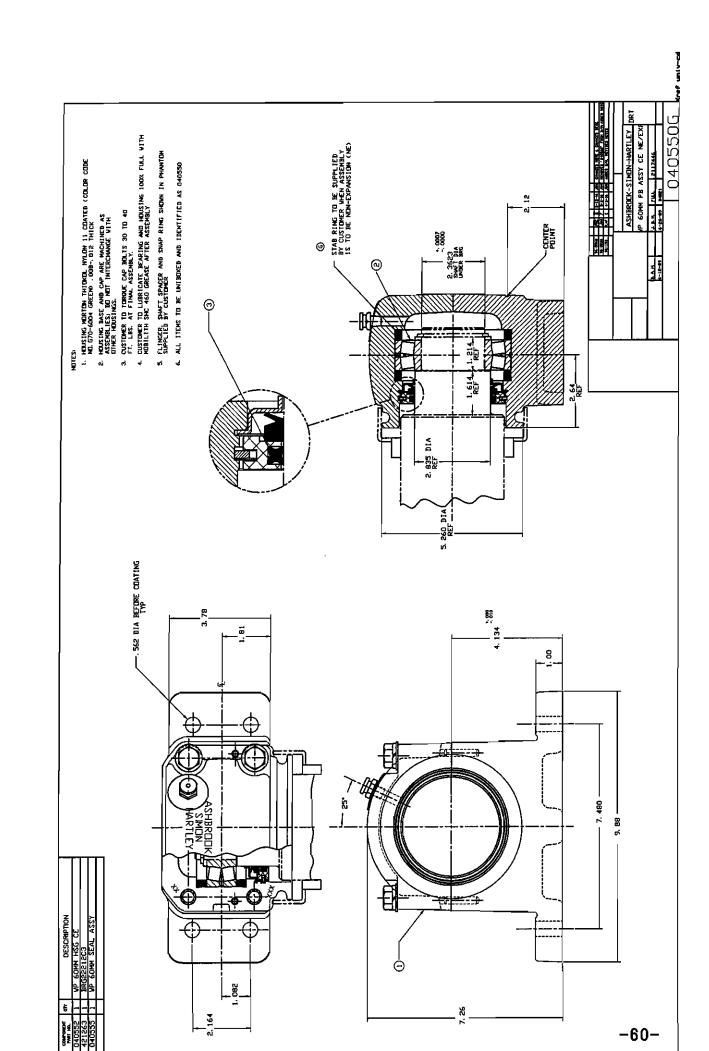
60MM TRACKING ROLL PILLOW BLOCK- NON EXPANSION











#### 10.9 STEERING ASSEMBLY:

#### 10.9.1 <u>Drawings:</u>

- a. Hydraulic Cylinder
- b. Hydraulic Steering Cylinder

#### 10.9.2 <u>Inspection Items</u>:

- a. Ensure sensing paddle is moving with belt.
- b. Ensure steering cylinder is responding to sensing paddle.
- c. Ensure belt is tracking in approximately the center of the belt press.
- d. Ensure belt misalignment limit switches are functioning.

#### 10.9.3 Wear Strip Replacement:

- a. Shut down belt press and lock out controls.
- b. Unbolt wear strip from paddle.
- c. Position new wear strip on paddle and replace bolts.



#### ASHBROOK WINKLEPRESS HYDRAULIC CYLINDERS

#### **TENSIONING CYLINDERS**

Part Number:

027452

Mounting Style:

Flange Mounted

Service:

750 psig

Cushion:

Non-Cushion

Bore Size:

2 ½"

Stroke:

12"

Rod Diameter:

1 3/4"

#### STEERING CYLINDERS

Part Number:

026520

Mounting Style:

Double Rod End Tapered

Service:

1,000 psig

Cushion:

Non-Cushion

Bore Size:

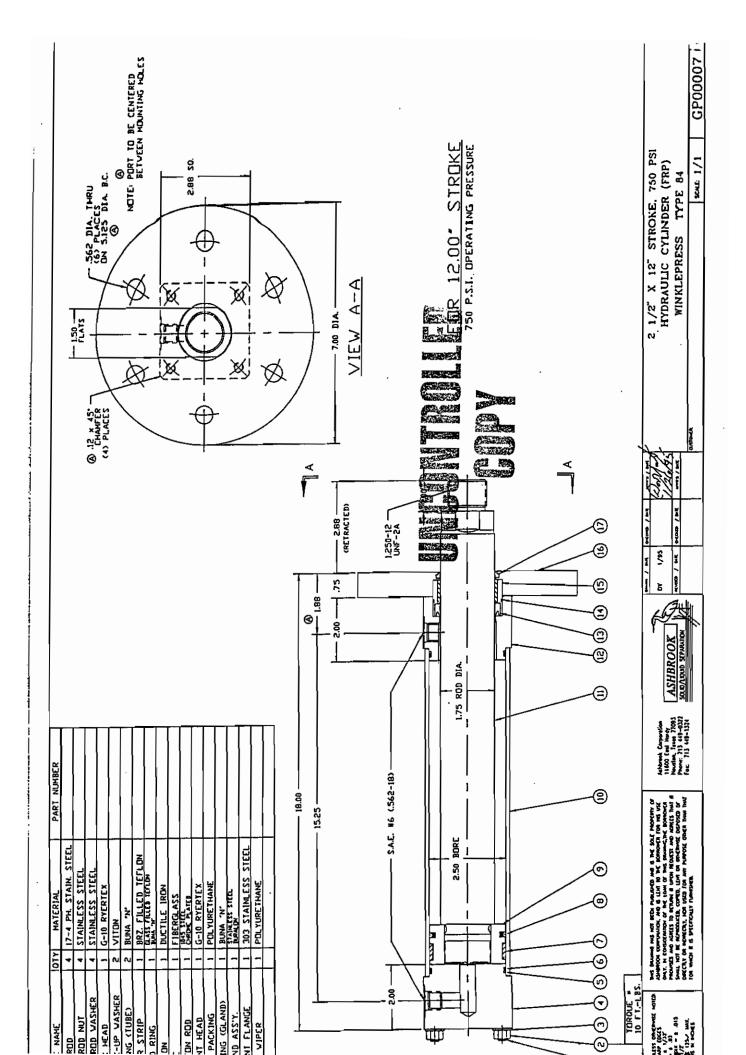
4"

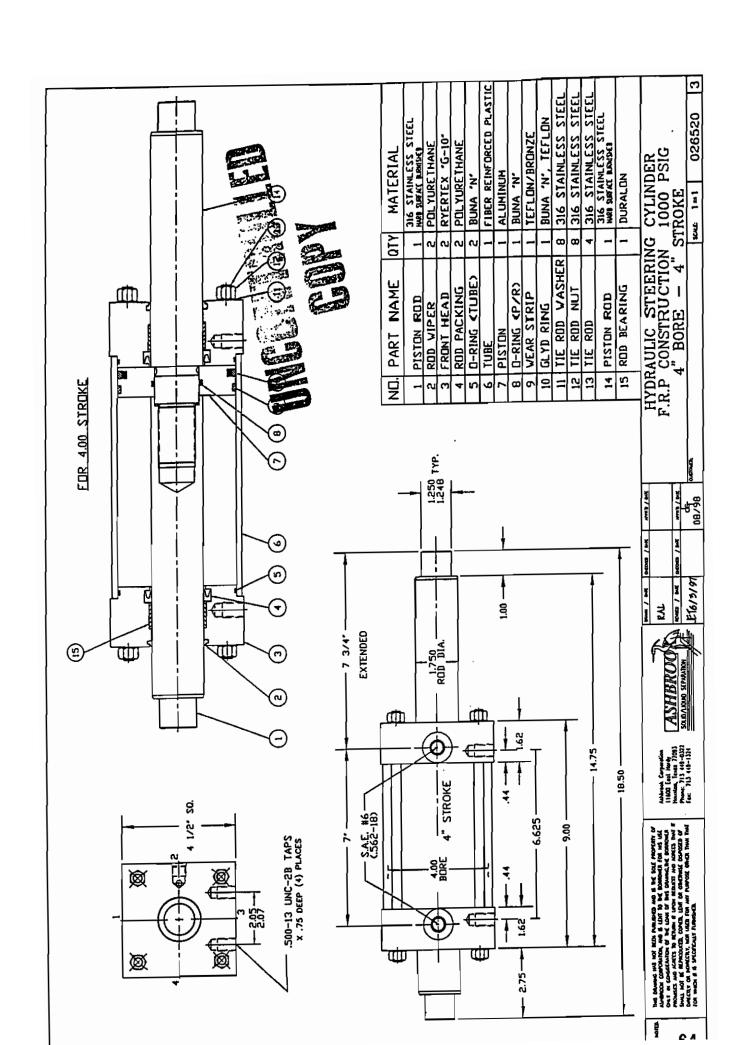
Stroke:

4"

Rod Diameter:

1 3/4"





#### 10.10 TENSIONING ASSEMBLY

10.10.1

#### 10.10.2 Inspection Items:

a. Inspect tension cylinders for leaks.

#### 10.10.3 Tension Yoke Cylinder Replacement:

- a. Shut down press and lock out controls.
- b. Disconnect hydraulic lines from cylinder.
- c. Remove clevis pins from cylinder.
- d. Reverse process to install new cylinder.
- e. Replace hydraulic lines.
- f. Check for proper belt tensioning operation before starting belt drive.

#### 10.10.5 Hydraulic Manifold Repair:

- a. Tension valve replacement
  - (1) Turn off pump.
  - (2) Screw out defective valve.
  - (3) Wash out port.
  - (4) Screw in new valve.
- b. Pressure reducing valve replacement.
  - (1) Turn off pump
  - (2) Screw out defective pressure reading valve.
  - (3) Wash out port.
  - (4) Screw in new pressure reducing valve.
- c. Pressure gauge replacement.
  - (1) Turn off pump.
  - (2) Screw out defective pressure gauge while holding the gauge snubber with a wrench to prevent it from turning in the manifold block.
  - (3) Wash out the port.
  - (4) Screw in new pressure gauge while holding the gauge snubber with a wrench to prevent it from turning in the manifold block.
- d. Pressure switch replacement.
  - (1) Turn off pump.
  - (2) Screw out defective pressure switch while holding the gauge snubber with a wrench to prevent it from turning in the manifold block.
  - (3) Wash out the port.
  - (4) Screw in new pressure switch while holding the gauge snubber with a wrench to prevent it from turning in the manifold block.

#### 10.11 HYDRAULIC POWER UNIT

The hydraulic pump and motor do not have parts that are maintainable in the field. If maintenance on these items is required, please call Ashbrook Service Department.

#### 10.11.1 Drawings:

a. Standard Hydraulic Unit: SK001603

#### 10.11.2 Filter Screen Cleaning or Replacement:

Note: Clean filerancen sem ennually (every stamonika). Renant tre tension cylinders to return most of the old to the reservoir. This will be purple more of the old old and prevent over filling the reservoir.

- a. Unscrew the bowl from filter body; catch the oil in a bucket.
- b. Remove and wash the suction screen. Be careful not to damage the screen.
- Reinstall the screen in the filter bowl. Do not operate without a filter screen installed.
- d. Screw the filter bowl back onto the filter body.
- e. Refill the hydraulic reservoir to the high level mark.

#### 10.11.3 Hydraulic Oil:

Moter Change the hydraulic off after the first 500 operating hours and anytime the off appears decolored, derivated or about 1. The hydraulic officencies of moisture from the atmosphere.

- a. Check the oil level when the tension cylinders are retracted. If the oil is too low, add sufficient oil to restore the proper level. Find and repair any leaks which caused the oil level to decrease.
- Inspect the level of the oil and its color. If the oil is discolored or cloudy, drain and replace.
- Hydraulic oil is drained by removing the filter bowl and catching the oil in a bucket.
- d. Properly dispose of any waste oil.
- e. Start the hydraulic unit and allow belts to tension.
- Retract the cylinders and check the level of the hydraulic oil in the reservoir and add oil as required.

#### TECHNICAL DATA SHEET

# HYDRAULIC POWER UNIT HIGH EFFICIENCY

1	VICKERS PRESSURE RELIEF VALV	E MODEL RV5-10.
1	VESCOR SUCTION STRAINER SS-3	MESH 100.
1		GAUGE (GLYCERIN FILLED), CALIBRATED () TO
•	1000 PSI WITH ACTUAL DEWATER	ING PRESSURE DISPLAY ON SECONDARY SCALE.
1	STAINLESS STEEL GAUGE SNUBBI	
i	NEMA B DESIGN MOTOR AS MAN	
•	ENCLOSURE:	TEFC
	FRAME:	145T
	NEMA DESIGN:	В
	INSULATION CLASS:	F
	HORSEPOWER:	1.5
	SERVICE FACTOR:	1.15
	VOLTAGE:	230/480
	FULL LOAD AMPS:	4/2
	FULL LOAD RPM:	1735
	PHASE:	3
	HERTZ:	60
	DUTY CYCLE:	CONTINUOUS
	KVA CODE:	Н
	AMBIENT TEMPERATURE:	40 DEGREES C (UP TO 75 DEGREES C MAX.)
	FULL LOAD EFFICIENCY: FRAME MATERIAL:	85.5%
	FRAME MATERIAL:	CAST IRON
	BEARING BRACKETS:	CAST IRON
	FAN MATERIAL:	PHENOLIC
	FAN COVER:	CAST IRON
	CONDUIT BOX:	CAST IRON
	UL RECOGNIZED:	
1	MOTOR GASKET	
1	PUMP/MOTOR ADAPTER	
1	DELTA POWER SERIES C-6 HYDRAU	
1	PNEU-TROL INLINE CHECK VALVE	
1	BARKSDALE PRESSURE SWITCH "I	
1	BARKSDALE PRESSURE SWITCH "I	
1	SIGHT LEVEL/TEMPERATURE GAUG	GE .
1	LENZ 8-03 FILTER ELEMENT	
1	FILTER BREATHER	
1	RETURN FILTER	
1	RELIEF VALVE ADJUSTMENT	•

20 GALLON RESERVOIR 316L STAINLESS STEEL

REMOVABLE TANK TOP 316L STAINLESS STEEL

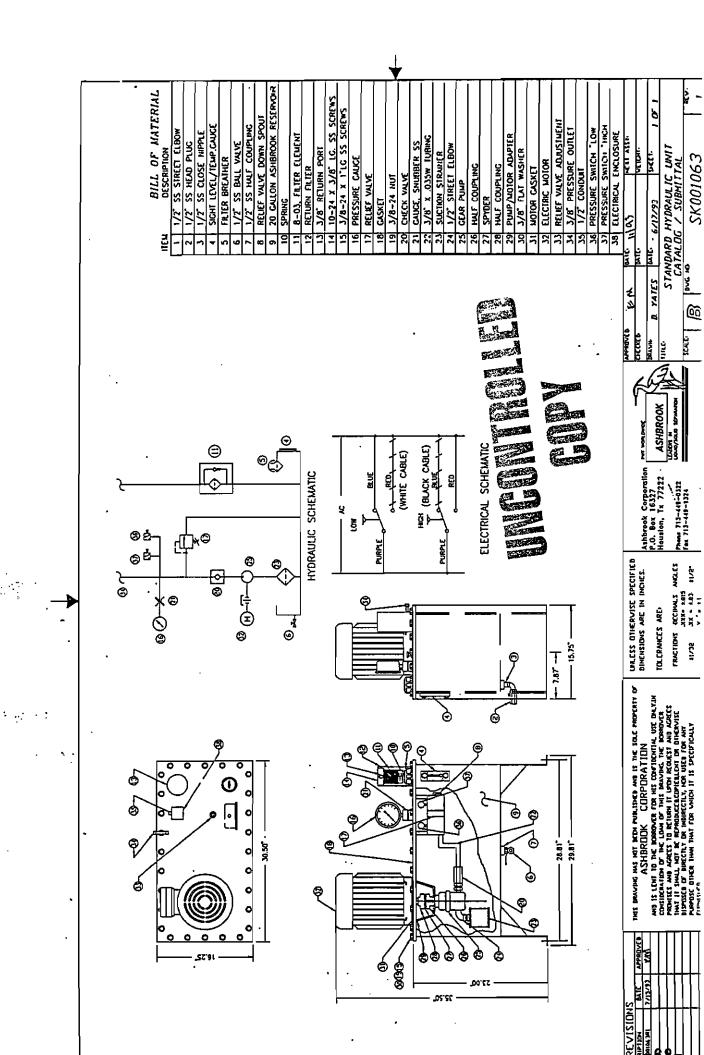
LANCE DRAIN STAINLESS STEEL BALL VALVE

RESERVOIR TANK GASKET

1

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1 1

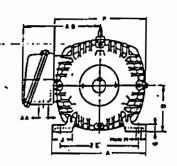


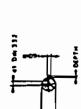
# Severe Duty Line NEMA Design B ratings Standard & Premium Efficiency

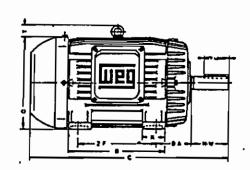


The WEG Severe Duty line of three phase motors is specially designed to work under special operating conditions in hostile environments without affecting their useful life. These motors are recommended for chemical plants, pulp and paper mills, fertilizer plants, foundries, marine duty, cement plants and many other applications where a standard motor is not suitable.

#### MECHANICAL DATA







As per Nema Standard MG 1.11.31

TOLERANCES:

Height D ≤ 8 = - 1/32 of frame up to 326 > 8 = 1/16 of frame 364 and above.

Shaft # U From 0.875 to 1.375 = 0.0005\* From 1.625 to 3.875 = 0.001\*

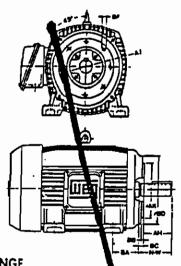
#### DIMENSIONS IN INCHES

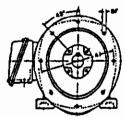
	<u>.                                      </u>							_										<u> </u>		•															
	NEMA		Моч	mting				١		6		K		,	,	Keyway		Key	Shaft E	Shaft Extension		_ w	dl	Bearings											
	Frame	2 E	2 F	H	M	^	•				'			_	Ľ	5	R	Lenght	H-W	U			_ ••	J.D.	3.Q.O										
	143 1	3.500	4.000	- 0.343	3 2.250	6,460	5.257		- 3.500	0.550	1_500	1,660	7,000	7.000	Ī.	0,187	0.766	1.417	2.250	0.875	5,905	NPT 3/4*			\$20±Z										
5	1451	1	5.000	<del>-</del>		-	6.141	_	_				4		<u> </u>																				
	142 T	7.500	4.500	0.404	2750	8.670	5.944	+	4.500	0.750	1.900	1.970	8.870	8.850	1.755	0.250	0.984	1,771	2,750	1,125	7.050	NFT I*		6307-2	62062										
	1841		5,500			<u> </u>	6.964	-		ļ	-	_			ļ																				
Į	2137	8.500	5.500	0.404	3.000	9.770		-	5.250	0.880	2.000	2.170	10.370	10.650	1.850	0.312	1.203	2.480	3.375	1.375	8.075			A308-Z	6207-Z										
ŀ	2151	<u> </u>	7.000	┈		-	1.250	-			<u> </u>		<del> </del> -	<u> </u>									4												
ŀ	2541	10.000	8.250	1220	4.250	12.130	10.100	_	á.250	0.820	2.520	2.560	12.370	12.500	1,950	0.375	1.406	2.755	4.000	1.625	10.390		.	4309 C3	6209-Z C3										
ŀ	256 7		10.000	<del> </del>	<del> </del>		11.73	24.970			<u> </u>			_	_			99.0				ł	A4		-										
ŀ	284 TS		9,500				11.574	25.055	1				1 4.000	'	١.	0.500	1.406	3.149	3.250	1.675		NFT 1-1/2"													
ŀ	284 T	11.000	<b>—</b> —	0.531	4.750	13,780	· <del> </del>	27,955	7.000	1.020 3.	1.150	2.960		14,100	2.950	0.500	1.504	3.149	4.625	1,475	11,190	٥		क्षा 🖰	6211-Z C3										
ŀ	286 13		11.000				13.070	26.555	1			1				0.375	1,406	1.968	3.250	1.625															
ı	324 T				$\vdash$			29.615								-	1,844	3.937	5.250	2,125			1												
ı	324 75		10.500				13.070	28.115				1					1.594	1,960	3,750	1.875															
ı	326 7	12.500		0.656 5.250	15.160	1	31.115	8.000	ן סובנו	J.230	3.350	15.700	15.600	2.520	0.500	1.844	3.937	5.250	2.125	11.750	NFT2"		4312 C3	62122 (3)											
ı	326 TS		12.000				14.566	29.615								1	1.594	1,968	3.750	1.875			1		i I										
	364.7	-						33,700		l	3.150 4.	0 4.140	-		1	0.625	2.014	4.330	5.875	2.375				814 C3	8314 CJ										
	364 13	14000	11.250	0.750	5.875	17 170	15.400	31.600	9.000					19,100		0.500	1,594	1,968	3,750	1.875															
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	104 (		12.250					38.100		•						0.750	2.453	3311	7.250	2.175				W) 31+CI											
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Ļ	405 T		13,750				,,,,,,,,	38.100				<b>3</b>				0.750	2.453	5.511	7.250	2.875		2 a N#T 2"		M 314 CI	2,.0										
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L	1111		14.500					43.950							L	0.875	2.875	7.086	_	3.375	- 1		UNC 3/4"	NJ 319 C3	4316 C3										
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⊢	4457	18.000	14.500	0.812	7.500			43.950	11.000	1.630	3.950	5.590	20.220	23.900	3.470 F		-		$\rightarrow$	3.375	18.150			NU 319 C3	6316 C3										
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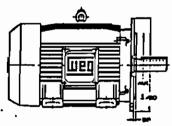
# INE Standard & Premium Efficiency



#### **FLANGE DIMENSIONS**







WEG also offers a complete line of motors suitable to work in hazardous locations:

- NEMA-T explosion proof motors - standard & premium efficiency
- NEMA 56 explosion proof motors - single & Ihree-phase

CSA & UL Approved

#### **C FLANGE**

	_									_
frome	BA.	~	AK.	30	<u>                                      </u>	Top Size	84	K	AH	l
143 TC	2.250	5.875	4.500			NC 3/8 - 16	0.156		2.125	l
162 TC	2.750				]	$\Lambda$		0.125	2.625	ľ
213 TC	3.500	7,250	8.500	8.875					3.725	
254 TC 256 TC	4.250					UNC 2-13			1.750	
26	.750	9.000	10.500	11,031	'				4.375 3.000 4.375 3.000	
326 TC	<b>5.250</b>								5.000 3.500 5.000 3.500	
364 TC 364 TSC 365 TC 365 TSC	5.075	11.000	12.500	15_562			250	0.250	5.875 3.500 5.875 3.500	
404 TSC 404 TSC 405 TC 405 TSC	4.425	'		.		UNC 5/8 - 1].	N		7,000 4,000 7,000	
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#### **D FLANGE**

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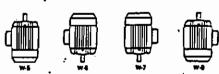
#### STANDARD MOUNTING **CONFIGURATIONS AND SYMBOLS**





CELLING MOUNTINGS





WALL MOUNTINGS, VERTICAL SHAFT



WEG ELECTRIC MOTORS CORP.

ENSTRUCTION DIVISION World Trace Cerear Belon Sute #2414 BALTIMORE, MO 21202 U.S.A. Phone (1-410) 576-9199 Fax (1-410) 576-9040

# Severe Dury Line NEMA Design B ratings

#### PERFORMANCE DATA

r	le	· · ·					locked	Pull	Locked	Break	.	Efficience	y 1%		pwer fa	cler (e) (		Mariera	Monoble	$\overline{}$
<u> </u>		put	NEMA Frame	Bated Speed	I UII LOI	ed Current	Rater	lood	Reter	down	; <del> </del>		•	of full lo			Sorvice Factor	mertiq	Locked Botor Time	Appres. Weight
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L	2	1.5	145 T 184 T 213 T	1720 1160 863	2.4 3.0 3.3	2.1 2.4 2.6	14.2 17.7 21.1	6.0 8 9 12.0	280 200 220	320 250 260	85.3 84,3 81.4	2 87 ( 84.	94. 1 87. 3 83.	5 0.7 5 0.3 5 0.3	4 0.8 4 0.8	1 0.85 3 0.72	1.13	0.1144 0.5560 1.5616	9/14 14/26 11/21	33 75 141
	3	2.2	182 T 182 T 213 T 213 T	3510 1760 1170 863	3.7 4.1 4.5 4.9	2.9 3.3 3.6 3.9	28.9 27.9 30.2 29.4	9.8 13.0 18.0	750 330 170 220	350 340 250 260	84 5 85 8 87.0 84.7	88 2	88.6	3 83	1 0.7	7   0.83 4   0.73	1.15 1.15 1.13 1.13	0.1745 0.2887 0.9579 1.7489	28/53 18/23 13/29 11/21	90 88 112 154
	5	3.7	184 T 184 T 215 T 254 T	3480 1750 1160 880	6.0 6.5 6.0 7.0	4.7 5.4 4.9 5.7	46.8 41.0 45.0 44.1	7.4 15.0 22.0 29.0	270 250 180 200	350 260 250 240	86.5 86.6 88,7 85.4	89.4	89.0	0.7	0.7	0.81	1.15 1.15 1.15 1.15	0.2195 0.3350 1.2428 2.0439	10/19 13/24 10/18 14/26	106 92 163 218
,	1/2	5.5	213 T 213 T 254 T 256 T	3500 1765 1170 860	8.5 9.5 10.0 11.3	6.7 7.5 8.0 9.1	56.1 63.7 60.0 63.3	11.0 22.0 33.0 44.0	250 280 200 190	250 280 230 230	87.0 89.3 88.6 86.5	91.0 89.9	80.9	0.70	87	0.83	1.15 1.15 1.15 1.15	0.5361 0.9654 1.8708 2.3029	14/24 13/24 8/14 13/29	121 136 235 277
\[	•	7.5	215 T 215 T 256 T 284 T	3490 1765 1170 885	11.0 12.5 12.5 15.0	8.8 10.0 10.0 12.0	77.0 81.3 80.0 79.5	15.0 29.0 44.0 58.0	250 300 200 220	300 290 240 250	87.6 90.8 89.4 88.9	90.6	91.8 91.8 91.0 89.7	0.73	0.80	0.80	1.15 1.15 1.15 1.15	0.5991 1.2398 2.3025 6.3983	13/24 11/26 8/14 10/19	161 152 282 374
1.	5	11	254 T 254 T 284 T 286 T	3500 1765 1170 840	16.5 17.5 17.5 19.0	13.0 14.0 14.0 15.0	107.3 115.5 115.5 115.9	22.0 44.0 66.0 88.0	280 300 220 200	260 250 250 230	87.0 91.1 91.2 89.7	89.8 92.1 91.8 90.3	91.5 91.9 91.7 90.2	0.83 0.75 0.82 0.72	0.83	0.89	1.35 1.15 1.15 1.15	1,2728 1,7136 6,3983 7,1618	25/48 14/26 8/15 11/21	253 240 306 422
20	,	15	256 T 256 T 286 T 324 T	3500 1765 1170 885	22.5 23.5 22.5 27.5	18.0 19.0 18.0 22.0	146.3 143.4 144.0 145.8	30.0 59.0 88.0 117	250 280 230 190	270 240 250 220	90.0 91.6 91.8 90.7	91.0 92.6 92.2 91.5	92.0 92.2 92.0 91.4	0.84 0.78 0.76 0.65	0.92 0.13 0.84 0.75	1 0.89	1.15 1.15 1.15 1.15	1.3821 2.0627 7.1618 9.0671	21/40 9/16 9/16 19/35	286 273 429 513
	,	8.5	284 TS 284 T 324 T 326 T	3545 1765 1180 680	27.5 29.0 29.0 34.0	22.0 23.0 23.0 27.0	181.5 182.7 182.7 183.6	36.0 73.0 110 147	240 230 200 190	250 · 250 220 220	88.0 91.8 92.1 91.1	90,1 92,9 93.0 91.9	92.0 92.7 92.9 91.8	0.85 0.76 0.76 0.68	0.90 0.84 0.83 0.73	0.90 0.87 0.87 0.76	1.15 1.15 1.15 1.15	3.2777 3.5748 9.0671 10.017	16/31 16/31 19/35 15/31	312 350 526 585
30	· ] ;	22	286 TS - 286 T 326 T 364 T	3540 1765 1180 885	32.5 84.0 35.0 39.0	26.0 27.0 28.0 31.0	214.5 214.2 217.0 218.4	44.0 88.0 132 176	260 220 200 180	260 230 230 230 220	89.6 92.0 92.7 91.6	91.6 93.2 93.4 92.2	92.5 93.0 93.3 92.0	0.86 0.79 0.75 0.63	0.90 0.85 0.80 0.74	0.91 0.87 0.86 0.78	1.15 1.15 1.15 1.15	3.8285 4.2084 10.017 22.091	16/31 -16/31 12/23 10/19	387 396 579 880
40	3	<b>20</b>	324 TS 324 T 364 T 365 T	3555 1770 1180 885	44.0 45.0 46.5 52.5	35.0 36.0 37.0 42.0	286.0 288.0 274.4 288.8	58.0 117 176 234	300 250 180 180	300 230 220 200	89.7 92.5 92.8 91.8	92.6 93.6 93.5 92.4	93.1 93.5 93.4 97.2	0.88 0.76 0.75 0.69	0.90 0.83 0.85 0.75	0.91 0.87 0.86 0.78	1.15 1.15 1.15 1.15	4.5702 6.9672 23.553 25.018	30/56 21/40 18/33 11/21	51.5 54.1 880 950
50	3	17	326 TS 326 T 365 T 404 T	3555 1770 1180 885	55.0 56.0 59.0 63.3	44.0 45.0 47.0 51.0	357.5 360.0 358.4 376.1	73.0 146 219 292	260 240 200 220	250 230 220 210	89.8 92.8 93.6 92.4	92.5 93.8 94.0 92.9	93.3 93.8 93.9 92.7	0.88 0.76 0.73 0.72	0.90 0.83 0.82 0.78	0.91 0.88 0.85 0.80	1.15 1.15 1.15 1.15	4,8775 7,9259 24,930 28,872	24/45 20/38 23/43 11/21	548 594 880 1137
40	4	5	364 TS 364 T 404 T 405 T	3550 1775 1180 - 885	66.5 67.5 70.0 74.0	\$3.0 \$4.0 \$6.0 \$9.0	430.6 432.0 434.0 435.1	88.0 175 243 351	200 220 200 170	280 230 230 210	91.0 92.9 94.0 92.6	92.5 94.2 94.4 93.1	93.5 94.0 94.2 93.0	0.86 0.84 0.74 0.73	0.89 0.88 0.83 0.79	0.90 0.89 0.85 0.82	1.15 1.15 1.15 1.15	9.2979 18.711 32.329 35.217	15/29 14/26 15/29 13/24	805 851 1085 1305
75	5.	5	365 TS 365 T 405 T 444 T	3550 1775 1180 885	82.5 84.0 89.0 95.0	71.0	536.3 536.0 541.4 541.5	109 219 329 439	200 230 210 160	* 250 240 230 200	92.1 94.0 94.2 92.9	93.0 93.0 94.5 97.4	93.7 94.3 94.3 93.5	0.87 0.85 0.70 0.68	0.89 0.88 0.79 0.76	0.90 0.89 0.84 0.79	1.15 1.15 1.15 1.15	10.431 20.363 35.483 64.510	13/24 18/33 13/24 18/33	913 898 1133 1481
100	7.	5	405 TS 405 T 444 T 445 T	3560 1775 1185 890	110 112 119 127	95.0 95.0	715.0 723.1 724.4 719.6	145 292 437 582	190 210 220 170	220 240 250 200	92.8 94.2 93.4 92.3	94.0 95.0 94.3 93.7	94.5 94.7 94.5 93.6	0.84 0.84 0.72 0.66	0.90 0.89 0.79 0.75	0.91 0.89 0.84 0.79	1.15 1.15 1.15 1.15	14.744 26.521 62.622 \$0.057	9/16 11/71 25/48 16/31	1203 1115 1540 1720
- 125	90	T .	444 T 444 T 445 T 504 T	3560 - 1780 - 1185 - 890	139 140 144 154	112	901.9 896.0 906.8 907.1	182 364 546 727	200 200 220 180	250 220 250 200	92.9 94.4 94.0 93.5	93.8 95.2 94.7 94.1	94.7 95.0 94.7 94.1	0.84 0.84 0.73 0.70	0.89 0.87 0.80 0.76	0.90 0.88 0.85 0.81	1.15 1.15 1.15 1.15	26.435 45.796 71.860 95.982	20/38 18/33 21/40 18/33	1621 1467 1476 2039
150	111	o [	445 TS 445 T 504 T 505 T	3565 1780 1185 890	176	134 141	1081 1055 1075 1080	218 436 656 873	190 220 190 170	200 220 220 200	92.9 94.8 94.4 93.4	94.2 95.6 95.0 94.0	95.0 95.4 95.0 94.3	0.84 0.85 0.70 0.64	0.89 0.88 0.78 0.75	0.90 0.88 0.84 0.80	1.15 1.15 1.15 1.15	29,632 54,758 81,903 113,30	31/59 20/38 16/31 18/33	1685 1661 1965 2768
200	150	o s	504 TS 504 T 505 T 86/7 T	1780 1185	224 232	179 185	1434	290 582 874 1185	250 230 200 100	210 240 220 210	93.0 95.0 95.2 94.0	94.0 94.8 95.8 94.5	95.0 95.8 95.8 95.2	0.85 0.85 0.77 0.60	0.89 0.88 0.82 0.71	0.90 0.88 0.85 0.76	1.15 1.15 1.15 1.00	34.370 65.187 116.01 346.00	34/64 24/45 18/33 28/53	1852 1991 2264 3806
250	18.5	'  \$	505 TS 505 T 86/7 T 86/7 T	1190	280   304	224 243	1854	363 727 1095 1464	200 · 210 180 100	270 230 210 210	93.4 95.0 93.6 94.0	95.0 95.9 94.7 94.7	95.6 96.0 95.5 95.5	0.88 0.82 0.68 0.60	0.90 0.87 0.76 0.71	0.91 0.88 0.90 0.77	1.15 1.15 1.15 1.00	43.664 79.587 231.00 450.00	34/64	2044 2211 3597 4235
300	220	)   3	16/7 15 56/7 [ 86/7 [	1790 1190	362   3	71 2	2136 172	434 866 302 741	110 170 180 100	210	94.0 95.0 93.6 94.0	95.1 95.6	95.5 96.2 95.5 95.5	0.87 0.50 0.69 0.60	0.88 0.84 0.76 0.62	0.89 0.85 0.80 0.77	1.00 1.15 1.15 1.00	89.560 182.00 306.00 475.00	34/64 26/49 35/66	2970 3432 4081 4466
	250	5	6/7 IS 86/7 I 86/7 I	1190   4	365 184 410 434	106   2 128   2	381   1 501   1	1480 1480 1493	100 180 180 110	210	93.0 93.6	95.1 95.6 94.8	95.5 96.2 95.7 95.5	0.87 0.80 0.70 0.60	0.88 0.84 0.77 0.64	0.90 0.85 0.80 0.78	1.00 1.15 1.00 1.00	98.420 196.00 326.00 484.00	35/60 24/45 30/37	3201 3894 4312 4620
400	300	)   SI	16/7 I	3570 1790 1190	(38 (55 (93	164 2	1821   1	592 180 776	100 180 180	200		95.1 95.6 94.8	95.5 96.2 95.7	0.87 0.81 0.70	0.89 0.85 0.78	0.90 0.86 0.90	1.00 1.15 1.00	113.60 218.00 346.00	30/56 18/34 32/60	3663 4279 4354
450	330	58 51	6/7 IS 16/7 I	3570 1790		85 00 3	150 I	31 298	110 180	200 200	94.0 95.0	95,1 95.6	95.5 96.2	0.87 0.81	0.89 0.85	0.90 0.84	1.00	150.00 234.00		4180 4796

#### adard Features

- \* Class "F" insulation
- Corrosion resistant finish & hardware
- 3 phase, 208-230/460, 460 or 575 V
- ★ 60 Hz (50 Hz also available)
- ★ Squirrel cage rotor, cast iron frame
- \* From 143T to 586/7T frame
- ★ Enclosure: TEFC
- Continous duty

reduces noise.

um die cast into a etic steel lamination

ynamically balanced for smooth operation, reduced vibration and less noise.

- 104°F (40°C) Ambient temperature
- Altitude: 3300 ft [1000m]
- Service factor: 1.15
- Thermistors from 324T and up
- Double vacuum pressure impregnation (364T and up)
- Sponge at the outlet leads passage [betwen frame and T box]
- See others standard features in the picture below

#### **Optional Features**

- \* Roller bearing on drive end
- ★ Labyrint TACHONITE (frame 213T and up)
- \* NILOS ring (143T up to 184T frames)
- \* Second shaft end
- ★ Shaft dimensions to customer requirements
- \* Motor whith cannopy [drip cover] for shaft down applications
- ★ Also available in IEC frames, 50 or 60 Hz
- ★ Stainless steel shaft
- ★ class H insulation
- ★ Thermistors, thermostats or calibrated resistances for all frames, in the winding or/and in the bearing

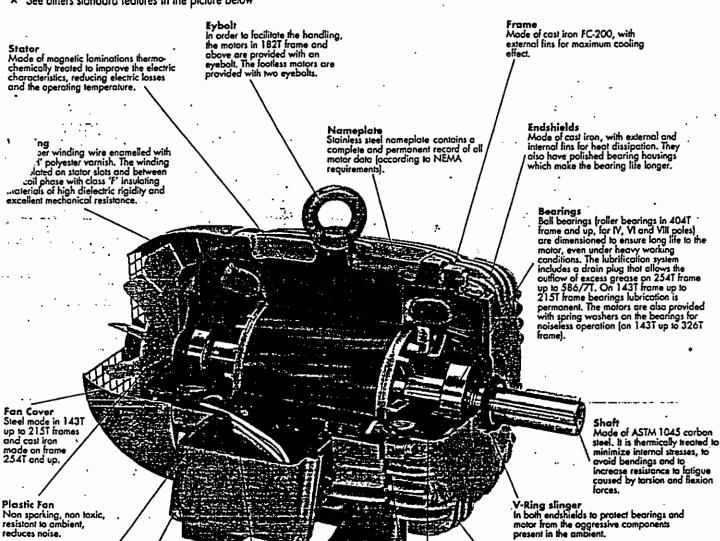
Drain Plugs

occumulation

Internal primer coat

Provided with plastic drain plug for quick draning of any condensate

- Cable glands
- \* Grounding extend into frame



Oversized Terminal Box

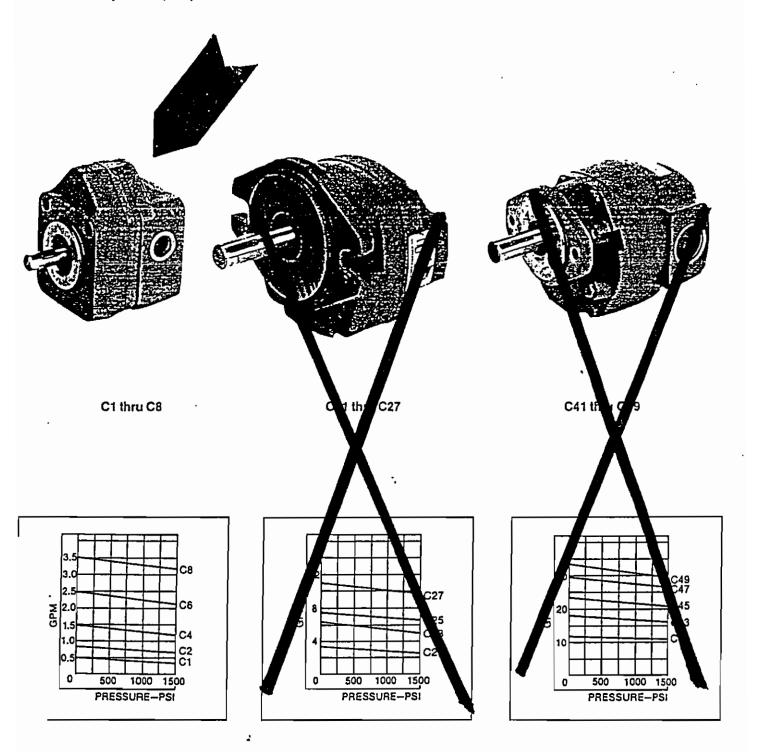


# "C" Series

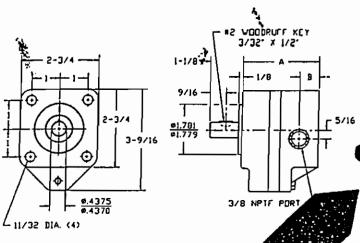
#### **Pumps**

...I Series C pumps are bi-directional. Series C pumps have high-strength, cast iron bodies with precision machined filling and trapping grooves, leaded bronze bearings, hardened alloy gears and shafts, Buna N seals and O-rings, all contributing to the line performance of Delta Power Hydraulic pumps.

The three series available are produced from three basic sizes of external gear sets. They are intended to be directly driven at speeds up to 5000 RPM at pressures up to 2500 PSI.

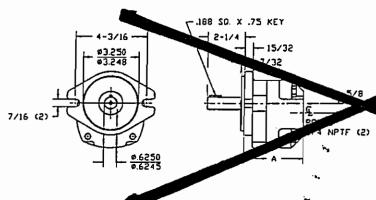


### Specifications and Performance Data



Şin	GPM 31 1750 8PM	0-751 <sup>-7</sup> 6sl./ Am.	Dispi. Cu. in./Rey.	Silp GPM/ 100 PSI	Pres. Pump Max. Ester- mittent	Pres. Pump Max. Con- Unixous	Speed MLI RPM	Dims. A	Direc.
CI	.49	.00028	.065	.015	2500	1500	5000	2.48	11/16
ន	.82	.00047+	.108	.017	2500	1500	5000	2.57	11/16
					<b></b> :	- ;	4		
C6	2.39	.00137	.316	.025	1850	1500	3000	3.02	11/16
			, ·	*:					1

SAE 4F17 MOUNTING FLANGE



Size	GPM #1 1750 RPM	O-P\$i Eal./ Rev.	Olspl.	100 PSI	Pres. Pump Max. Inter- mittent	Pres. Pump Max. Con- Unyous	Speed Max. RPM	Dimz.
C21	.11	.00178	.411	.040	2500	1500	5000	3.21
	5.30	.00304	.702	.045	2350	1500	4000	3.56
C25	7.42	JEDO.	981	.055	1500	1500	3000	3.78
C27	11.10	.00633	1.45	.075	1200	1000	1800	4.21

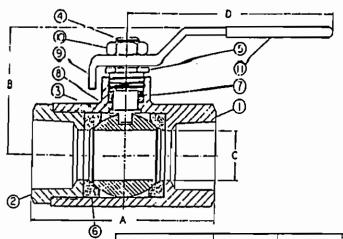
SAE "A" 2 BOLT MOUNTING FLANGE

.188	A A	
1-7/8 3-11/16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7/16 DIA (2) 29/32	

Size	6PM # 1750 RPM	0-PSI 6±L/ Rev.	Displ. Cal.	SIIp GPY	er jum.	Fres. Pump Mex. Con- Enuous	Speed Max. RPM	Dims.	Dienst.
CAI	11.0	di0	1.57	.07	2500	1500	4000	5.41	4-7/32
C43	17.80	.01020	2.35	.09	2450	1500	3000	5.72	4-19/32
C45	ğ	01320	3.04	.11	1850	1500	2300	6.06	4-15/16
C47	29.50	.01690	ŝ	7	1500	1200	1800	6.47	5-13/32
C49	33.60	.01920	4,43	.18	É	700	1800	6.72	5-19/32

Values are average at viscosity of 150-200 SSU

#### AVAILABLE IN FIRESAFE DESIGN



PRESSURE RATING SIZES: 1/1" 2000 WOG 1 %"-2" 1500 WOG 150 WSP

1 - BODY - ASTM A-351-748 CF8M Stainless

2 - END CONNECTOR - ASTM A-351-74B CF8M AISI T-316 Stainless Steel

3 - BALL - AISI T-316 Stainless

4 - STEM - AISI T-316 Stainless

5 - GLAND NUT - AISI T-316 Stainless

6 - SEATS - Glass filled Teflon

7 — STEM PACKING — Glass filled Teflon\*

8 - STEM BEARING - Glass filled Teflon®

9 - HANDLE - AISI 304 Stainless

10 - HANDLE NUT - 18-8 Stainless

11 - HANDLE GRIP - Vinyl

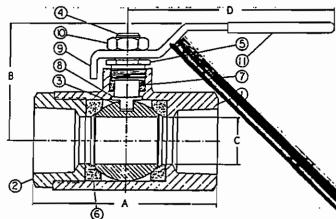
PART NO.	SIZE	Α	В	С	D	Cv
22-021	4	2-1/4	1-4	34	3.4	5.3
22-031	4	2.1/4.	1-14	*	3.4	5.3
22-041	4	2-1/4	1-17/4	<b>%</b>	3.1/4	9.8
22-061	%	3	2.4	11/1.	4.1/4	18
22-081	1	3.%	2.1/4	4	4-4	32
22-101	1-4	4	2-4	1	5-1/4	40
22-121	1-¼	4-%	2.14	1-4	5-4	75
22-161	2	5-1/4	3.1/4.	1-1/2	5-1/2	98

The state of the s

Conforms to Federal Spec: WW-V-35B, Type II, Class C, Style 3, End Connection A. Meets NACE Std. MR-01-75

#### CARESTONI CHIEFEIL = THE REPAID





PRESSURE RATING SIZES: 14"-1" 2000 2 1-14"-2" 1500 W 150 WS

AISI T-316 Stainless

5 - GLAND NY 6 - SEATS 7 - STEM 8 - STEM as filled Teflon\*

KING — Glass filled Teflon\*

ARING - Glass filled Teflon\*

LE - Steel, Plated

TOLE NUT - Steel, Plated

NDLE GRIP - Vinyl

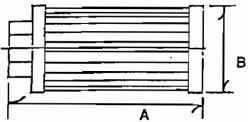
: Stainless Stem & Gland Nut Standard

					_	
PART NO.	SIZE	A	В	l c	D	Cv
23-021	1/4		1-14		3-%	5.3
23-031	3/4	2-4.	1-%	3	3.%	5.3
23-041	1/4	2-1/4	1- <sup>13</sup> %,	1/4	18	9.8
23-061		3	2.4	"አ•		18
23-081		3-%	2.4	74	4-7	32
23-101	1-1/4	4	2.4	1	5-14	40
23-121	1-%	4.14	2-14	1-14	5.1/2	75
	1					

# VESCOR SUCTION STRAINER TECHNICAL DATA

#### **SPECIFICATIONS:**

Stainless Steel Mesh
Reusable
Epoxy Bonded Joints for
Compatibility With All Fluids
Rugged Steel Inner Support
Plated End Caps
100 Mesh From Stock



#### **ORDERING INFORMATION:**

Model: SS-3

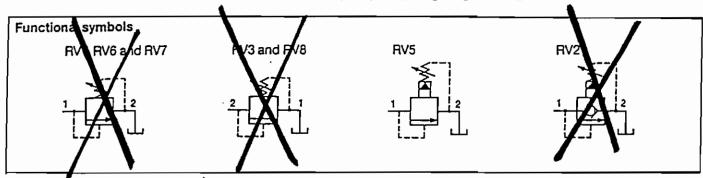
Nominal Flow: 3 GPM (11 L/Min)

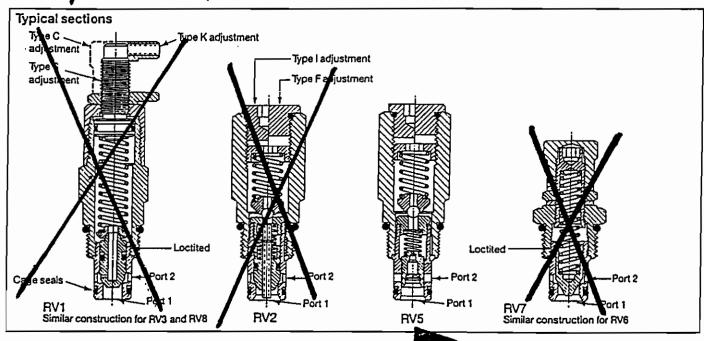
Pipe (NPT): 3/8 in.

Filter Area: 3/4 in<sup>2</sup> (220 cm<sup>2</sup>)
Dimension A: 3.56 in. (90 mm)
Dimension B: 2.63 in. (67 mm)

## Pressure relief valves

RV1/2/3/5/6/7/8-10





#### Model and ordering code

RV \* (A)-10(V)-\*-\*\*-\*\*/\*\*

12 34567

1 Type and	l max. power	capaci	ty
------------	--------------	--------	----

Code	Description Also see "Functional symbols" section	Max. pressure bar (psi), all ports	Rated flow Vmin (US gpm)	
1	Direct-acting poppet type	207 (3000)≡	38 (10)	
2	Two-stage poppet type	207 (3000)	114 (30)	
3	Direct-acting poppet type	207 (3000) 🗷	76 (20)	
5	Two-stage spool type	207 (3000)■	114 (30)	
6	Direct-acting ball type	207 (3000)■	15(4)	

2 Cage seals

Blank = For standard valves; seals as shown above.

= Back-up ring on both sides of O-ring. Option for RV3, 5 and 8 models if high pressure is to alternate between both ports e.g. in cross-line relief packages, see CRV3-10 models.

#### 3 Fluid compatibility

Blank = Antiwear hydraulic oil

 As above or with phosphate-ester (not alkyl type)

#### Cracking pressure setting adjustment

C = Cablanonut

F = Factory-set, see 6 A

I = Internal A

K = Knool

S = Screw A
A Cotions not available with RV6 and RV7

#### [5] Form

0 = Carridge only

In light-duty housing; 207 bar (3000 psi) max.

6T = With SAE 6 size ports

In NFPA fatigue-rated housing; 207 bar (3000 psi) max.

6H = With SAE 6 size ports

8H = With SAE 8 size ports

2G = With GW\* (BSPF) size pons

3G = With G% (BSPF) size pons

#### 

RV1 models #

3 = 3,45-20.6(50-300)

9 = 6.9-62.0(100-900)

18 = 17,3-124(250-1800)

#### RV2 models x

3 = 3,45-20.6(50-300)

20 = 6.9 - 137 (100 - 2000)

#### RV3 models x

3 = 3.45 - 20.6(50 - 300)

6 = 6.9 - 41.3(100 - 600)

9 = 13,8-62,0 (200-900)

15 = 20.7 - 124 (300 - 1300)

27 = 0.189(0.2750)

#### RV5 models ¥

3 = 3.45 - 20.6 (50 - 300)

20 = 6.9 - 137 (100 - 2000)

#### RV6 models x

25 = 3.45 - 172(50 - 2500)

#### RV7 models

2 = 1.73-17.2(25-250)

5 = 3.45 - 34.4 (50 - 500)

10 = 17.3-68.9(250-1000)

#### RV8 models #

4 = 3.45 - 31.0(50 - 450)

12 = 6.9-85.2(100-1250)

25 = 17.3-172(250-2500)

A Differential pressure, intet-outlet

For higher pressure moders, consult your local sales engineer

# Factory-set cracking pressure Within ranges in 3 above

Slank = Normal factory setting, at approx, mid-range

User-requested settings in 3,45 bar (50 psi) steps, coded as in following

examples:

10 = 68.9 bar (1000 psi)

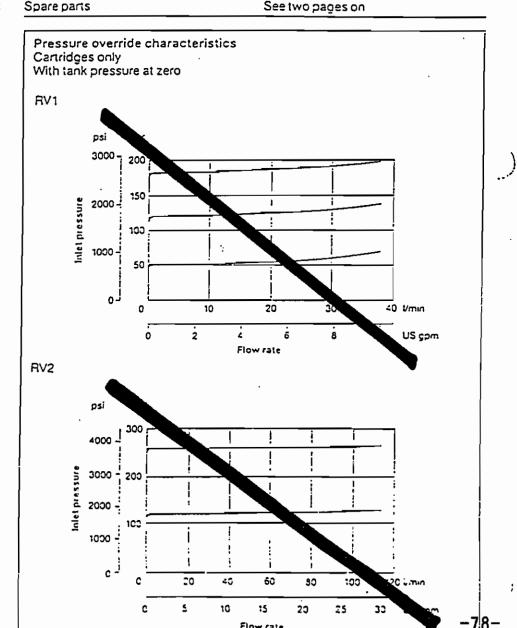
Operating data Performance cata is typical with fluid at 28 cSt (132 SUS) and 38°C (100°F) See 6: and 77 in "Model code" Cracking pressure adjustment range See Tiin "Model code" Max, power capacity Pressure overrige characteristics See graphs below and on next page Re-seat pressure: RV2 and RV5 valves Approx. 5.2 bar (75 psi) below cracking pressure Approx. 90% of set cracking pressure All other models Hydraulic fluids, temperature ranges See [3] in "Model code" on previous and filtration recommencations page, and also page 259 Installation dimensions, cartridge only See two pages on C-10-2 Cavity size For dimensions see page 240 Mass, carridge only 0.22 kg (0.48 lb) approx. Housing options: Standard light-duty type See page 246

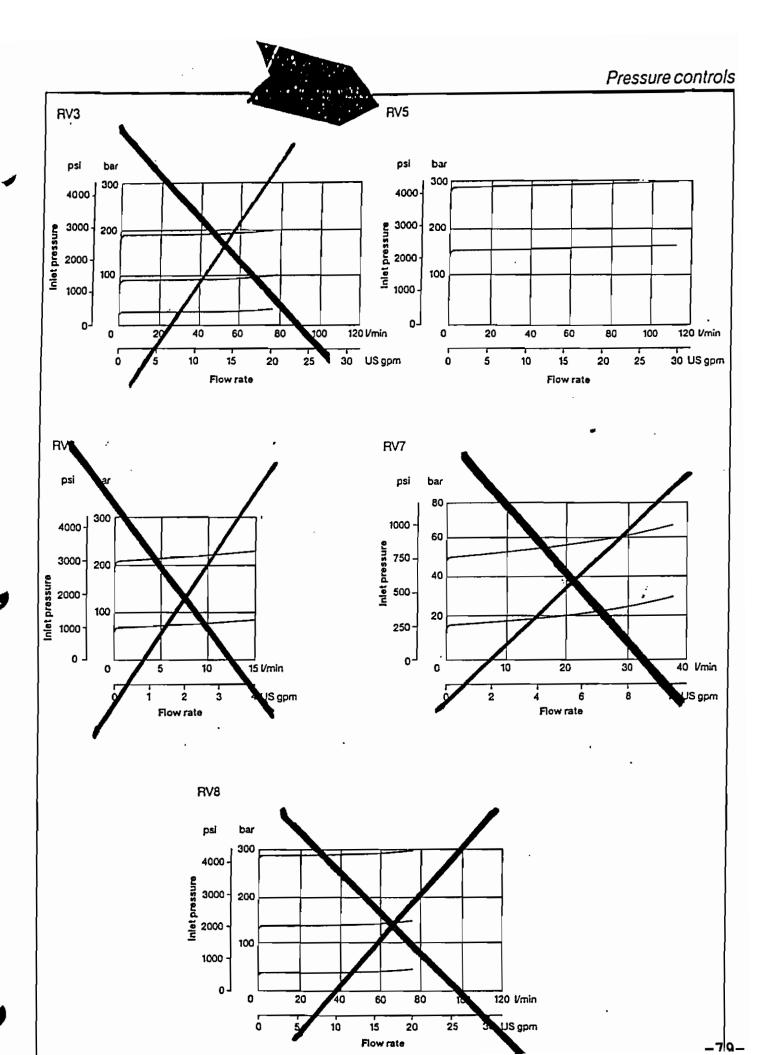
See page 244

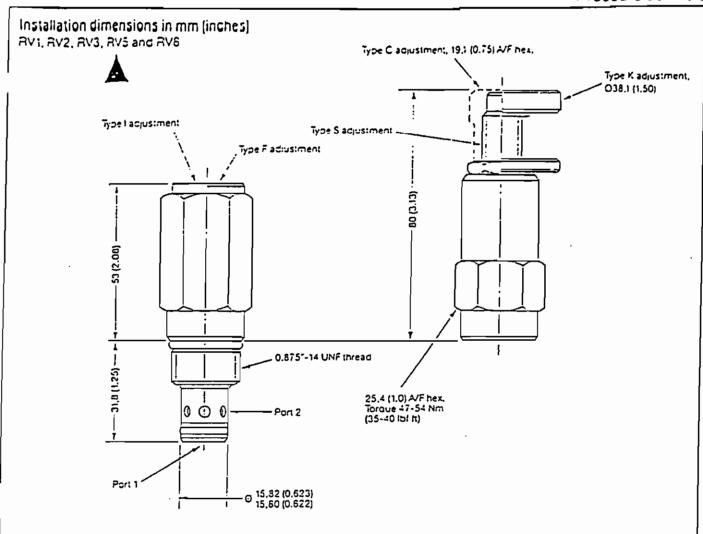
Consult your local sales engineer

Standard fatigue-rated type

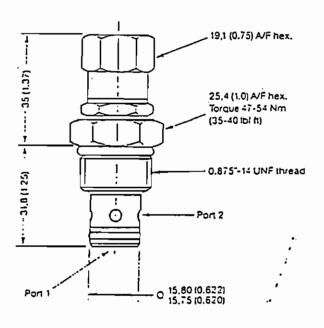
Customized types







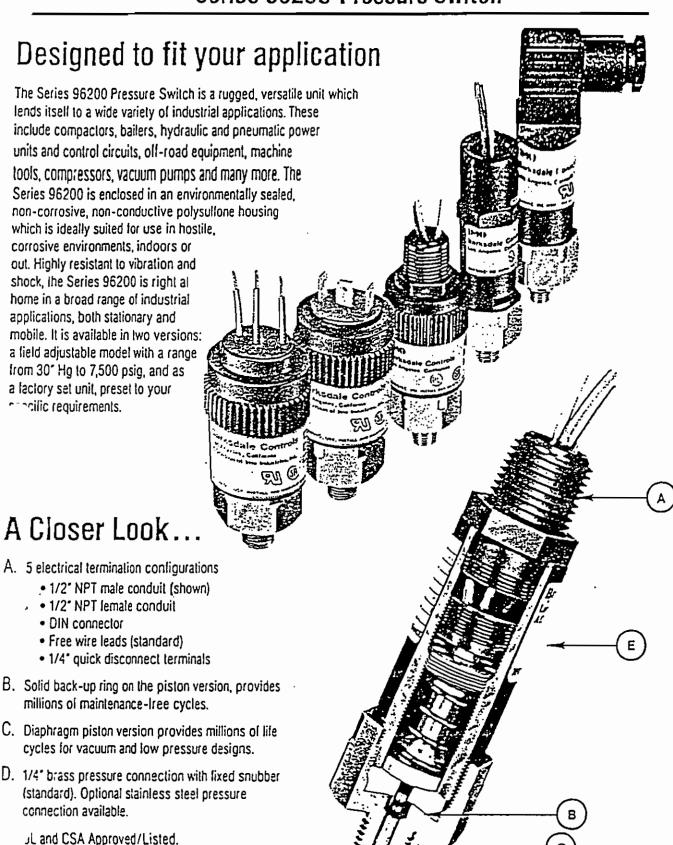
#### RV6 and RV7



#### Port data

For cartridge	Port				
	Identity	Function			
RV1, 2, 5, 6 & 7	1	Pressure Tank			
NV1, 2, 3, 0 & 7	2	Tank			
FV3 & 8	1	Tank			
UA200	2	Pressure			

### Barksdale Series 96200 Pressure Switch



## Barksdale

#### **Factory Set Pressure Switch**



General	Descrip	tion
---------	---------	------

The 96200 series switch utilizes a sealed piston sensor. The 96210 and 96220 series switches use a diaphragm piston sensor.

Each switch is factory set to meet your specific application requirements. The differential is fixed and varies with pressure setting. Electrical Connections include free leads as standard with optional spade terminals, DIN type connector or 1/2" NPT conduit connector (male or lemale).

These lactory sel pressure switches are environmentally sealed and ristant to shock and vibration. Designed to deliver millions of vice free cycles, the sealed piston and diaphragm piston , are ideally suited for harsh environments,

			Operal	Ing Charac	teristics		
	P	C SIU2251	etling Rac	ige	Approx.	0	Catalon
Range	Decr	easing	Incr	easing	Actuation Value	Pressure	Catalog Humber
	Min.	Mar.	Mła.	Mar.	(Differential)		
30° lig (Vac)	1" Hg	28.1ld	G. Hig	30° Hg	1-6'1lg	30 psi	96220-881*
15	2.5	12.8	3	15	5-22	1000	96210-881
35	5	31	6	35	1,0 - 4 0	1000	96210-B82*
50	8.5	44	10	50	1.5 - 6.0	1000	96210-883
125	22.5	112	25	125	2.5-13	1000	96210-884
250	70.0	220	80	250	10-30	1000	96210-885
500	116	440	130	500	20 - 60	1000	96210-886
600	190	450	250	600	60 - 150	7000	96200-B81
1700	350	1450	430	1700	70-250	7000	96200-882
4400	1450	3900	1650	4400	200 - 500	7000	96200-B83
7500	3650	6700	4000	7500	350 - 800	12000	96200-B84

Detail Data

**Electrical Connection** Free leads approximately 12" long.

Pressure Connection 1/4" NPT male.

96200 series - - 40° lo 165°F. 96210 series - - 20° lo 165°F. Temperature Range

(\*O\*F Min, as noted)

96220 series - 0° to 165°F.

Welled Malerials 96200 series

Body - Brass Seals - Buna N o'ring

Piston - Slainless steel

Open type plastic housing.

UL and CSA recognized. Approvals/Listings

Optional Modifications

Housing

Electrical

Wetted Material

Diaphragm/Seal

Process Connection

See Optional Modification Page. Body: Stainless steel. To specify, add sulfix -SS to catalog number.

Other compounds available. Consult factory.

7/16-20 SAE type male straight threads with o'ring seal, add sullix -P1. 1/4" BSP male straight threads with o'ring seal, add sulfix -P3.

96210 & 96220 series

Diaphragm --- Buna N

Body — Brass

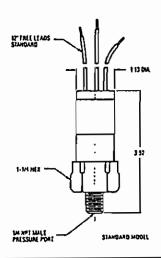
To ensure correct switch is furnished, always specify full catalog number Ordering Instructions (including required modifications), set point (increasing or decreasing) and service. Example: 96210-BB2-SS-T2 set at 15 psi increasing. Service, Dry

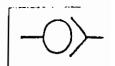
Nitrogen.

WIRE COOE	PRESSURE	VACUUM
Lead	Color	Color
Normally Closed	Blue	Red
Common	Purple	Purple
Normally Open	Red	Blue

ELECTRICAL RATING					
Limit Switch	Voltage (Volts)		Continuous (Amps)		
Class	( taits)	Resistive	Inductive		
88	125/250 VAC	5	5		
CC	125/250 VAC	10	10		

's incorporate Underwriters' Laboratories, and CSA approved single pole double p-action switches.



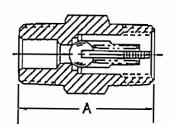


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#### (Pncu-Trof

#### INLINE CHECK VALVES

- · Soft Seat for Bubble-Tight Seal on Gas
- · Metal-to-Metal Seat for Leak-Tight Seal on Liquids
- · Compact Over-All Length
- · NPTF Threads Standard
- Maximum Operating Temperature 240°F (115°C) Standard





#### **DIMENSIONS**

		В		GPM	Max. Oper. Pr	ress. PSI (Bar)
Size	Α .	HEX	Cv	(L/min)	Brass	Steel & S.S.
1/8*	31/32 (24.5)	7/16 (11.0)	.17	1.0 (3.8)	2,000 (138)	-
1/4*	1-3/8 (35.0)	5/8 (16.0)	.56	2.5 (9.5)	2,000 (138)	3,000 (207)
3/8*	1-5/8 (41.5)	3/4 (19.0)	1.31	6.0 (23.0)	2,000 (138)	3,000 (207)
1/2*	2-1/16 (52.5)	7/8 (22.0)	2.71	10.0 (33.0)	1,000 ( 69)	2,000 (138)
3/4*	1-1/4 (31.5)	1-1/8 (28.5)	3.40	15.0 (57.0)	2,000 (138)	3,000 (207)

( ) Parentheses = Millimeters

#### ORDERING INFORMATION

METAL-TO-METAL SEAT

		DESCRIPTIO	N
· Size	Brass :	Steel	St. Steel ·
1/8*	CMM10B1	-	
1/4*	СММ20В	CMM20S	CMM20SS2
3/8*	CMM25B	9	_
· 1/2*	СММ30В	n na N	_

#### **EOFT SEAT**

		DESCRIPTIO	N
· · · Size	458	Steel	St. Steel
1/8*	CMMOTO		-
1/4*	CMMQ20B	19205	CMMO20SS2
3/8*	CMM	CMMOZ	CMM0255S
1/2"	B0CDIvin	CMMQ30S	
	CMMQ35B	_	-

#### **SPECIFICATIONS**

Standard Cracking Pressure 1 PSI to 2.5 PSI (.07 to .17 bar) Other cracking pressures available. Consult factory.

Operating Temperature (Soft Seat Only), Buna N Maximum Operating Temperature 240°F. (115°C).

Other materials available. Consult Factory.

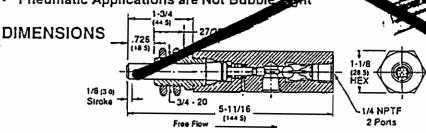
Threads

CMMQ33B = -

## Pneu-Tro

# PLUNGER OPERATED CHECK VALVES

- Normally Closed, Push to Open
- For Hydraulic or Pneumatic Operation
- 5 GPM (19 L/min) Rated Flow
- Cv Factor is .54
- 3,000 PSI (207 bar) Operating Pressure (Non-Service
- Pneumatic Applications are Not Bubble Tong



Plunger Effort per 1,000 PSI (69 bar) Is 70 lbs. (311 N).

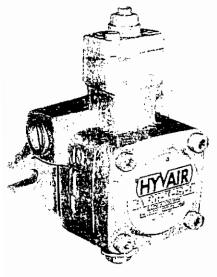
MATERIAL DART NUMBER



**Vane Pumps** 

PRESSURE COMPENSATED, VARIABLE VOLUME

SAE A, 2-Bolt, Flange Mounted

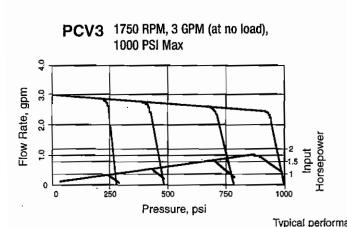


Series PCV3/ PCV5

#### FEATURES

- Variable Volume, Pressure Compensated Design: Reduces heat, noise and horsepower requirements. Pump maintains constant pressure while matching system flow demands.
- Simplified Circuit Design: Direct spring operated compensator, no safety relief valve required.
- ✓ Quiet Operation: Noise levels as low as 67 dBa.
- Compact and Simple Design: Dependable operation- compensator not prone to contamination.
- ✓ Long Service Life: Sturdy construction, precise machining ensures durability.
- Volume Adjustment Standard: Pumps can be reduced as much as 50% of total maximum displacement.

#### **Specifications**

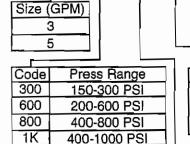


Typical performance curves based on ISO VG46 Oil @120°F, (49°C)

# PCV5 1750 RPM, 5 GPM (at no load), 1000 PSI Max

#### Ordering Information

PCV3 - 1K - 2AK -



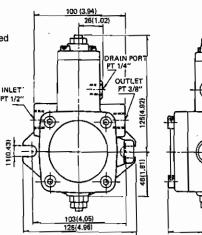
Note: Available right hand rotation (only)- viewed facing pump shaft.

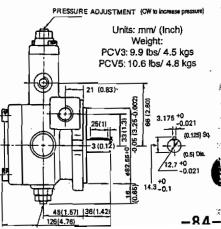
Series 1 Porting 1/2" inlet, 3/8" outlet, 1/4" case all female NPT

Mounting Style

2-Bolt, SAE A, 1/2" Dia. Keyed Shaft x 1.42" Long w/ 1/8" Key, Flow Adj. Std.

#### **Dimensional Data**





#### 10.12 FEED ASSEMBLY:

#### 10.12.1 Feed Assembly:

The Winklepress is equipped with an inlet feed spreader in the form of a flattened funnel that transitions the flow from the circular pipe diameter to a sheet of fluid extending across the entire working width of the belt on the gravity drainage deck. At the widest part of the feed funnel where the fluid is discharged onto the belt there is a rubber flap attached at the top edge of the feed funnel and hanging down over the opening to suppress splashing and assist with the final leveling of the incoming fluid. There is another rubber flap attached to the bottom edge of the feed funnel to form a seal to prevent the incoming fluid from flowing backwards underneath the feed funnel.

The feed inlet spreader funnel requires minimal attention. At initial start up the funnel outlet edge is adjusted to be level with the belt. Check the height at both sides of the outlet end of the funnel periodically to see if it may have moved. Reset it level if necessary. Also, check for wear on the lower rubber flap seal that lies on the belt. It is a wearing part and will have to be replaced when it wears to the point that fluid leaks under the feed inlet.

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#### 10.13 GRAVITY DRAINAGE SECTION:

#### 10.13.1 Drawings:

- a. SK001607 Upper Grid Assembly
- b. SK001609 Wedge
- c. SK001602 Drain Tray Assembly
- d. SK001599 Chicane Group Assembly
- e. SK001605 Upper Sludge Restrainer Assembly

#### 10.13.2 Wear Strip Replacement:

#### Note: Replace grid strips before belt contacts metal support grid.

- a. Shut down belt press drive.
- b. De-tension belts and shut down all belt functions.
- c. Lock out machine controls.
- d. Raise sludge side restrainers.
- e. Pull out and dispose of worn wear strip.
- f. Insert new wear strip and tap into place with rubber mallet.
- g. Unlock controls and start hydraulic unit, tension belts.
- h. Lower sludge restrainers into place.

#### 10.13.3 Sludge Restrainer Adjustment:

- a. Loosen side bolts in supporting brackets.
- b. Raise or lower restrainers until seals are touching the belt.
- c. Tighten bolts.

#### 10.13.4 Seal Replacement:

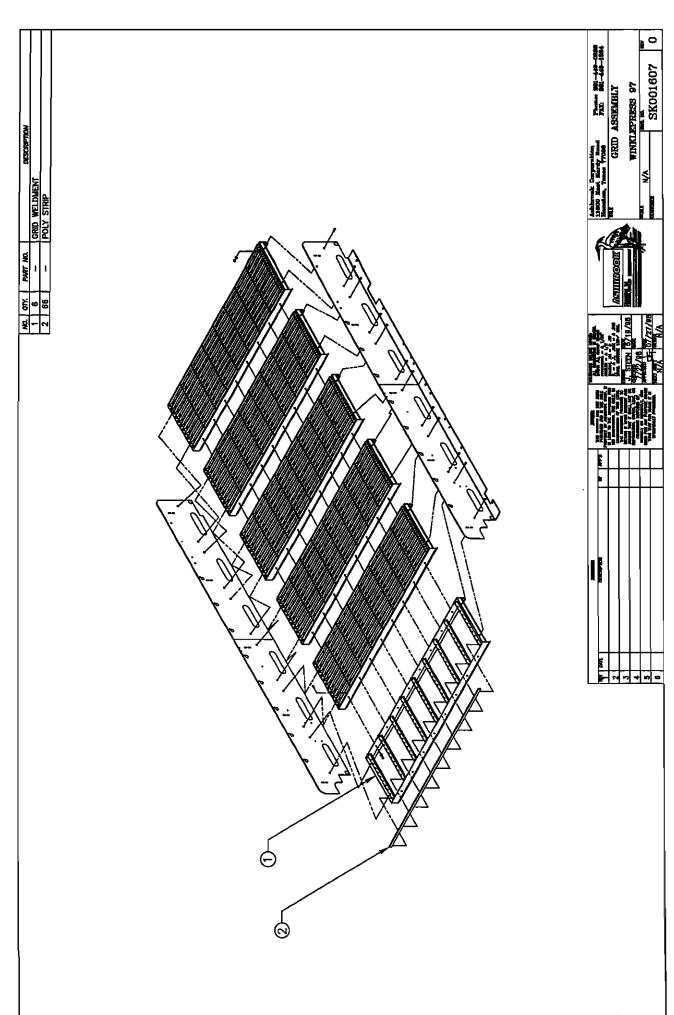
- a. Raise side restrainers.
- b. Remove old seals and discard.
- c. Install new seals on restrainers.
- d. Lower side restrainers and tighten bolts.

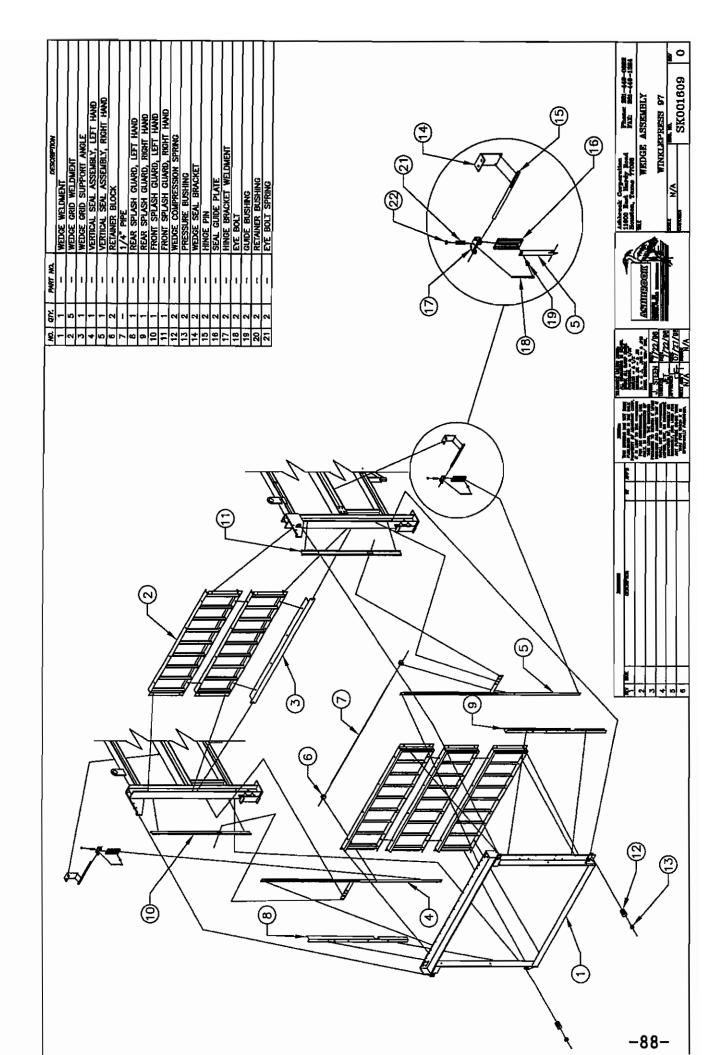
#### 10.13.5 Wedge Plate Adjustment: The opening of the wedge may

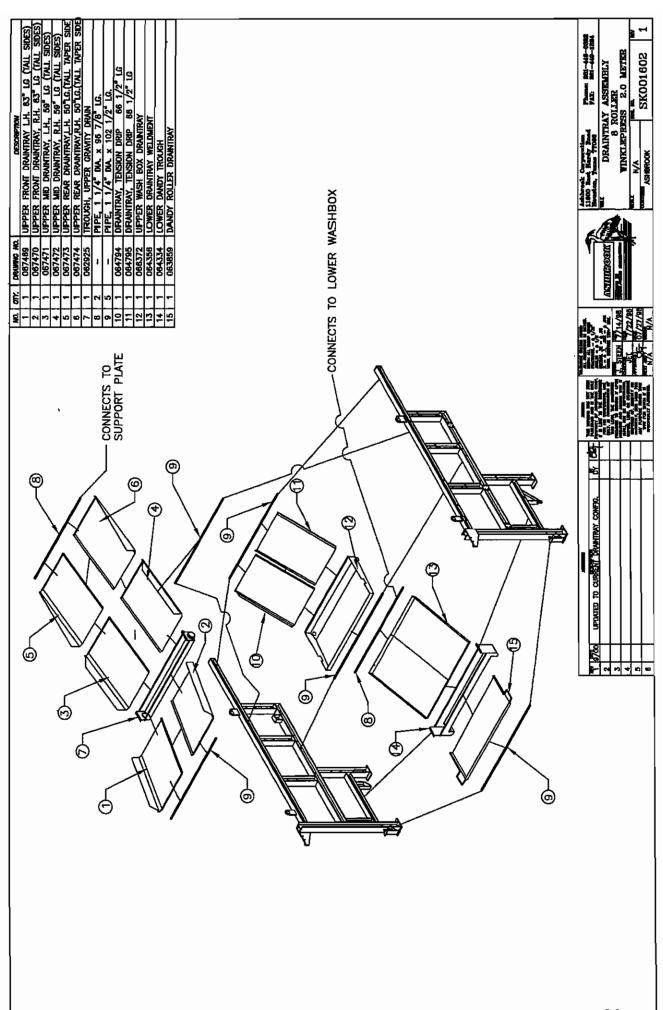
be adjusted at both the top (inlet) and at the bottom (outlet). Measure at both sides to be sure both sides are open the same amount. The top is usually open about twice as much as the bottom, but this will need to be adjusted according to the process requirements.

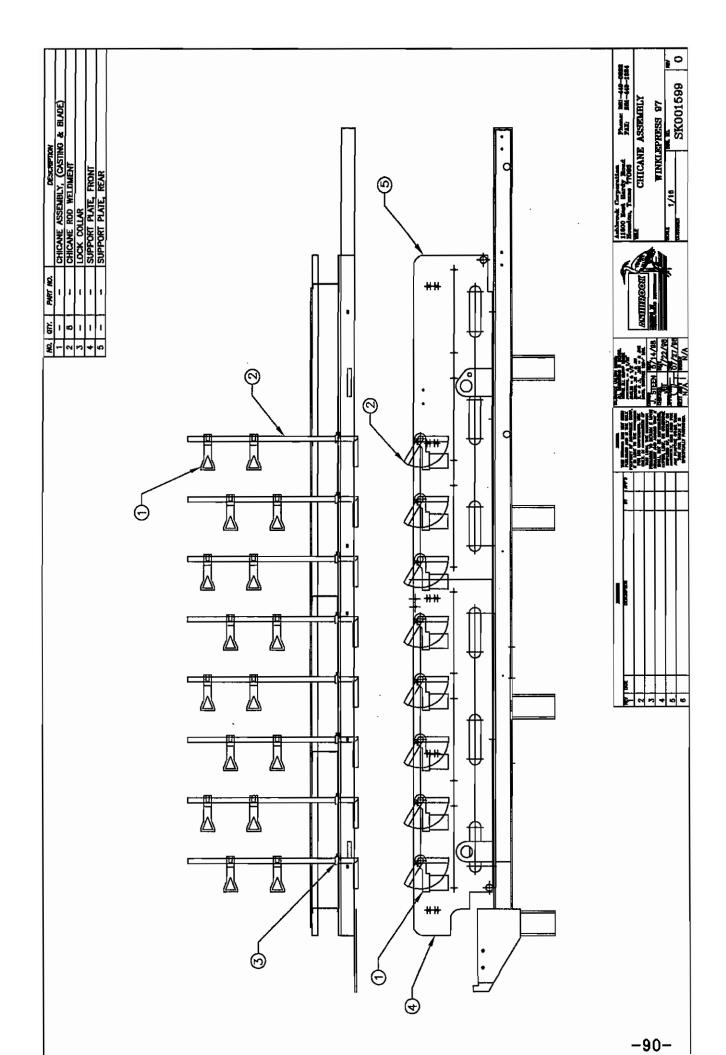
#### a. Upper (Inlet) adjustment:

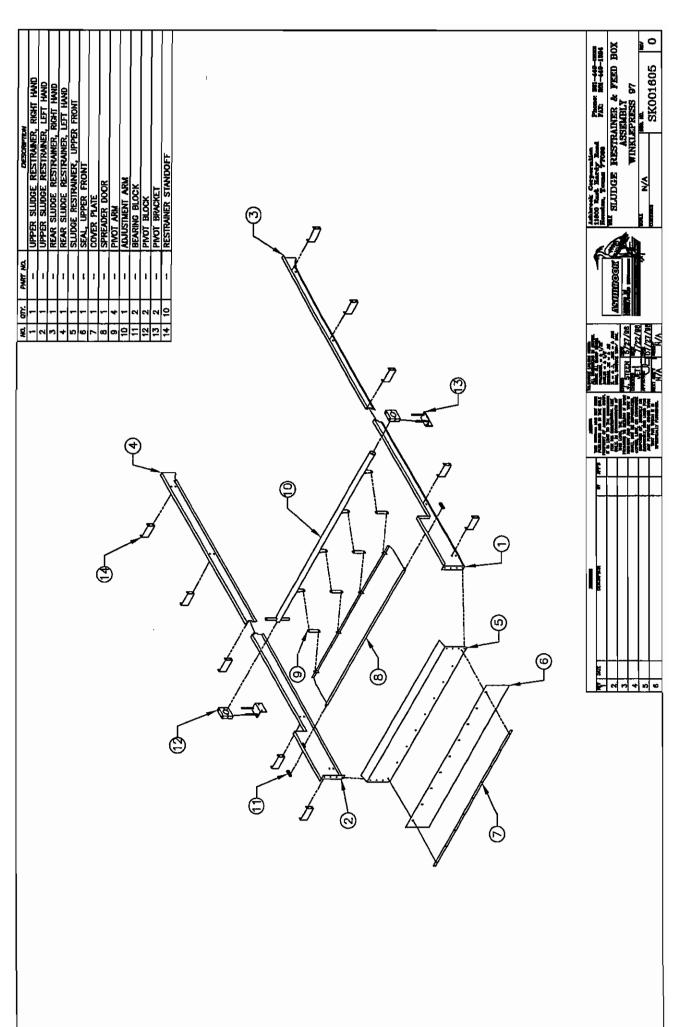
 Adjust the opening by turning the nuts on the jack screws. Located at the top of the wedge on either side of the frame.











- 2. Measure the gap between the grid bars to be sure the wedge is open the same amount on both sides.
- 3. Lock the nuts in place to prevent movement during operation.

#### b. Lower (Outlet) Adjustment:

- Adjust the opening by turning the nuts on the jack screws located at the bottom of the wedge on either side of the frame.
- 2. Measure the gap between the grid bars to be sure the wedge is open the same amount on both sides.
- 3. Lock the nuts in place to prevent movement during operation.
- 4. Do not over tighten the nut. The spring is for a builtin safety feature to protect the machine from damage due to over pressure should an object or mass pass through the wedge.

#### 10.13.6 Chicane Adjustment:

#### a. Horizontal Adjustment:

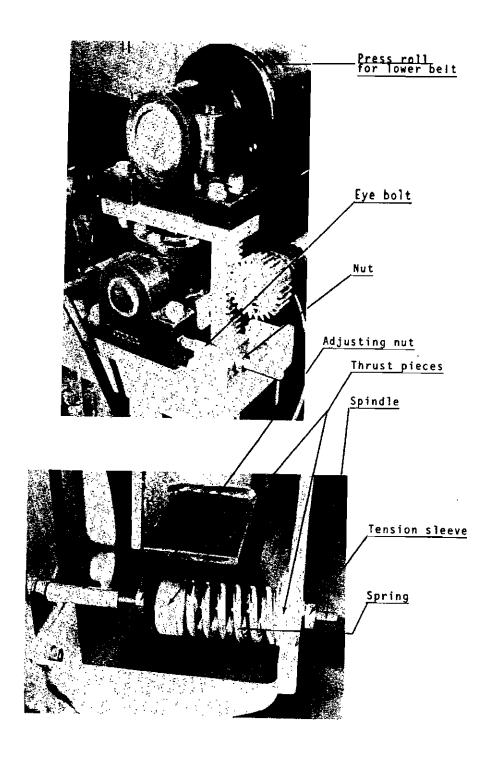
- (1) Loosen bolt.
- (2) Slide chicane to desired position.
- (3) Tighten bolt.

#### b. Vertical Adjustment:

- (1) Loosen bolt.
- (2) Rotate retaining ring until chicane is resting on belt.
- (3) Tighten bolt.

#### 10.13.7 Chicane Replacement:

- Stop belt press and lock out controls.
- b. Rotate chicanes off belt.
- c. Knock out roll pin.
- d. Remove old blade.
- e. Insert new blade.
- f. Install roll pin.
- g. Rotate chicanes onto belt.
- h. Resume operations



#### 10.13.7 Chicane Replacement:

- a. Stop belt press and lock out controls.
- b. Rotate chicanes off belt.
- c. Knock out roll pin.
- d. Remove old blade.
- e. Insert new blade.
- f. Install roll pin.
- g. Rotate chicanes onto belt.
- h. Resume operations

#### 10.14 WASH STATION:

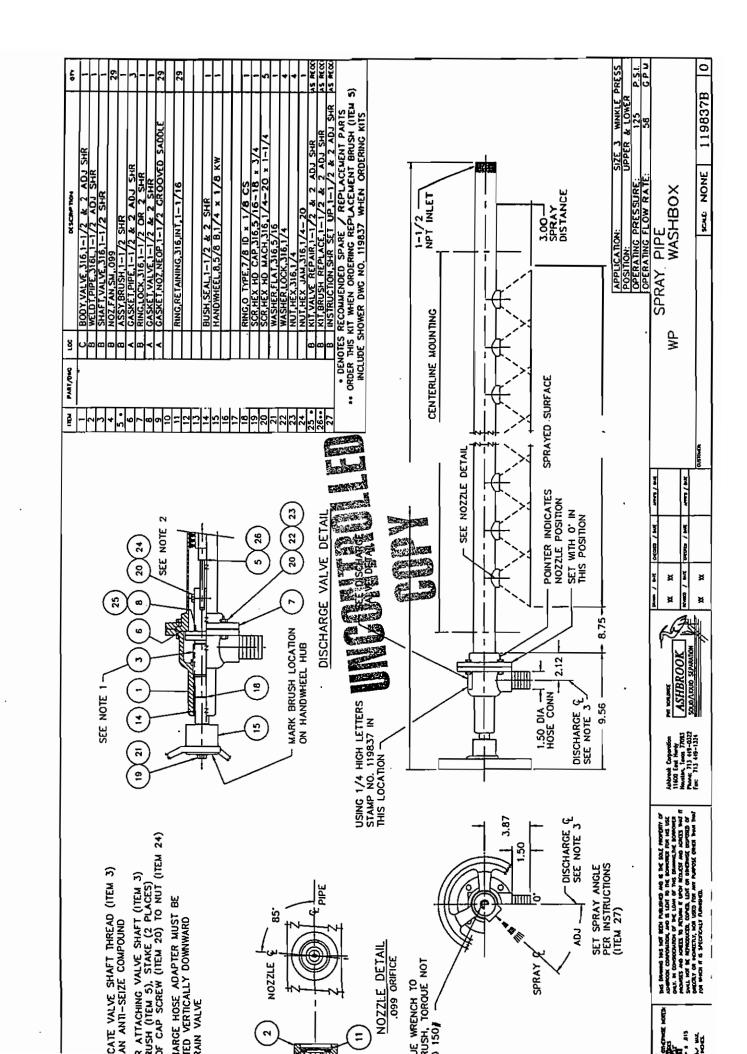
#### 10.14.1 Drawings:

- A. Lower Belt Wash Box Assembly
- B. Upper Belt Wash Box Assembly
- C. Wash Tube Cut Sheets
- D. Nozzle Replacement Instructions
- E. Nozzle Information

#### 10.14.2 Seal Replacement Instructions:

- A. Shut down belt press and detension belts
- B. Lock out control panel
- C. Loosen wash box bracket bolts and position wash box so that seals are accessible
- D. Remove old seals and discard
- E. Press new seals onto wash box edge. Cut seal so that the edge of seal flares out from the box edge at a 45 degree angle to the belt. This flare helps reduce the over-spray
- F. Reposition wash box and tighten bolts

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OVE FOUR (4) 1/4 SCREWS (ITEM E) AND
L VALVE SHAFT (ITEM C) AND BRUSH (ITEM D)
OF PIPE WELDMENT (ITEM F) FAR ENOUGH TO
OVE SCREW (ITEM 4) AND NUT (ITEM 5) THAT
INECT VALVE SHAFT TO BRUSH.

ARATE VALVE SHAFT FROM BRUSH. SCREW NUT ARE STAKED TOGETHER AND MAY HAVE BE SEPARATED BY GRINDING.

OVE WORM PIPE GASKET (ITEM 1) MATERIAL, M END OF PIPE WELDMENT AND VALVE BODY.

# STALL NEW BRUSH

E NEW BRUSH (ITEM 2) INTO PIPE WELDMENT M F), LEAVING ENOUGH EXPOSED TO ATTACH VE SHAFT.

THREE (3) NEW PIPE CASKETS (ITEM 1) VALVE BODY RECESS (ITEM B).

REATTACH VALVE SHAFT TO BRUSH WITH A NEW SCREW (ITEM 4) AND NUT (ITEM 5). THE NUT MUST NOT BE MORE THAN FINGER TIGHT, STAKE (2 PLACES) END OF SCREW TO NUT. Ġ.

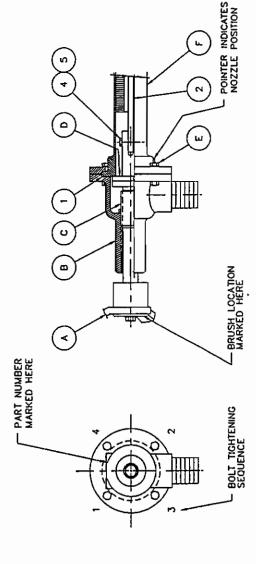
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LUBRICATE VALVE SHAFT THREAD (ITEM C) WITH AN ANTI-SEIZE COMPOUND.

۲.

- PUSH VALVE BODY, VALVE SHAFT AND BRUSH INTO THE PIPE WELDMENT. MAKE SURE VALVE BODY (ITEM B) CONTACTS PIPE WELDMENT BEFORE VALVE GASKET (ITEM D) TO ENSURE PROPER SEAL. œ,
- ROTATE HOSE CONNECTION ON VALVE BODY TO THE O' POSITION. တ်
- 10. ALIGN SCREW HOLES.
- INSTALL SCREWS AND TIGHTEN TO LOCK THE VALVE ASSY AND PIPE TOGETHER.
- 12. USE A MAX. OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN.

- GASKET,VALVE,FIBRE,1-1/2 & 2 SHR ASSY,BRUSH,1-1/2 & 2 SHR (SEE ASSY DWG) SCR,MACH,HEX HD,316,1/4-20 x 1-1/4
  NUT,HEX JAM,316,1/4-20
  COPY OF THIS DWG ള 104481 104484 PART/DWG
- 13. CLOSE VALVE COMPLETELY
- CHECK BRUSH LOCATION TO MAKE SURE BRUSH DOES NOT INTERFERE WITH NOZZLE DISCHARGE. 4.
- IF BRUSH INTERFERES WITH NOZZLES, REMOVE FOUR (4) SCREWS (ITEM E) AND PULL THE VALVE BODY (ITEM B) AWAY FROM THE PIPE. <u>5</u>
- REMOVE BY TEARING IN HALF AND TAKING OUT ONE PIPE GASKET WILL ROTATE THE THE BRUSH APPROXIMATELY 45". 9
- SLIDE VALVE BODY TOWARD PIPE AND ALIGN SCREW HOLES. INSTALL SCREWS AND TIGHTEN TO LOCK THE VALVE ASSY AND PIPE TOGETHER. 7.
- 18, USE A MAX, OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN.



SPRAY PIPE BRUSH REMOVAL WP WASHBOX

THE DOWNER HAS NOT BEEN PARADRED AND IS THE SOLL PROPERTY OF
AMERICAL CORPORATION, AND IS LIDAT TO THE BURNOWER FOR HIS USE
DACK. BY COMSOCIANTIN OF THE LOW OF THIS DEMANG, THE BORNOWER
PROMESTS AND ACREES TO RETURN IT UPON REQUEST AND ACREES THAT IT
SHALL HOT BK REPRODUCTS, COPPES, LEAT OR EMETHRIC DISPOSED OF
DARCTLY OR SCHOOLIN, NOR USED FOR ANY PURPOSE OTHER THAN THAT
FOR WHICH IT IS SPECIFICALLY PURPLESS.

Ashbrook Corporation 11600 East Newy Houston, Team 77093 Phone: 713 449-0322 Fee: 713 449-1324	Voros
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-	119745	¥	GASKET, PIPE, FIBRE, 1-1/2 & 2 ADJ SHR	-
2				
3	102397	<	GASKET, VALVE, UHPE, 1-1/2 & 2 SHR	-
4	104481		SCR,MACH,HEX HD,316,1/4-20 x 1-1/4	-
5	104484		NUT,HEX JAM, 316,1/4-20	-
9			COPY OF THIS DWC	-

# REATTACH VALVE SHAFT TO BRUSH WITH A NEW SCREW (ITEM 4) AND NUT (ITEM 5). THE NUT MUST NOT BE MORE THAN FINGER TIGHT, STAKE (2 PLACES) END OF SCREW TO NUT. ۲. JOVE FOUR (4) 1/4 SCREWS (TEM D) AND L VALVE SHAFT (ITEM C) AND BRUSH (ITEM E) T OF PIPE WELDMENT (ITEM F) FAR ENOUGH TO JOVE SCREW (ITEM 4) AND NUT (ITEM 5) THAT NNECT VALVE SHAFT TO BRUSH.

EMOVE VALVE GASKET

LUBRICATE VALVE SHAFT THREAD (ITEM C) WITH AN ANTI-SEIZE COMPOUND.

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PARATE VALVE SHAFT FROM BRUSH. SCREW O NUT ARE STAKED TOGETHER AND MAY HAVE BE SEPARATED BY GRINOING.

- PUSH VALVE BODY, VALVE SHAFT AND BRUSH INTO THE PIPE WELDMENT. MAKE SURE VALVE BODY (ITEM B) CONTACTS PIPE WELDMENT BEFORE VALVE GASKET (ITEM 3) TO ENSURE PROPER SEAL. 6
- ROTATE HOSE CONNECTION ON VALVE BODY TO THE O' POSITION.

MOVE WORM PIPE GASKET (ITEM 1) MATERIAL OM END OF PIPE WELDMENT AND VALVE BODY.

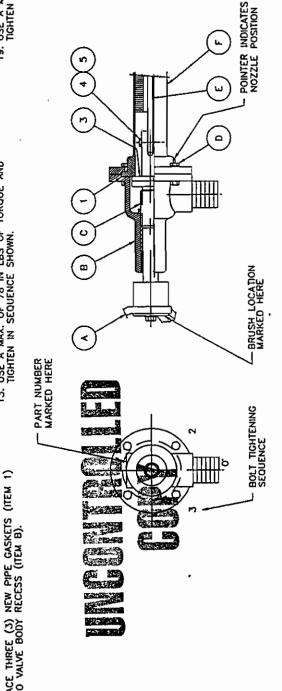
MOVE VALVE GASKET (ITEM 3).

DE NEW VALVE GASKET (ITEM 3) ONTO VALVE AFT (ITEM C) UNTIL IT IS AGAINST FLANGE.

ASTALL NEW VALVE GASKET

- 11. ALIGN SCREW HOLES.
- INSTALL SCREWS AND TIGHTEN TO LOCK THE VALVE ASSY AND PIPE TOGETHER.
- 13. USE A MAX, OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN.

- 14. CLOSE VALVE COMPLETELY
- CHECK BRUSH LOCATION TO MAKE SURE BRUSH DOES NOT INTERFERE WITH NOZZLE DISCHARGE. 5
- IF BRUSH INTERFERES WITH NOZZLES, REMOVE FOUR (4) SCREWS (ITEM D) AND PULL THE VALVE BODY (ITEM B) AWAY FROM THE PIPE. 16.
- REMOVE BY TEARING IN HALF AND TAKING OUT PIPE GASKET. ONE PIPE GASKET WILL ROTATE THE BRUSH APPROXIMATELY 45. 17.
- SLIDE VALVE BODY TOWARD PIPE AND ALIGN SCREW HOLES. INSTALL SCREWS AND TIGHTEN TO LOCK THE VALVE ASSY AND PIPE TOGETHER. <u>α</u>
- USE A MAX. OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN. <u>6</u>



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VALVE GASKET REMOVAL WP WASHBOX

304 / BM CED / SMI

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119843B SOUTH NONE

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8 PART/DWG Ē

L CALL

# TO SET SPRAY ANGLE

- 1. THE SHOWER IS ASSEMBLED WITH THE SPRAY ANGLE AND DISCHARGE HOSE ADPT. SET AT O'.
- TO CHANGE THE SPRAY ANGLE, LOOSEN FOUR (4) 1/4 SCREWS (ITEM D) ENOUGH TO ROTATE THE PIPE. USE THE LOCK RING (ITEM C) AS A DEGREE INDICATOR.
- SET THE SPRAY ANGLE TO THE DESIRED DEGREE 'n
- TICHTEN SCREWS TO LOCK THE VALVE ASSY AND PIPE TOGETHER.
- USE A MAX. OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN. 'n.

# TO CHECK FOR BRUSH LOCATION

- CLOSE VALVE COMPLETELY ě.
- CHECK BRUSH LOCATION TO MAKE SURE BRUSH DOES NOT INTERFERE WITH NOZZLE DISCHARGE. ۲.
- IF BRUSH INTERFERES WITH NOZZLES, REMOVE FOUR (4) SCREWS (ITEM D) AND PULL THE VALVE BODY (ITEM B) AWAY FROM THE PIPE. ထ
- REMOVE BY TEARING IN HALF AND TAKING OUT ONE PIPE GASKET(ITEM #1). 6
- SLIDE VALVE BODY TOWARD PIPE AND ALIGN SCREW HOLES. INSTALL SCREWS AND TIGHTEN TO LOCK THE VALVE ASSY AND PIPE TOGETHER. ġ

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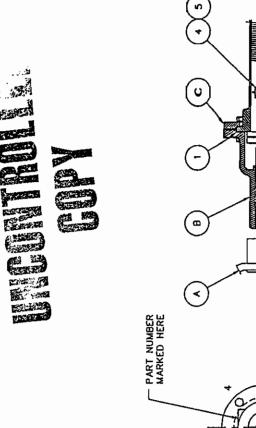
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POINTER

BRUSH LOCATION MARKED HERE

BOLT TICHTENING SEQUENCE

11. USE A MAX. OF 78 IN LBS OF TORQUE AND TIGHTEN IN SEQUENCE SHOWN.





ASHBROOK
solo/koug separation

Abbrook Corportion 11600 East Hordy Houston, Texas 77093 Phone: 713 419—0322 Fee: 713 419—1324

SPRAY ANGLE SETTING WP WASHBOX

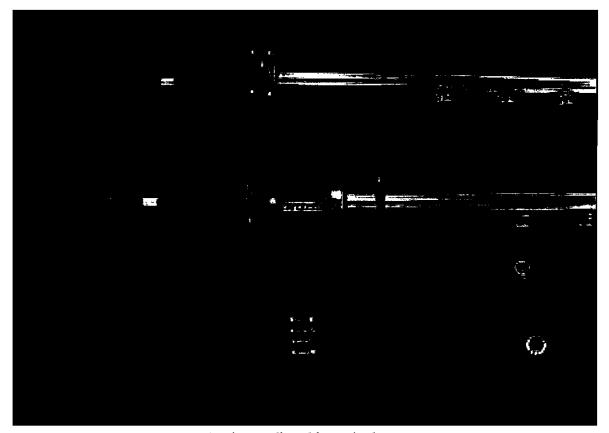
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SCALE NONE

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# ADJUSTABLE ANGLE SHOWER INSTRUCTIONS FOR 1-1/2" AND 2"

The Appleton Adjustable Angle Shower provides variable spray angle and brush position. This manual includes the information necessary to service the 1-1/2" and 2" showers.



Appleton adjustable angle shower



Disconnect the water source to the shower before disassembly. High pressure water can cause personal injury.

The following procedure will ensure that the shower is safe to disassemble:

- 1- Turn off and lock out the pump that supplies the shower.
- 2- Turn off and lock out the oscillator (if present).
- 3- Open the shower valve to discharge any water that may be present in the shower.

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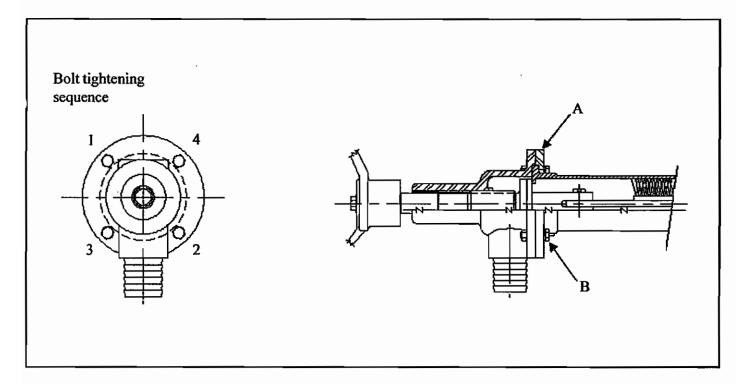
#### **SECTION 1: SETTING SPRAY ANGLE**

- 1- The shower is assembled with the spray angle and discharge hose adapter set at 0 degrees.
- 2- The spray angle can be changed by loosening four 1/4" screws (B), permitting pipe rotation. The lock ring (A) is marked in degrees to aid in determining the shower angle. The hose connection on the valve body should be oriented vertically downward to drain the valve.
- 3- When the proper angle is reached, tighten the four screws (B) to lock the valve assembly in the new position. See the drawing below for the tightening pattern.



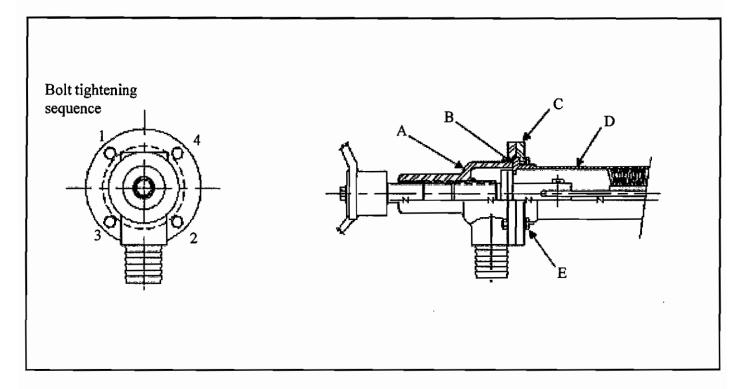
Do not apply a torsion force in excess of 78 in-lbs to the four screws (D). Excessive force will break the screws.

4- Check the location of the brush to ensure that it is not blocking the spray nozzles. If the nozzles are blocked adjust the brush position using the procedure outlined in section 2.



#### **SECTION 2: SETTING BRUSH LOCATION**

- 1- Close the valve completely.
- 2- Check the brush location to make sure that the brush does not interfere with nozzle discharge.





#### Disconnect the water source to the shower before disassembly. High pressure water can cause personal injury.

- 3- If the brush blocks the nozzles, loosen the four screws (E) and pull the valve body (A) away from the pipe (D) providing access to the valve gaskets (B).
- 4- Remove a gasket (B) by tearing it in half and pulling it out of the gap, or add a gasket. Each gasket will rotate the brush about 45 degrees.
- 5- Re-assemble the valve by aligning the pipe pointer with the desired angle mark on the lock ring (C) and tightening the four screws (E). Tighten the screws as shown on bolt sequence above.



Do not apply a torsion force in excess of 78 in-lbs to the four screws (D). Excessive force will break the screws.

#### SECTION 3: INSTALLING NEW VALVE GASKET

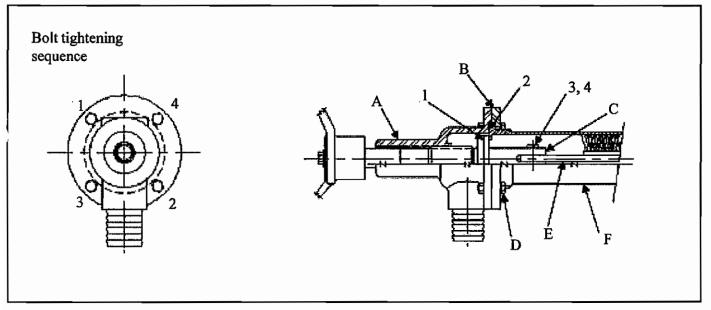


Disconnect the water source to the shower before disassembly. High pressure water can cause personal injury.

#### 3.1. Service Parts Required

Valve repair kit 119843 includes:

Item	Part No.	Descriptio	Req'd
1	119745	Gasket, Pipe, Fibre, 1-1/2 & 2 Adj Shr	3
2	102397	Gasket, Valve, UHPE, 1-1/2 & 2 Shr	1
3	104481	Scr, Mach, Hex, HD, 316, 1/4-20 x 1-1/4	1
4	104484	Nut, Hex Jam, 316, 1/4-20	1

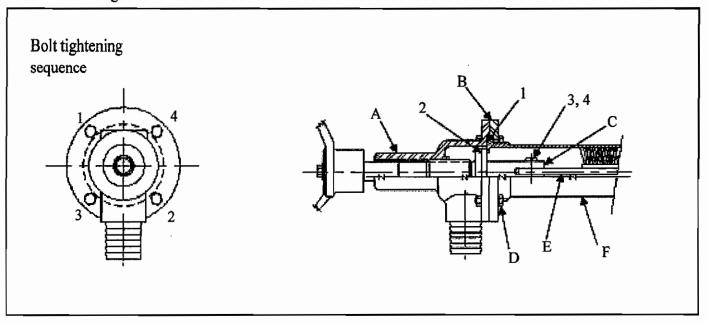


#### 3.2 Disassemble the Shower

- 3.2.1.Remove four screws (D) and pull the Valve Bonnet (A) away from the Pipe (F) and Lock Ring (B) until the Screw (3) that connects the Valve Shaft (C) to the Brush (E) is accessible.
- 3.2.2. Remove the Nut (3) from the Screw (4), disconnecting the Valve Shaft and Brush. The nut and screw are staked and may have to be separated by grinding. The Valve Bonnet is now detached from the Pipe.
- 3.2.3. Remove the old valve gasket (2) by sliding it off the valve shaft.
- 3.2.4. Remove the old pipe gasket (1) from the end of the pipe (F) and valve body (A). Take care not to scratch the cast gasket seats on the pipe weldment and valve body.

#### 3.3. Assembly

3.3.1. Slide the new valve gasket(s) onto the valve shaft (C) until it is against the flange.



- 3.3.2. Place three new pipe gaskets (1) into valve body recess (A).
- 3.3.3. Attach valve shaft (C) to brush (E) with a new screw (3) and nut (4). The nut should not be tightened more than finger tight. Stake the nut and screw in two places.
- 3.3.4. Lubricate the valve shaft threads (C) with an anti-seize compound.
- 3.3.5. Push the valve body, valve shaft and brush into the pipe weldment. Make sure the valve body contacts pipe weldment before valve gasket (2) to ensure proper seal. If the valve gasket contact first, screw the valve shaft out until the valve body contacts the pipe weldment.
- 3.3.6. Rotate the hose connection on the valve body to the desired angle.
- 3.3.7. Align the holes for the four screws (D) and install the four screws.



Do not apply a torsion force in excess of 78 in-lbs to the four screws (D). Excessive force will break the screws.

- 3.2.8. Close the valve completely.
- 3.2.9. Check the brush location to ensure that the nozzles are not blocked. Adjust per instructions 2.0 above, setting brush location.

#### **SECTION 4: BRUSH MAINTENANCE**



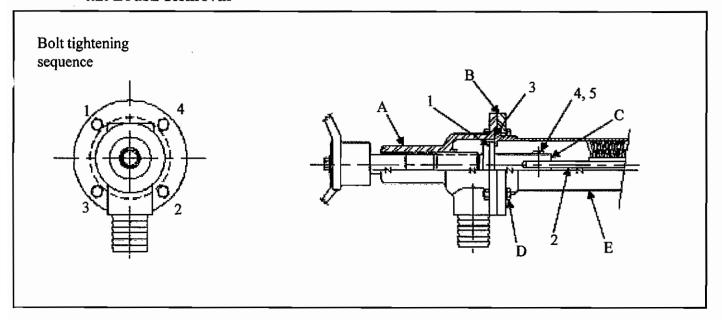
Disconnect the water source to the shower before disassembly. High pressure water can cause personal injury.

#### 4.1. Service Parts Required

Brush replacement kit 119840 includes:

Item	Part No.	Description	Req'd
1	119745	Gasket, Pipe, Fibre, 1-1/2 & 2 Adj Shr	3
2		Ass'y, Brush, 1-1/2 & 2 Adj Shr	Ref
3	102397	Gasket, Valve, UHPE, 1-1/2 & 2 Shr	Ref
4	104481	Scr, Mach, Hex, HD, 316, 1/4-20 x 1-1/4	1
5	104484	Nut, Hex Jam, 316, 1/4-20	1

#### 4.2. Brush Removal



- 4.2.1. Disassemble the shower per 3.1 above.
- 4.2.2. Slide the old brush out of the shower.

#### 4.3. Installation

- 4.3.1. Slide the new brush into the pipe weldment (E) leaving enough bush exposed to attach the valve shaft.
- 4.3.2. Place three new pipe gaskets (1) into valve body recess (A).
- 4.3.3. Attach valve shaft (C) to brush (2) with a new screw (4) and nut (5). The nut should not be tightened more than finger tight. Stake the nut and screw in two places.
- 4.3.4. Lubricate the valve shaft threads (C) with an anti-seize compound.
- 4.3.5. Push the valve body, valve shaft and brush into the pipe weldment. Make sure the valve body contacts pipe weldment before valve gasket (3) to ensure proper seal. If the valve gasket contact first, screw the valve shaft out until the valve body contacts the pipe weldment.
- 4.3.6. Rotate the hose connection on the valve body to the desired angle.
- 4.3.7. Align the holes for the four screws (D) and install the four screws. Tighten the screws a shown on the bolt tightening sequence.



# Do not apply a torsion force in excess of 78 in-lbs to the four screws (D). Excessive force will break the screws.

- 4.3.8. Close the valve completely.
- 4.3.9. Check the brush location to ensure that the nozzles are not blocked. If they are, adjust per instructions 2.0 above, setting the brush location.

#### 5.0 Nozzles - Ring Retained

- 5.1. Appleton belt press showers utilize a stainless steel ring to hold the nozzle assembly in place. This section contains instructions on removing and replacing these nozzles.
- 5.2. Tools required:
  - Soft Head Hammer
  - 1-1/16" Punch (Appleton PN 105448)
  - 1/8" Punch
  - Tapered Collar (Appleton PN 105449)
  - · Small Needle Nose Pliers
  - Small Awl

#### 5.3. Nozzle Removal



Wear safety glasses while assemblying or disassembling nozzles. Metal chips or flying retaining rings could result in eye injury.

- 5.3.1. Use an awl or pointed tool to pry one end of the retaining ring out of the slot.
- 5.3.2. Grip the retaining ring with a needle nose pliers and pull the ring out with a twisting motion.
- 5.3.3. Remove the nozzle and itsgasket.

#### 5.4. Nozzle Replacement

- 5.4.1. Clean the nozzle seat and the groove for retaining the ring.
- 5.4.2. Lay one nozzle gasket into the nozzle seat (ref. figure 1).
- 5.4.3. Place one nozzle on the gasket with the fan opening at 85 degrees to the pipe centerline (ref. figure 2). The nozzle should be placed so it protrudes into the pipe.
- 5.4.4. Set the tapered collar tool on the nozzle saddle with the recessed end over the saddle. (ref. figure 3).
- 5.4.5. Insert one retaining ring into the top of the tapered collar tool (ref. figure 4).
- 5.4.6. Drive the retaining ring into the recessed groove with the 1-1/16 diameter punch (ref. figure 4).
- 5.4.7. Remove the collar tool and seat the ring with the 1/8" diameter punch (ref. figure 5).

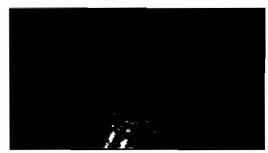


Fig. 1, place the gasket



Fig. 2, place the nozzle



Fig. 3, place tapered collar



Fig. 4, drive ring in place

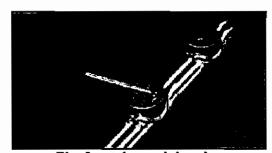


Fig. 5, set the retaining ring

#### 6.0 Nozzles - Nut Retained

Paper machine showers utilize a retaining ring and a nut to hold the nozzle in place. These nozzles can be serviced as follows.



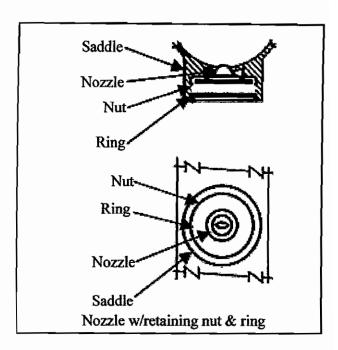
Wear safety glasses while assemblying or disassembling nozzles. Metal chips or flying retaining rings could result in eye injury.

#### 6.1. Nozzle Removal

- 6.1.1. Remove the retaining ring from the nozzle saddle.
- 6.1.2. Thread the retaining nut out of the nozzle saddle.
- 6.1.3. Remove the nozzle.
- 6.1.4. Remove the gasket taking care not to scratch the seat in the nozzle saddle.

#### 6.2. Nozzle Replacement

- 6.2.1. Clean the nozzle seat, threads, and retaining slot.
- 6.2.2. Lay one nozzle gasket into the nozzle saddle.
- 6.2.3. Lay one nozzle on the gasket with the fan openning 85 degrees to the centerline of the shower pipe (ref. figure 6). The nozzle should be placed so that it protrudes into the pipe.
- 6.2.4. Thread the retaining nut into the saddle taking care not to rotate the nozzle.
- 6.2.5. Install the retaining ring.



#### 7.0. Ordering

- 7.1. The parts shown in the instructions above, or any other shower parts you require, can be ordered from Appleton Mfg Division as easily as calling 1-800-531-2002 or (920) 751-1555.
- 7.2. Ask for the Customer Service Representative covering your area.
- 7.3. Give the representative the part number, description and quantity of the parts you need. . . with your order number.
- 7.4. We'll get your parts packaged and shipped... usually within 24 hours.



#### WASHWATER SPRAY TUBE DATA DESCRIPTION

# The press is equipped with a belt cleaning shower which can be cleaned during normal press operation.

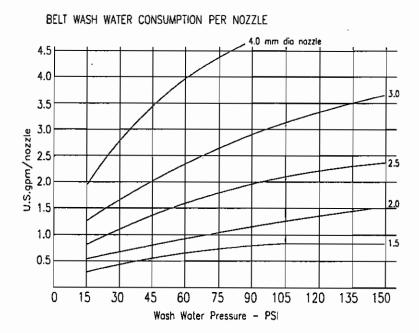
Cleaning of the flat spray nozzles is achieved by turning the handwheel one full term in a counter clockwise direction.

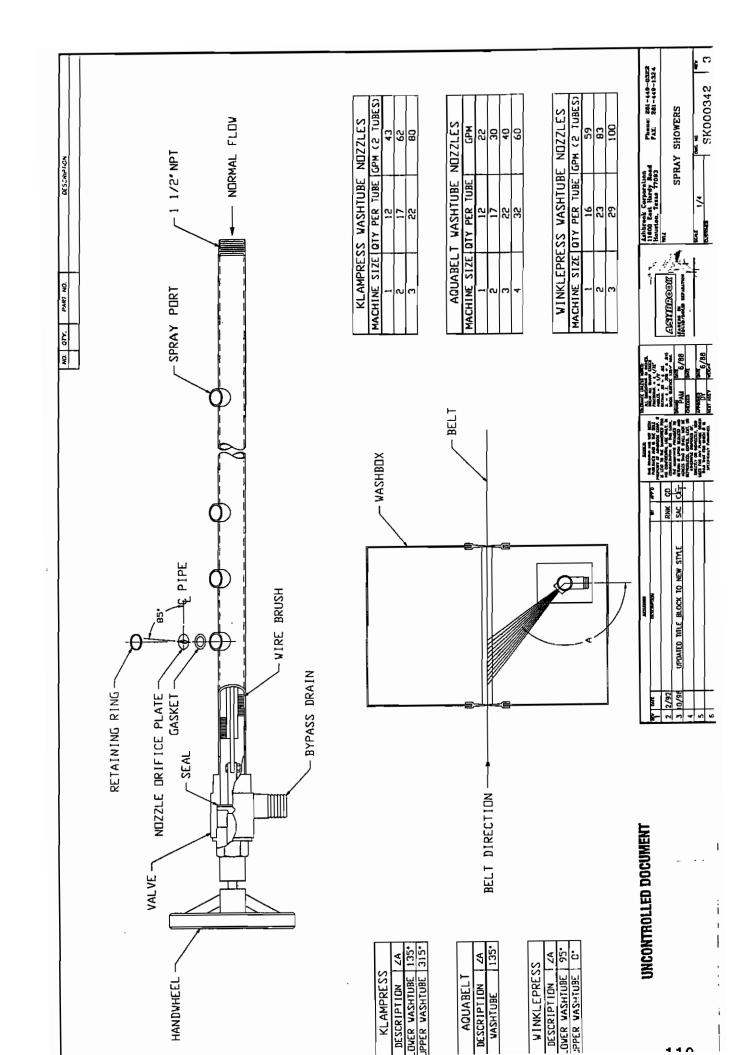
This action opens the drain valve and the bristles in the brush dislodge any contaminants from the nozzles. The wash water flushes the contaminants out to the sump through the drain valve.

Turning the hand wheel in a clockwise direction closes the discharge valve and returns the press to normal operation.

#### Some of the advantages of this system include:

- 1. You may use fresh or re-cycled water.
- 2. The water consumption is low.
- 3. Nozzle cleaning and dirt removal occurs during press operation.
- 4. Nozzle size may be changed for various applications.
- 5. No additional space is required on either side of machine to operate the internal cleaning brush.
- 6. Complete spray tube is made of corrosion resistant stainless steel.
- 7. You get uniform drainage through the filter belts due to the thorough cleaning which eliminates blinded areas across the belt.





#### 10.14 SCRAPERS

#### 10.14.1 Scraper Assembly

#### 10.14.2. Scraper Blade Replacement:

- a. Shut down the press and lock out drive controls.
- b. Rotate the blade away from the belt.
- c. Remove the cover plate. Save the plate and bolts.
- d. Remove and replace the scraper blade with new blade.
- e. Replace the cover plate and bolts.
- f. Resume operations.

#### 10.16 **DRIVE TRAIN**:

10.161\_

- a. Drive unit Technical Data
- b. Motor Data
- c. Electrical Motor Data
- d. Electrical Motor Dimensional Data
- e. Manufacturer's Instructional Data

#### 10.16.2 Lubrication:

Note: Lubrication frequency - Primary Gear Box 10,000 hours.

#### a. Primary Gear Box:

- (1) Check oil level every 6 months.
- (2) Replace oil every 10,000 hours or annually.
- (3) Should oil be observed leaking from the gear reducer the seals must be replaced immediately to prevent serious damage to the gearing.

WP84-10 Rev. 2

## ASHBROOK SIMON-HARTLEY

Belt Press Drive Data

# Technical Data for Winklepress <u>Drive Unit</u> 2.0 Meter with a VFD

#### **Motor Data:**

Manufacturer: Eurodrive

Nameplate Horsepower: 3.0

Frame Size: DT100L4

Power Requirement: 240/480 Volt Three Phase, 60 Hertz

Full Load Speed: 1700 Nema Design: B

Ambient Temp: 40 Degrees C

Insulation Class: F

Full Load Torque: 110lbs-in Service Factor: 1.15

Time Rating: Continuous Enclosure: TEFC

#### Gear Reducer:

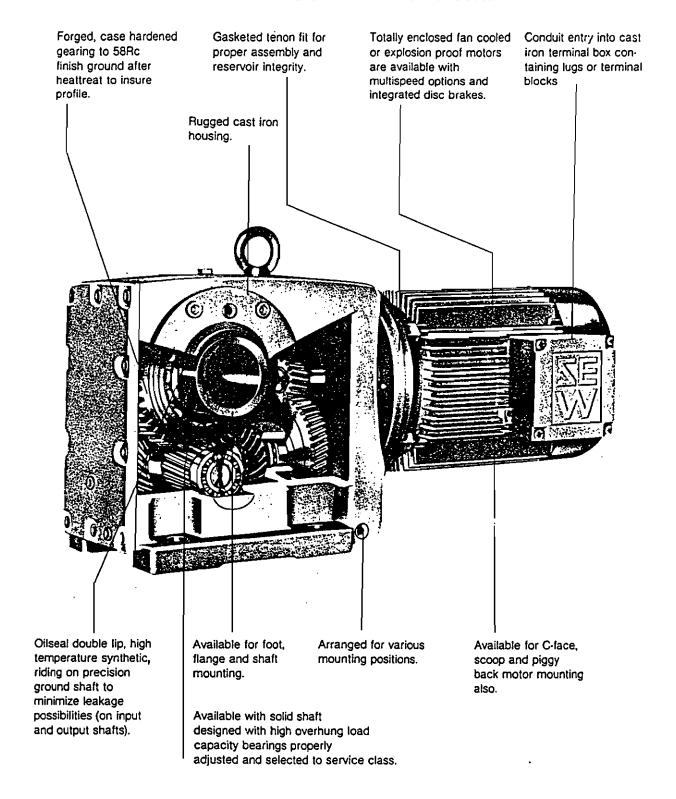
#### **Special Features:**

Manufacturer: Eurodrive [X] Severe Duty Protection
Model: FA97 [ ] Motor Thermostats
Reduction Ratio: 276.67:1 [ ] Motor Theristors
Output Speed: 6.1 RPM

Type of Gearing: Helical
Lubrication: Oil Splash
Mounting: H1 Position

Service Factor: 1.2 Shaft Size: 70mm

## **Helical-Bevel Construction Features**

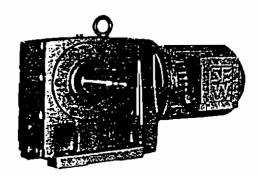




#### Helical - Bevel Gearmotors

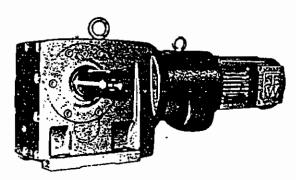
EURODRIVE'S range of helical-bevel gearmotors and reducers has many advantages over conventional right angle (worm) and combination (helical-worm) designs, the most important is their efficiency (95% over the range of ratios) and their ability to backdrive (overhauling loads) without the problem of self locking worms. In addition the compactness of the helical-bevel reducers lower structural costs at installation point.

Standard helical-bevel gearmotors are available in the horse power range from 0.75 to 350 hp.



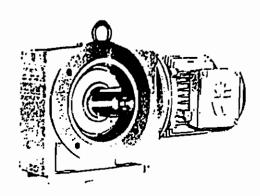
TYPE K.. DT..

A selection of output speeds is available from approximately 10:1 to 160:1. These helical-bevel reducers may be joined to a preceding parallel (helical) unit to provide extremely large ratios up to 16,000:1.

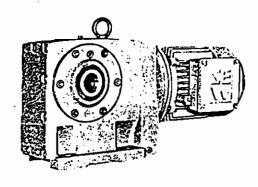


TYPE K.. R.. DT..

The helical-bevel can be arranged for flange and shaft mounting as well as the more common foot mount.



TYPE KF., DT.,



TYPE KA.. DT..



## Helical - Bevel Gearmotors \*

1 hp = 0,746 kW 1 lb. in = 0,113 Nm



Output 3.0 HP 2.2 kW

Output	Gear	Torque		Overhung		Service		Esama Cl-s	Weight	Dimensi
n <sub>a</sub>	Ratio	Ma	Ma	Fa	F <sub>Q</sub>	factor	ŀ	Frame Size	lb.	Sheet
ıрm	_:1	lb in	Nm	ib	N	S.F.				Page
144	11.81	1310	148	1200	5340	3.05	K 66	DT100LS4	106	K-38
121	14.05	1560	174	1240	5530	2.55	KF66	DT100LS4	117	K-52, K-
103	16.58	1830	205	1280	5710	2.20	KA66	DT100LS4	104	K-87, K-
89	19.02	2120	235	1320	5860	1.90	10.00	51100201	''	
79	21.53	2390	265	1340	5960	1.65				
70	24.45	2700	300	1360	6060	1.45				
81	28.03	3100	345	1380	6160	1.30				
54	31.20	3500	390	1640	7320	2.30	K 78	DT100LS4	143	K-38
48	35.51	3940	440	1670	7410	2.00	KF76	DT100LS4	154	K-52, K-
41	41.45	4610	510	1690	7510	1.75	KA76	DT100LS4	143	K-87, K
34	50.55	5560	620	1700	7550	1.45				ŀ
30	57.57	6300	700	1690	7540	1.25				•
26	66.59	7270	810	1680	7470	1.10				
26	65.90	7270	810	4720	21000	2.20	K 88	DT100LS4	212	K-39
23	74.26	8220	910	4720	21000	1.95	KF86	DT100LS4	229	K-53, K-
20	85.65	9450	1050	4720	21000	1.70	KA88	DT100LS4	209	K-68, K-
18	96.37	10500	1170	4720	21000	1.50				
16	107.31	11800	1310	4720	21000	1.35				
14	120.19	13500	1500	4720	21000	1.20				
13	135.96	14500	1620	4720	21000	1.10			+	
17	98.00	11100	1240	6070	27000	2.40	K 96	DT100LS4 DT100LS4	357 408	K-40 K-54, K-
15	111.63	12600	1400	6070	27000	2.10	KF96	DT100LS4	346	K-69, K-
14 11	125.01 153.78	13500 17200	1500 1910	6070 6070	27000 27000	1.95 1.55	KA96	D1100034	3.00	1,00,10
10	111.63	18900	2100	6070	27000	1.40	K 96	DT112M8	388	1
9.0	125.01	21000	2330	6070	27000	1.25	KF96	DT112M6	439	
7.5	153.78	25200	2800	6070	27000	1.05	KA96	DT112M6	377	
8.0	230	23600	2630	10600	47000	1.85	K 106R70	DT100L4	655	K-45
6.0	281	31500	3500	10600	47000	1.40	KF106R70	DT100L4	712	K-57, K-
5.0	350	37800	4200	10600	47000	1.40	KA106R70	DT100L4	602	K-74, K-
4.0	<del>4</del> 44	47300	5250	10600	47000°	1.10				
4.0	424	47300	5250	15400	68500	1.50	K 126R70	DT100L4	1016	K-46
3.0	535	63000	7000	15400	68500	1.10	KF126R70	DT100L4	1122	K-58
							KA126R70	DT100L4	955	K-75
5.0	356	37800	4200	15400	68500	2.35	K 126R80	DT100L4	1102	K-47
4.0	460	47300	5250	15400	68500	1.85	KF126R80	DT100L4	1208	K-59
3.0	563	63000	7000	15400	68500	1.40	KA126R80	DT100L4	1041	K-76
2.5	689	75600	8400	15400	68500	1.15				
2.5	699	75600	8400	20200	90000	1.85	K 156R92	DT100L4	1585	K-48
2.0	858	94500	10500	20200	90000	1.50	KF156R92	DT100L4	1695	K-60
1.5	1102	126000	14000	20200	90000	1.10	KA156R92		1497	K-77
1.5	1130	126000	14000	27000	120000	1.75	K 166R92	DT100L4	2429	K-49
1.2 1.0	1387 1704	157500 189000	17500 21000	27000 27000	120000 120000	1.40 1.15	KH166R92	DT100L4	2350	†
							V 100000	DT100L4	3611	K-50
1.0	1702	189000	21000	33700	150000	1.85	K 186R92	DT100L4	3501	\ \^30
0.80	2273	236300	26300	33700	150000	1.50	KH186R92	DIIOCA	3301	ı '
0.60	2900	315000	35000	33700	150000	1.10				

† See factory for dimensions.

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<sup>\*</sup> See motor specification. \*\* Overhung load calculated at shaft mid point. The weights indicated in the above table are those of units without oil.

**DIMENSION SHEET** Helical-Bevel Gearmotors 34 003 09 US -QB-VO PD OA В Before ordering or specifying the above shown gearmotor, refer to mounting position pages K-34 - K-37 of this catalog for location of the conduit box or cable entry. If no mention is made on the order the unit will be shipped per B3 mtg., conduit box at 0°, cable entry at normal, output shaft at A-side. The above shows the conduit box at 180\*, output shaft at 8-side. Eyebolts can be removed Dimensions AB<sub>B</sub> and C<sub>B</sub> refer to brake motors
Eyebolts are supplied only on motor sizes DT132M and up -A8 For the second motor output shaft refer to the motor dimen When using a double output shaft the dimension WG = WJ Tolerance range for U ABA WG FRAME С AB AÉ<sub>8</sub> 8 BA CB D DB Ε EΑ L P PD QB ZG u SIZE н OA DT90S 6.73 6.73 26.69 30.04 9.76 DT90L 7.76 DT100LS 6.89 6.89 28.70 32.05 11.77 DT100L 9.45 1.50 3.94 5.59 29.53 33.27 DT112M 12.60 7.40 7.40 8.70 DT132\$ 31,30 35.04 32.13 37.17 0.19 1.10 9.45 11.46 14.37 12.99 1.42 6.73 11.81 10.87 9.57 2.875 5.51 DT132M 15.20 DT132ML 9.06 9.06 10.B3 34.49 39.53 17.56 DT160M 2.95 1.02 2.76 5.71 36.37 43.03 DT160L 19.44 DT180M 9.96 9.96 13.03 39.21 45.87 22.28 DT180L DT90\$ 171 171 678 763 248 DT90L 197 DT 100LS 175 175 729 814 299 DT100L 240 38 100 475 142 DT112M 750 845 320 188 188 221 795 890 DT132S 330 171 365 290 265 28 240 291 300 276 243 70 140 DT132M 816 944 386 DT132ML 230 230 275 876 1004 445 DT160M 75 26 70 413 145 924 DT160L 1093 494 253 DT180M 253 331 1165 996 566 DT180L DT100LS

= (SQ m6

DIN 332

.60 3.20

4.33 .750

15 74,5

110 20

.60 4.01

5.51.875

ΩМ

DT180M 9.96 9.96 42.16 48.82 22.05 DT180L DT200 11.22 11.22 43.94 50.75 23.82 DT225 15.51 11.38 11.38 47.1653.98 27.04 DT100LS 175 175 805 888 292 197 DT100L 827 920 DT112M 314 188 188 221 DT132S 872 965 110 359 557 270 42 168 15 95 DT132M 891 1019 380 DM 24 230 DT132ML 390 mm 230 340 212 315 50 280 347 275 350 321 291 90 170 951 1079 **44**0 DT160M DT160L 999 1168 33 90 488 95 494 170 140 25 **DT180M** 253 253 331 1071 1240 560 OT180L 285 285 1116 1289 605 687 DT200 DT225 289 289 1198 1371

12.40 | 1.97 | 11.02 | 13.66

TYPE-CERTIFIED FOR-FRAME -

6.89 6.89

7.40 7.40

9.06 9.06

15.35

DT100L DT112M

DT132\$

DT132M

DT132ML

DT160M

DT160L

K 106

31.69 34.96

32.56 36.22

34.33 37.99

35.08 40.12

37.44 42.48

39.3345.98 ·.039

13.35 8.35

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11.50

12.36

14.96

17.32

19.21 19.45

10.63 1.64 4.33 14 13 21.93

3.74 1.30 3.54

7.76

8.70

10.83

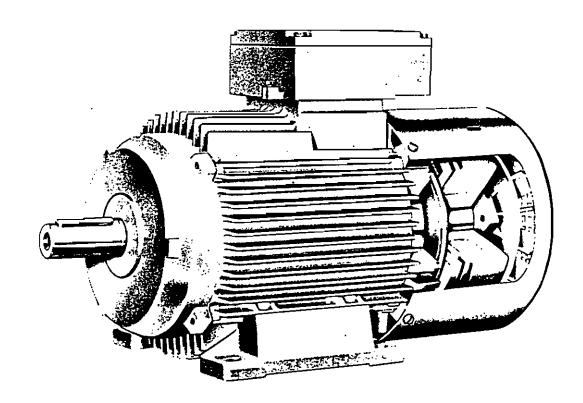
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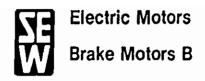
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6.69

11.46 3.625 6.69

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EURODRIVE'S standard motor voltages are 3 phase, 230/460 V, or 575V, 60HZ.

#### Motor Voltages

200V, 208, 60HZ and 220/380V, 50HZ, 415V, 50HZ are considered optional.

For other voltages and frequencies contact EURODRIVE.

#### **Brake Coll Voltages**

Motors with dual voltage connections: 230/460V, 60HZ will be supplied with a 230V brake coil. By connecting the brake rectifier to terminals T7 and T8 of the 9 terminal "block" the brake can operate with a 230V or a 460V power supply.

For Brake Motors Operating On: 200V/208V, 575V, 60HZ or 220/380V, 415V, 50HZ, the above does not apply. In all cases the brakes will be connected for the requested operating voltage.

#### **Motor Options**

- Severe Duty: Motors can operate in humid environments and washdown applications.
- Explosion proof motors: dual label; Class I, Group D, Class II, Group F and G.
- Class B F or H insulation.
- 1.15 service factor.
  - · Tropical protection.
  - · Thermistor or thermostat protection.
  - Heavy fan/flywheel.
  - · Motor back stop.
  - · Motor canopy.

#### **Motor Winding Connections**

Number of Poles	Synchronous speed RPM	Connection
2	3600	Y/YY
4	1800	Y/YY
6	1200	Y/YY
8	900	Y/YY
4/2	1800/3600	△/YY Single winding, constant torque
8/4	900/1800	△/YY Single winding, constant torque
6/2	1200/3600	Y/Y 2 separate windings, constant torque
8/2	900/3600	Y/Y 2 separate windings, constant torque
12/2	600/3600	Y/Y 2 separate windings, constant torque
6/4	1200/1800	Y/Y 2 separate windings, constant torque



## **Electric Motors and Brake Motors**

Synchronous Speed 1200 rpm, 60Hz
Continuous Duty, 40° C Ambient, up to 3300ft. elevation

**DATA SHEET**08 721 09 US

	Motor data .																			
FRAME SIZE		ninal Rating	Full load rpm	'	ull Los Current at 460 V Amp.						Tor	gue F.L. Break down	Power Factor	Elli- cien- cy % EFF	Code letter	Motor Inertia WK <sup>2</sup> Ib. It <sup>4</sup> with Brake	Max. Brake Torque	Max No. operations per hour (no load) Z <sub>Q</sub>	Wt. i	Motor with Brake
DT71C 6	.20	.15	1044	1.00	.50	.41	2.5	1.25	.41	12	140	140	0.8	50	F	0.0178	44	6800	15	24
DT71D 6	0.33	0.25	1100	1.56	0.78	0.62	4.2	2.1	1.68	19.6	180	180	0.8	50	F	0.0178	44	6800	15	24
DT80K 6	0.5	0,37	1100	2.3	1.15	0.92	5.8	2.9	2.3	29	170	180	0.77	54	E	ს.0266	87	4600	19,4	28.4
DT80N 6	0.75	0.55	1100	2.9	1.45	1.16	8.4	4.2	3.35	43	180	190	0.77	62	ε	0.0356	87	6000	22	31
DT90S 6	1	0.75	1100	4.05	2.0	1.60	13.8	6.9	5.5	57	220	230	0.7	67	F	0.0685	174	3200	<b>3</b> 3	54.2
DT90L 6	1,5	1.1	1120	5.8	2.9	2.3	22	11	8.8	83	240	250	0.69	69	G	0.090	174	2800	36	57
DT100L 6	2	1.5	1120	7,0	3.5	2.8	30	15	12	112	240	240	0.7	79	G	0.135	354	1900	45	67
DT112M 6	3	2.2	1140	8.9	4.45	3.55	50	25	20	164	180	220	0.78	78	н	0.254	486	1400	52	74
DT132S 6	4	3	1140	12.2	6.1	4.9	68	34	27	223	220	230	0.75	80	н	0.436	662	960	88	116
DT132M 6	5	3.7	1150	16.5	8.3	6.6	76	38	30	295	200	200	0.74	82	G	0.822	662	680	152	191
DT132ML 6	7.5	5.5	1150	23.0	11.5	<b>'9.2</b>	107	54	43	405	200	200	0.74	82	G	0.955	662	590	211	273
DT160M 6	10	7.5	1165	28.0	14.0	11.2	152	76	51	545	170	220	0.78	87	G	2.574	1740	360	255	317
DT160L 6	15	11	1165	40	20	16	260	130	104	800	200	220	0.79	87	н	3,1089	1740	180	256	318
DT180L 8	20	15	1170	50	25	20	370	185	148	1090	210	220	0.85	89	j	4.90 5.01')	1740 3470')	160	422	490 570')
DT200LS 6	25	18.5	1170	61	30.5	24.5	460	230	184	1340	210	220	0.85	89	J	7.10 7.34'}	1740 3470'}	140	444	490
DT200L 6	30	22	1170	73	36.5	29	540	270	216	1590	210	220	0.85	89	J	8.36 8.54')	1740 3470')	130	484	520

1) Double Disc Brake BH2

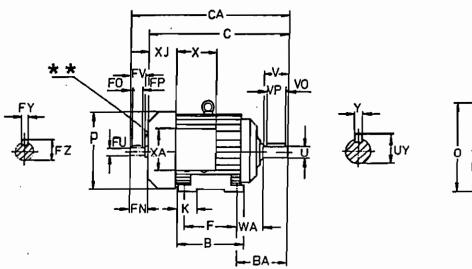
PLEASE NOTE: Max. No. of operations per hour (Zo) indicates: The Max. No. of start and stops a motor can handle thermally when the motor has no
load attached to it. The figure is used for computations.

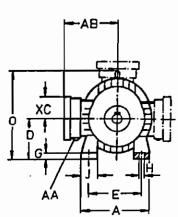


## **Electric Motors**

( Motors conform to applicable CSA - NEMA standards except for the frame size )

## **DIMENSION SHEET** · · · 08 075 09 US





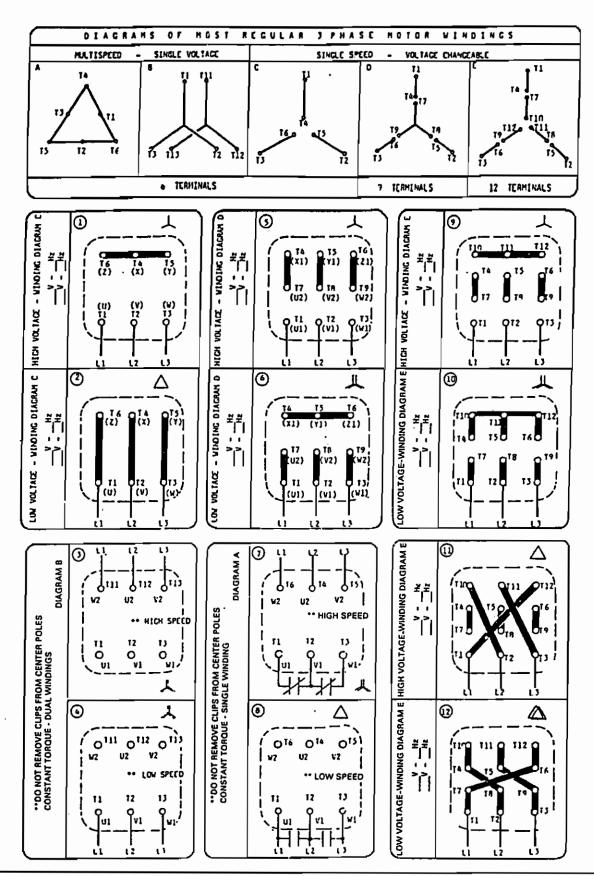
- 1) Fan guard flattened towards the bar
  3) 2 holes NPT
  4) Note: Dimension D = 160 mm l.e. 6.3 inches
  The eyebolt can be unscrewed

FRAM		DIMENS	A	AA <sup>31</sup>	A8	В	ВА	С	CA	D	E	F	G	н	1	κ	٥	P	WA	X XA	х¢	χJ	u v	VΟ	VP	UΥ	۲	Centr. DIN 332	fU	F۷	FN	FO	FP	FΥ	FZ
DT71K	_					452	205	0.02	10.08	3.30		,,,		20		. 20		5.71	,				.55		.87	.63	.20		.43	.91	1.06	n/	.79	16	.49
DT71C	_		5.67		5.43		2.95	9.02	110.06	2./9	7.41	13.54	.20	.28	₹20	1.26	-	3./1	1.77	5.43	1	ر ده		١,,		.63	.20	-	ا*`ا	.31	٠٠	ا".	./3	٠١٠	.43
DT71D	_			₩"	5.43		_	_	⊢		_	⊢		L	L	L	$\vdash$			l	2.09		1.18	۰۱٥	_		Ш	Н	Н				_	Ш	
DT80K	_		5.87	<u> </u>		4.92	3.54	11.38	12,72	3.15	4.92	3.94	.39	1	1.38	1.10	-	. 5.71	1.97	l	2.00		.75	П	1.26	.85	.24	-	.55	1.18	1.34		.87	.20	.63
DTBON	$\dashv$				<b> </b>					_	<u> </u>	⊢	-	.35	L	⊢	$\vdash$		⊢	ł		⊢	1.57	Н	-			Н	$\vdash$		$\dashv$		_	-	_
OT90S	$\dashv$		6.93		6.73	5.98	4.17	12.60	14.37	3.54	5.51	4.92	.31		1.30	1.26	-	7.76	2.20	4.17		1.14	.94 1. <del>9</del> 7	ı	1.57	1.06		-				.16			
DT90L	ᅴ				-	<u> </u>	<u> </u>				L	⊢	⊢	⊢	⊢	<u> </u>	-		┝	┝	⊢	Н	1.10	l					.75	1.57	1.77		1.26	.24	.85
DT100	_	in	7.40		6.89		4.84	14.49	16.26	3.94	6.30		47		1.57		-	7.76	2.48	6.22		1.26	1.10	<b>.</b>	1.97	1 22	.31	-						Ш	ı
DT1001	_		0.00			6.69	5 12		17.00	44:	2.00	5.51	<del> </del>	١.,		1.38	$\vdash$		- 75	ł	2.24	-	2.36	-24	,	1.22		Н	- 1	. 07	217	┥	1 67	Н	
DT112	_		9.84	¥"	7,40		3,12	_	17.68 20.63		7.48	ł	.55 .83	.47	1.85		┝═┥	8.70	2.76	4.49		1.42		H	_	_	-		Ī	2.36	2.17		1.57 1.97	.31	1.06 1.22
DT132	$\overline{}$		10.20	_	$\vdash$	250	6.65	18.35		5.20	8.50	7,00	182		2.44	1 77	12.68	10.831	3,50		H	Н	1,50	H		1.61	.39	-		2.30	2.30	لہ	1.57	Н	1.22
DT132	_	- 1	-		9.06		_	_		8.3041		7,00	.07	Н	2.60	1.//	12.00	10.03		7.17		1,69			2.76				1.50	3.15	3.35	-24	2.76	.39	1.61
DT160	-		11,38	1%'' 1%''		9.92					10	8.27	.98	.55	3.23	1.97	13.78	10.83	4.25		2.99		3.15	П				_				- 1			
DT160	_		12.13		9 96	11.57	8.58	23.54	25.24	6.30		10					14.92	13.031		5.98		6.18	1.65	.39		1. <b>7</b> 7	.47	-	1.65	4 27	4 53	30	2.76	47	1 77
D171K	_	$\neg$	12.10	$\vdash$	0.00	,,,,,,	Н	20.07	20.07		-	۳	ΪŤ	Н	2,33	2.00	17.32	13.03	-	3.50	┢	0.16	14	H				211		v.50	7		2.,,	,4,	```
DT71C	╗		144	l .		115	75	229	256	71	112	90	5	7	32	32	-	145	45	138			14		22	16	5	ОМ 5	11	23	27	۱	20	4	12,5
DT71D	-		•••		138								ĺ								l	15	30	4				9							
DT80K	$\neg$		140	₩.,			20	200	222					Н					_		53		19	ΙI			$\overline{}$	DM		$\overline{}$		┪	22	Ţ	
DTBON			149			125	90	289	323	80	125	100	140		35	28	-	145	50				40		32	21,5	8	6	14	30	34	- 1	"	5	16
DT90S	$\neg$		176			152	106	320	365	90	140	125	8	9	33	32	,—	197 13	56	106		29	24	Н	40	27		DМ	_	$\neg$		- 1			┪
DT90L	┪		170		171	132	100	320	300	30	140	123	I°ا		33	34	-	197	30	tuo		29	50	Н	40	"		_	19	40	45	4	32	6	21.5
DT1001	S	mm	100		4.5.5		123	368	413	100	160	_	12	_	40	$\vdash$	_	197	63	158		32	28			_		DM:		~	~	J		ľ	٦
DT1001	$\Box$		188		175	170	12.5	300	713	100	100	140	''		#2	35	-	137	03	130	57	34		5	50	31	-	10							
DT1128	$\overline{}$		220	*"	188	1/0	130	394	449	112	190	1140	14	12	47	33	-	221	70		ا "ا	36	60	٦					24	50	55	_	40		27
DT1325	П		250	74	.~		169	459	524	132	216		21		62		_	221	89	114		<b>30</b>	38	П			-	οм	28	60	65		50	<u> </u>	31
DT132N	┰	ĺ	259			218		466	551	132	£10	178	17		66	45	322	275 <sup>11</sup>	23	182						41	10	12				5	П		
DT132A	1L		289	1%"	230	252	188	526	611	16041		210	П		92	50	350	275			76	43	80		70			·	38	80	85			10	41
DT160	A	1	200	1%"		232	218	556	641	160	254	<b>L</b> '''	ka	14	82	العا	220	4/3	108		,,		42	10		45	12	DM				_	70		
DT160t			308		308	294		598	713	100	L	254	19	L	75	65	379	331 1)		152		157	110				•	16	42	110	115	10		12	45

FRAME	TYPE	_CERTIFIED FOR		ORDÉR
ITEMHP	RPMPH	_HZVOLTS	GEAR DATA-	BRAKE DATA-
EURODRIVE SALES ORDER-			APPROVED BY-	191

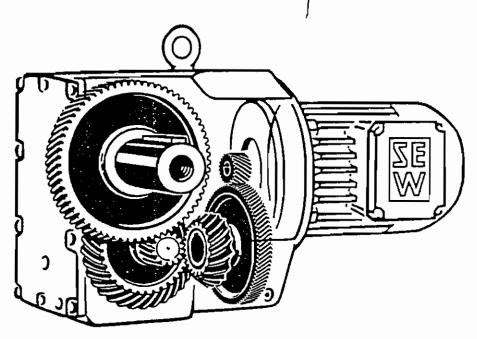


#### Motor Winding Diagrams & Terminal Box Connections for 3 Phase Motors



## Service and Repair Instructions Right-Angle Helical Bevel Reducers

Type K/KF/KA/KAF 66-126



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K-004-01

March 1989

Supercedes: Jan. 1989

#### Tools and Equipment

Tools, equipment, and material needed to repair the SEW-Eurodrive helical-bevel gear unit will depend on the unit size and type and the nature of the repair, but may include:

- 1. Metric wrenches and sockets
- 2. Torque wrenches
- 3. Metric socket head wrenches
- 4. Punches and cold chisels
- 5. Snapring pliers
- 6. Hand and hydraulic presses
- 7. Lifting equipment
- 8. Pry bars
- 9. Soft and hard faced hammers
- Wood or plastic blocks or wedges
- 11. Depth gauges, indicators, and feeler gauges
- 12. Sealants
- 13. Proper lubricants

## General Repair Procedures

#### Bearings

Bearings must be removed and installed on shafts by pressing only on the inner race or in bearing bores by pressing only on the outer race with a pressing tool of the proper size. Do not hammer on any bearing during installation or removal. To facilitate installation, the inner and outer races of taper roller bearings can be heated to 80°C to 100°C.

Bearings used within the helical-bevel gear units may be either grease or oil lubricated depending upon the mounting position. Bearings that employ shields and/or external nilos rings are grease lubricated and must be packed with grease during assembly.

Input grease lubricated bearings should have only 1/3 of their free volume filled with grease in order to avoid overheating the bearing. For output bearings and bearings with replaceable grease shields fill to 2/3 of the free volume.

If reusing a grease lubricated bearing, thoroughly clean the old grease from the bearing with an ap-

propriate solvent prior to repacking. Only use a solvent made especially for cleaning grease from bearings. Gasoline is not a suitable solvent.

When installing nilos rings or bearings with shields they must be in the same position as when removed from the gear unit.

#### Oll Seals

Shaft oil seals are easily damaged by dirt, exposure to solvents, and rough handling. The steel cases are easily bent. Seals should be kept wrapped and away from the immediate work area until they are to be installed. Never reuse an oil seal.

Shaft extensions with keyways should be taped and care should be taken when installing seals over shaft shoulders without chamfers to avoid damaging the seal lip during installation. Seals should be installed with sleeve-type press fitting tools and an arbor press to assure smooth uniform installation pressure. Seals must be installed square to the shaft. Prelubricating the seal lip and seal bore with the same oil that will be used in the gearcase aid in the installation of the seal.

A thin coat of anaerobic joint sealant on the seal outside diameter, especially those with an exposed steel casing, will help assure a leak-free installation.

#### Gears

Removing and installing gears requires the proper tools to prevent damage. Screw type gear pullers should be used with care to avoid damaging the gear teeth. On the larger gear units hydraulic presses are required to change the output gear. To aid the installation of gears, heat the gears to 120°C to 140°C and drop them into place on the shafts.

#### Flanges and Tenons

After disassembly, clean all mating flanges and tenons of sealant and/or gasket material. Inspect the mating surfaces for any damage resulting from the disassembly procedure. File smooth any nicks or raised areas. Failure to properly prepare mating surfaces may result in oil leakage in the repaired unit.

#### Sealants

SEW-Eurodrive uses various anaerobic sealants and gasket sealants in the assembly of the helical-bevel gear unit.

The output covers and flanges must be sealed with Loctite TM 574, a liquid anaerobic sealant. All other mating flanges and tenons can be sealed with any good quality anaerobic sealant or RTV silicone sealant that is designed for high temperature automotive engine use and is impervious to the gear oil. A gasket sealant should be used with all gaskets to assure leak-free operation after repair.

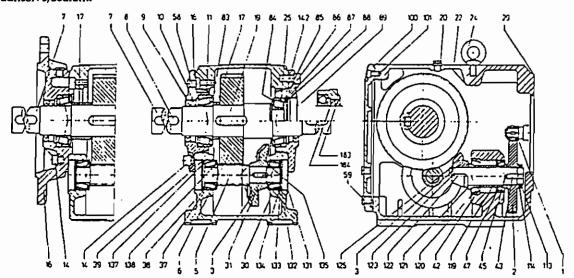
Follow the sealant manufacturer's guidelines for application and cure time. All surfaces to be sealed must be clean and free of oil and grease. Use the sealant sparingly. Normally an 1/8 inch continuous bead is sufficient to seal the mating surfaces. Apply the sealant to the machined surface of the gear housing between the bolt holes and the inside (oil side) edge of the housing. Any through tapped holes in the machined surface must have the top threads of the tapped hole coated with a suitable thread sealant. For easy disassembly later be sure to use only a thread sealant on the tapped holes and not a thread locking adhesive/sealant.

## Preparation for Repair

Remove the helical-bevel gear unit from the driven equipment. Remove any sprockets, belt sheaves, couplings, and keys from the input or output shaft extensions. Clean the outside of the drive thoroughly before moving it into the work area.

Drain the oil from the gearcase and discard the oil appropriately. Do not reuse the oil. If the drive is still warm, use extreme care when draining the oil as hot oil can cause severe burns.

Before disassembly inspect the input and output shafts for nicks or damage caused by set screws, clamps, etc. Smooth the shaft extensions with a fine toothed file as necessary. It is generally a good idea to completely wrap the shaft extensions with one or two layers of plastic electrical tape to protect the shafts as well as the hands.



Typical Parts Breakdown View for K/KF66-126 (K/KF96 shown)
See appropriate Parts List for your specific gear unit.

## Disassembly

#### Input Device

The helical-bevel gear unit may have a motor, input cover assembly, C-Face adapter, mechanical VSD, etc. as the input to the gearcase. All input devices are removed and replaced by the same procedures.

When working with the input device take care not to damage the attached pinion. Pull the input device straight out until the tenon is disengaged and then swing the input device to bring the gears out of mech.

 Support the input device so that it will not fall when it is removed. Use of slings is recommended.

- 2. Remove the bolts and/or nuts securing the input device to the gearcase.
- 3. Place a sharp cold chisel on one side of the gearcase where the input device flange mates with the gearcase and strike the chisel sharply with a heavy hammer to break the seal. As soon as one side separates, move to the other side of the gearcase and use the chisel and hammer to separate that side.
- Use siender pry bars to complete the separation of the input device from the gearcase.

#### Output shaft and gear

- Remove end cover #100 by removing the socket head screws #101. It will be necessary to use a sharp cold chisel and a heavy hammer to break the seal between the end cover and the gearcase.
- 6. Remove the output flanges and/or sealing flanges #16 and #85 by removing the socket head screws items #14 and #142 respectively. It may be necessary to use a sharp cold chisel and a heavy hammer to break the seal between the gearcase housing and the output flanges and/or sealing flanges.
  - On K/KF126 it will be necessary to remove closing flange #97 by removing the socket head screws #96.
- 7. Turn the gearcase on its side so that the bevel gear #3 is on the bottom side.
- Support the output gear #6 with blocks between the gearcase and the output gear so that as the output shaft is pressed out the output gear does not move.
- Place the gearcase in a press and press the output shaft out of the gearcase while supporting the output shaft so that it does not fall.
- After the output shaft has been pressed out, the output gear can be removed from the gearcase.
- 11. Remove and discard the oil seals #9 (#10) and #183 (#184) from the flanges. Also at this time remove any snaprings #88, thrust washer #87, shims #86, nilos rings #83 and #84, and closing caps #89 from the flanges as required by the nature of the repair.
- 12. Remove bearings #11 and #25 from the output shaft #7 and/or from the flanges #16 and #85 as the case may be.

#### Bevel gear and shaft

- 13. Remove both closing caps #131 by placing a sharp chisel or punch near the center of the closing cap and striking the chisel sharply to puncture the closing cap and pry out.
- 14. Remove snaprings #39 and #132, shims #38 and #134, and thrust washers #133 and #137.
- 15. Turn the gearcase on its side so that the bevel gear #3 is on the top side.
- 16. Support the bevel gear with blocks between the gearcase and the bevel gear so that as the pinion shaft #5 is pressed out the bevel gear does not move.
- 17. Place the gearcase in a press and press the pinion shaft #5 out of the gearcase while supporting the shaft so that it does not fall.
- 18. Remove bearings #30 and #37, and nilos rings #135 and #138 from the gearcase housing and/or pinion shaft #5 as required.

#### Bevel pinion and shaft

- Remove snapring #115 and shims #116 or lock nut #113 and locking washer #114.
- 20. Stand the gearcase on its end with gear #2 on top. Support the gear #2 with blocks between the gearcase and the gear so that as the bevel pinion shaft #3(#123) is pressed out the gear #2 does not move.
- 21. Place the gear case in a press and press the bevel pinion shaft #3(#123) out of the gearcase while supporting the shaft so that it does not fall. Inner race and rollers of bearing #42 and spacer #119 will come out with the bevel pinion shaft #3(#123).
- Remove gear #2, roller bearing, #45, snapring #47, spacer #117 (if present), and outer race of bearing #42.
- 23. Bevel pinion shaft:

#### 2 piece

Remove snapring #125 and press pinion shaft out of bevel pinon. Remove spacer #119, inner race of roller bearing #42, and shirns #120 and #121 from bevel pinion shaft.

#### 1 piece

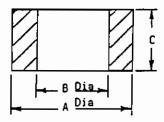
Remove spacer #119, inner race of bearing #42, and shims #120 and #121 from bevel pinion shaft (Bevel pinion and shaft are one piece).

## **Assembly**

- 1. Oil all bearing bores before installing bearings.
- Bevel pinion and bevel gear are matched and, if required, must be replaced as a sci.

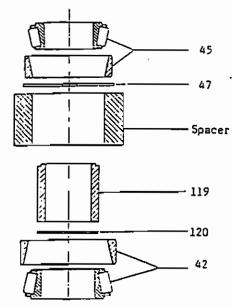
#### Bevel pinion and shaft

- 2. Determine the shimming required for bearings #42 and #45.
  - a) Make a spacer to the appropriate dimensions.

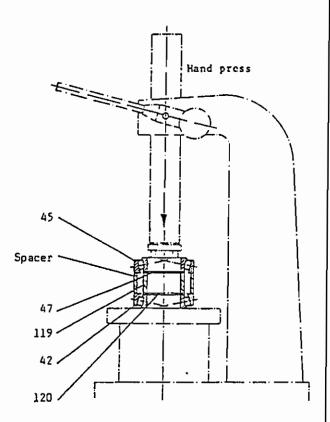


_	Dimen	Dimensions in millimeters									
Gearcase Size	A	В	C005								
66	56	38	23.010								
76	70	50	26.310								
86	90	66	38,510								
96	95	72	46.310								
106	130	100	44.800								
126	160	125	53.510								

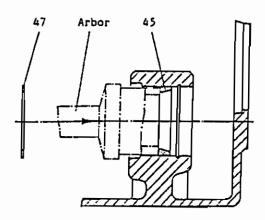
b) As shown, stack the bearing #42, spacer #119, shims #120, snapring #47, spacer made in a), and bearing #45 in a hand press. Initially use 0.5mm shims #120 for K66-K106 and 0.7mm shims #120 for K126.



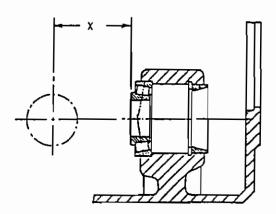
c) With the hand press apply slight pressure to the stack while rotating the bearings. Shims #120 are either added or removed until the spacer #119 and the one made in a) are well secured between the two bearings and the bearings rotate with ease.



3. Press outer race of bearing #45 into bearing bore.



- 4. Install snapring #47 and push outer race of bearing #45 against the snapring.
- 5. Press outer race of bearing #42 into place.
- 6. Determine the shimming required for bevel pinion #3.
  - a) Place inner race of bearing #42 into position and secure in place by means of an appropriate clamp.



b) Measure the distance X in millimeters from the face of the inner race of bearing #42 to the centerline of the cross bore for shaft #5.

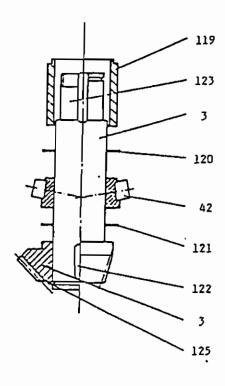
The difference between the value X and the dimension inscribed on the bevel pinion #3 is compensated for by means of shims #121. (X must always be greater than the value shown on the bevel pinion or assembly will not be possible).

#### 7. Bevel pinion

#### a. 2 piece

Install snapring #125, and key #122 onto shaft #123. Press on bevel pinion #3, install shims #121 as determined in step 6, press on inner race of bearing #42, install shims #120 as determined in step 2, and install spacer #119 onto shaft #123.

If spacer #119 has relief it must be toward bearing #45.

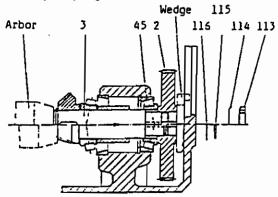


#### b. 1 piece

Install shims #121 as determined in step 6, press on inner race of bearing #42, install shims #120 as determined in step 2, and install spacer #119 onto shaft #3.

- Place preheated inner race of bearing #45 in its outer race.
- 9. Install key #43 in gear #2.

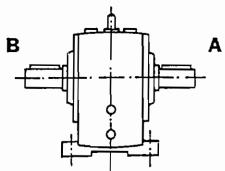
10. Place preheated gear #2 (and spacer #117 on K/KF/KA/KAF 126 only) in position and trap with a wooden or plastic wedge. Slide bevel pinion assembly into bearing bore and press completely together.



- After bearing races and gears are completely cooled down:
  - a) K66-86 Install shims #116 to eliminate any free float and install snapring #115.
  - b) K96-126 With gear #2 blocked so that it does not rotate, install locking washer #114 and lock nut #113 and tighten securely. Secure nut in position by bending over a tang on locking washer.

#### Bevel Gear and Shaft

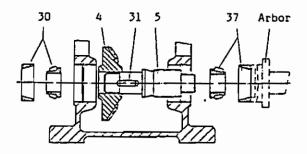
12. From the gear reducer nameplate, determine the mounting position. The mounting position designation consists of a series of letters and numbers with the suffix letters A and B to indicate output shaft and/or flange position. When looking at the helical-bevel reducer from the end opposite the input side, the right hand side is A and the left hand side is B.



In the standard assemblies the bevel gear is always on the opposite side of the gear reducer from the output shaft and/or flange position.

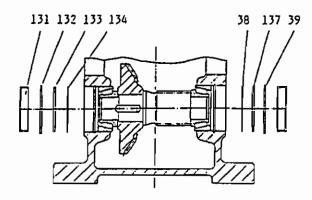
Gearcase	Output Shaft At	Flange At	Bevel Gear At
K, KF	Α	Α	В
K, KF	В	В	Α
K double			
extended shaft	A&B	-	В
KFF	A&B	A&B	В
KA	•	-	В
KAF	-	A	В
KAF	•	В	Α

- 13. Install key #31 in keyway on pinion shaft #5.
- 14. Place the preheated bevel gear inside the housing on A-side or B-side as determined in step 12. Then slide pinion shaft #5 into bevel gear.
  NOTE: Bevel pinion and bevel gear are matched and, if required, must be replaced as a set.
- For mounting positions V5, H5, and V1 install nilos ring #135 on pinion shaft #5.
- 16. For mounting positions V6, V1I, and H6 install niles ring #138 on pinion shaft #5.
- 17. Slide the preheated inner races of bearings #30 and #37 onto the pinion shaft #5.



18. Press the outer races of bearings #30 and #37 into the housing.

19. After the bevel gear and bearings are completely cooled down set the circumferential backlash (tooth clearance) of the bevel gear set to the appropriate value. Install shims #38 and #134, thrust washers #133 and #137, and snaprings #39 and #132 on both sides in such a way to achieve the prescribed backlash. With proper backlash setting, sufficient shims are installed so that the snaprings can only be installed with difficulty.



Gearcase Size	Circumferential Backlash (tooth clearance) (mm)
66	0.08-0.11
76	0.08-0.11
86	0.10-0.13
96	0.10-0.13
106	0.12-0.14
126	0.14-0.17

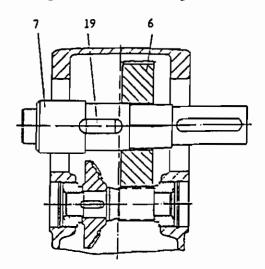
20. Install closing caps #131.

#### K/KF66 and 76

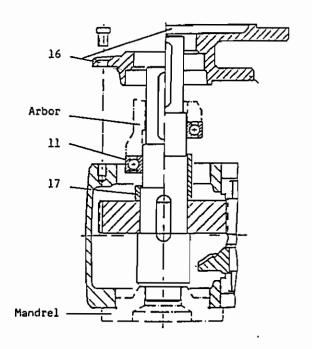
#### Output gear and shaft

- 21. Jam the bevel gear with a wooden or plastic wedge to prevent rotation.
- 22. Install key #19 in keyway on output shaft #7.

23. Place preheated gear #6 into position inside the housing and slide shaft #7 into gear #6.

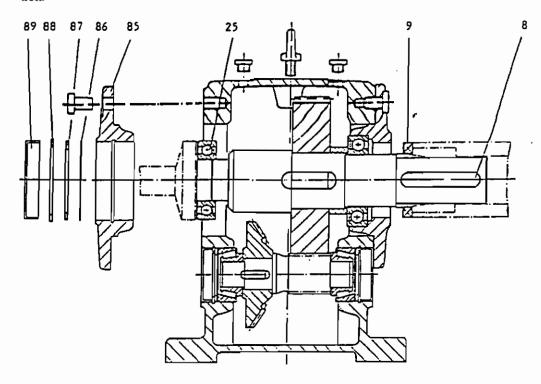


24. Rotate the housing on its side and support the shaft #7 as shown.



- 25. Install spacer #17.
- Press on bearing #11. Be sure to prelubricate the bearing before installation.
- Install sealing flange or output flange #16 and secure with the socket head screws #14. (Provide surface sealing).

 Turn housing upright. Press on bearing #25. Be sure to prelubricate the bearing before installation.



#### For single shaft extension

- Install sealing flange #85 and secure with the socket head screws #142. (Provide surface sealing).
- 30. Install shims #86 to eliminate any free float, thrust washer #87, and snapring #88.
- 31. Install closing cap #89.
- Install oil seals #9 (#10) in the scaling flange or output flange #16.

#### For double shaft extension

- 29. Determine the required number of shims #86.
  - a) Measure the distance from the housing sealing surface to the face of the bearing #25.
  - b) Measure the distance from the flange sealing surface to its bearing locating shoulder.
  - c) The difference between the distances in a) andb) is the amount of shims #86 required.
- 30. With the appropriate number of shims #86, install the sealing flange or output flange #85 and secure with socket head screws #142. (Provide surface sealing).

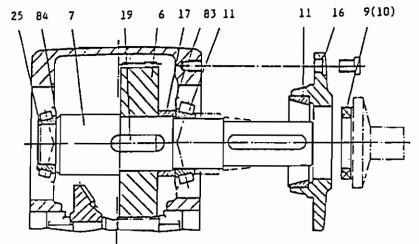
 Install oil seals #9 (#10) and #183 (#184) in the sealing flanges or output flanges #16 and #85.

#### K/KF 86-126

#### Output gear and shaft

- Jam the bevel gear with a wooden or plastic wedge to prevent rotation.
- 22. Install key #19 in keyway on output shaft #7.
- 23. Place preheated gear #6 into position inside the housing and slide shaft #7 into gear #6.

24. Install spacer #17, nilos rings #83 and #84, and preheated inner races of bearings #11 and #25 onto output shaft #7.



- 25. Press outer race of bearing #11 into sealing flange or output flange #16.
- Install sealing flange or output flange #16 and secure with socket head screw #14. (Provide surface sealing and lubricate bearing).

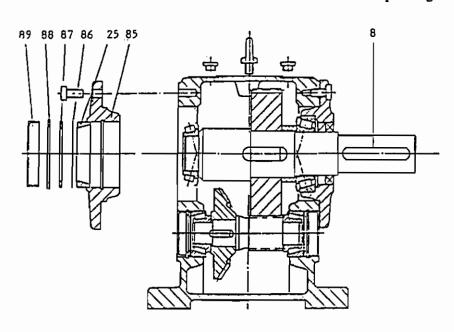
#### For single shaft extension

Install sealing flange #85 and secure with socket head screws #142. (Provide surface sealing).

- 28. Lubricate the bearing #25 and install the outer race of bearing #25 into the sealing flange #85.
  29. For K/KF86-106
  - a) Install the shims #86, thrust washer #87, and snapring #88. Use sufficient shims so that the snapring can only be installed with difficulty.
  - b) Install closing cap #89.

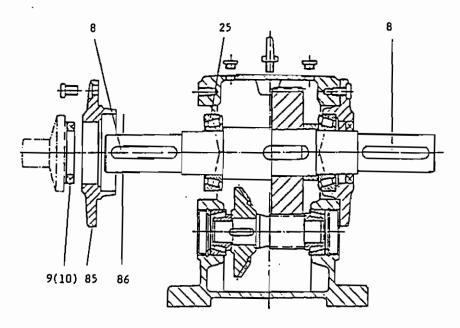
#### 29. For K/KF126

- a) Determine the required number of shims #86.
  - With the outer race of bearing #25 in place, measure the distance from the housing sealing suface to the face of the bearing #25.
- Measure the distance from the closing flange #97 sealing surface to its bearing locating shoulder.
- The difference between the distances in a) and b) is the amount of shims #86 required.
- b) With the appropriate number of shims #86, install the closing flange #97 and secure with socket head screws #96. (Provide surface sealing).
- 30. Install oil seals #9 (#10) in the sealing flange or output flange #16.



#### For double shaft extension

- 27. Determine the required number of shims #86.
  - a) With the outer race of bearing #25 in place, measure the distance from the housing sealing surface to the face of the bearing #25.
  - b) Measure the distance from the flange #85 sealing surface to its bearing locating shoulder.
  - c) The difference between the distances in a) andb) is the amount of shims #86 required.



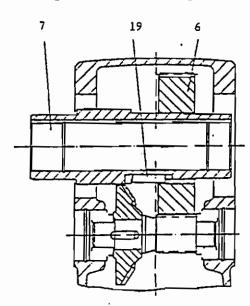
- 28. Install the appropriate number of shims #86 and press outer race of bearing #25 into sealing flange or output flange #85.
- Install sealing flange or output flange #85 and secure with socket head screws #142. (Provide surface sealing).
- 30. Install oil seals #9 (#10) and #183 (#184) in the sealing flanges or output flanges #16 and #85.

#### KA/KAF 66-126

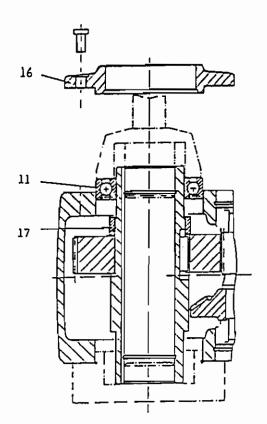
#### Output gear and shaft

- 21. Jam the bevel gear with a wooden or plastic wedge to prevent rotation.
- 22. Install key #19 in keyway on output shaft #7.

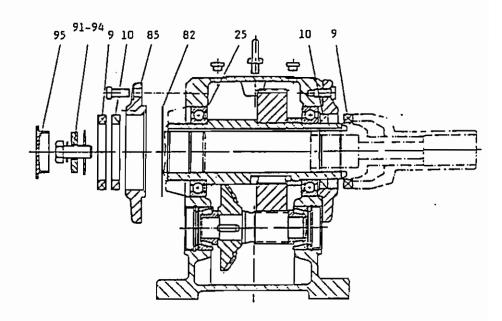
23. Place preheated gear #6 into position inside the housing and slide shaft #7 into gear #6.



24. Rotate the housing on its side and support the shaft #7, as shown.



- 25. Install spacer #17.
- 26. Press on bearing #11. Be sure to prelubricate the bearing before installation. For KA/KAF 106-126, install nilos ring #83 before installing bearing #11.
- Install sealing flange or output flange #16 and secure with the socket head screws #14. (Provide surface sealing).
- 28. Turn housing over and press on bearing #25. Be sure to prelubricate the bearing before installation. For KA/KAF 106-126, install nilos ring #84 before installing bearing #25.
- 29. Determine the required number of shims #82.
  - a) Measure the distance from the housing sealing surface to the face of the bearing #25.
  - b) Measure the distance from the flange #85 sealing surface to its bearing locating shoulder.
  - c) The difference between the distances in a) andb) is the amount of shims #82 required.



- With the appropriate number of shims #82, install the sealing flange or output flange #85 and secure with socket head screws #142. (Provide surface sealing).
- 31. Install oil seals #9 (#10) and #183 (#184).
- 32. Install snapring #91, disc #92, lockwasher #93, and hex head bolt #95 into the hollowshaft.
- 33. Install closing cap #95.

#### Final Assembly

- Install cover #100 and secure with socket head screws #101. (Provide surface sealing).
- 35. Install key #8 into keyway on output shaft #7.

- Screw in eyebolt, oil level and drain plugs, and breather. See Mounting Positions chart for correct location of oil plugs.
- 37. Place input gasket #29, if required, in place and install the input assembly. Secure input assembly with appropriate bolts and/or nuts.
- 38. Fill with proper lubricant. See Lubricant Schedule for recommended lubricants and approximate quantities.
- 39. Trial run and test for unusual noises and/or oil leaks.

## Lubrication

#### Schedule

LUBRICATION TYPE	AMBIENT <sup>1)</sup> AIR TEM- PERATURE RANGE *F	KIN VISCOSITY AT 40°C (cSI) APPROX.	GULF OIL CO.	CHEVRON OIL CO.	AMERICAN OIL CO.	MOBIL OIL CO.	SHELL	TEXACO CO.
	+104 to +32	210	Gulf E.P. Lubricant S 100	Chevron Non-Leaded Gear Compound 220	SPARTAN EP 220	Mobilgear 630	Shell Omala Oil 220	Meropa 220
Oil	+77 to +5	145	Gulf E.P. Lubricant S 60	Chevron Non-Leaded Gear Compound 150	SPARTAN EP 150	Mobilgear 629	Shell Omala Oil 100	Meropa 150
Grease Used for normal temp. range — 2			Gulfcrown Grease E.P. No. 2	Chevron Dura-Lith BEACON 3	ESSO Multipurpose Grease BEACON 2	Mobilux EP2	Shell Alvania Grease R 3	Multiflak EP-2

Mineral oils and greases should be changed every 10,000 operating hours or 2 years. Repack high speed (input) bearings to 1/3 of the available free bearing space. Repack low speed (output) bearings to 2/3 of the available free space.

Synthetic oils and greases should be changed every 20,000 operating hours or 4 years.

Under severe operating conditions (e.g. high humidity, aggressive environment, large temperature fluctuations or high ambient temperatures) shorter oil change intervals are necessary.

#### Quantity in (US) Gallons

		MOUNTING POSITIONS												
FRAME SIZE	B3, H1 B5;	B31	. B5	8511	BSIII	B6	B8	V1 V11	V5	V6	H2	нз	H4	H5, H6
K, KF, KA 66	0 24	0.90	0.63	0.90	0.79	0.63	0.79	0.82	0.87	0 87	0.77	0.87	0.61	0.85
K. KF, KA 76	0.45	1.64	1 32	1.69	1.56	1.29	1.51	1.64	1.74	1 74	1 45	1.59	1.24	1.69
K KF, KA 86	0 66	2 51	211	2.67	2.51	2.06	2 40	2.75	2.64	2.54	2.27	2.38	1.93	2.51
h KF, KA 96	1 27	4 76	3.65	4.91	4.39	3.57	4.23	5.18	5.02	5.02	4.10	4.62	3.43	4.89
K, KF KA 106	2 11	8.45	647	8.72	7.66	6.34	7 40	8 72	8 45	8.45	7.13	8.19	6.08	8.19
K. KF, KA 126	3.70	15 85	11 89	14 80	14 27	\$1.62	13 74	16.91	16.38	16.38	13.21	15 32	11,10	15.85

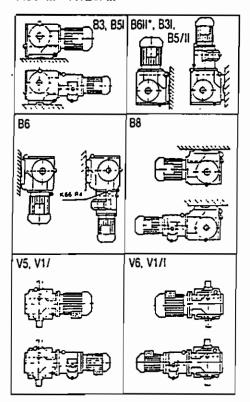
Note: The capacities are approximate, being dependent on the gear ratio.

Weight of oil: Approximately 7.5 lbs/gallon.

<sup>1)</sup>Consult factory for ambient temperatures outside the ranges shown.

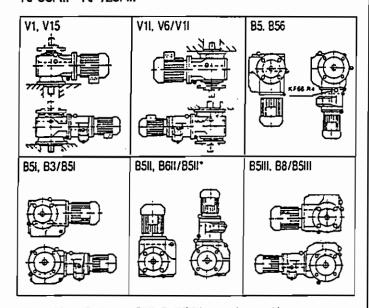
## Mounting Positions

K66 - K126 K66R.. - K126R..



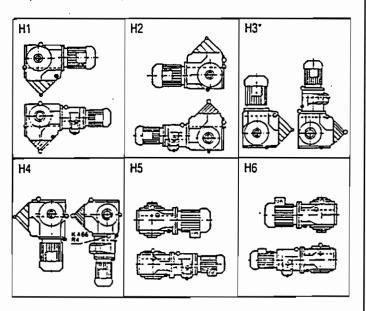
\*K66-K126 Reducers: B6II mounting positions are non-ventilated.

KF66 - KF126 KF66R... - KF126R...



\*KF66-KF126 Reducers: B5II, B6II/B5II mounting positions are non-ventilated.

KA66 - KA126 KA/KAF66R.. - KA/KAF126R..



\*KA66-KAF126 Reducers: H3 mounting positions are non-ventilated.

Symbols: Mounting surfa

Breatner Plug

OH - Level Plug - Red

Drain Plug - Blue

# Tightening Torques for Metric Threaded Fasteners

# Hex Head or Hex Socket Screws (Normal Thread Series)

Thread	Torque (lb-in) for				Hex Head
Size	Grade 4.8	Grade 6.8	Grade 8.8	Grade 10.9	Socket Wrench Size (mm)
M5	27	40	53	75	8
M6	50	73	97	125	10
M8	115	170	220	310	13
M10	220	320	425	610	17
M12	-	575	760	1060	19
M14	-	895	1195	1680	22
M16	-	1400	1860	2610	24
M18	-	1930	2565	3540	27
M20	-	2725	3630	5135	30
M24	-	4715	6285	8850	36
M27	-	6990	9295	13275	41
M30	-	9645	12850	17700	46
M36	•	16650	22150	31400	55_

Oil Plugs

Thread Size	Torque in lb-in	
M10x1	105	
M12x1.5	175	
M22x1.5	710	
M33x2	1150	
M42x2	1415	

#### 10.17 <u>DEWATERING BELTS</u>

10.17.1 Belt Data Sheet: Attached

10.17.2 Belt Use Record Sheet: Attached

#### 10.17.3 Belt Cleaning Instructions:

- a. Run wash water and belt drive (no sludge or polymer) for a minimum of 45 minutes per day of dewatering.
- b. If additional cleaning is desired, Apply mild soap directly onto the belts or inject into the spray wash system for one hour.

Note: Do NOT steam clean the belts. Steam cleaning will damage the belts. Use a maximum of 1,500-psi water at a maximum of 130 degrees F. Do not wash belts with hot water while they are under tension as this will cause stretching.

#### 10.17.4 Belt Repair Procedures:

#### a. Belt Puncture:

- (1) Clean around the puncture and allow belt to dry.
- (2) Using scrap belt material, cut a patch to size.
- (3) Coat area with marine epoxy and apply patch.
- (4) Allow epoxy to dry before operating press.

*Note*: When using marine epoxy, ensure belt is clean and dry before applying epoxy. Apply epoxy to both belt and patch as evenly as possible. Let epoxy thoroughly dry before operating. Dewatering will not occur in an area coated with marine epoxy.

#### b. Belt Edge Fraying:

- (1) Clean belt edge and allow belt to dry.
- (2) Cut off excess strands.
- (3) Apply marine epoxy and allow epoxy to dry.

10.17.5. <u>Belt Installation</u>: See Section 7.6.3 for belt installation and safety.

- a. For belt installation when there are no belts on the machine see Section 7.6.3 for belt installation and safety.
- b. Follow these instructions for replacing existing belts on the machine.

WARNING: Do not disable any alarms on the machine by disconnecting wires at the control panel or the junction box. The alarms exist to protect yourself and the equipment

- 1. See Section 7.6.3 for belt installation safety.
- Energize the belt drive and run the belts until the clipper seam is at a convenient location for access.
   This will be at the beginning of the gravity deck for the upper belt and the vertical wedge for the lower belt.
- 3. Stop the belt drive and retract the tension cylinders to remove tension from the belts.
- 4. Remove the belt seam wire and then connect the new belt onto the trailing edge of the old belt. Ensure the seams are properly meshed together and reinstall the belt seam wire.
- 5. Loosen the broken belt sensor proximity switches and move them back away from their original position by about ¼ to ½ inch.

WARNING: The belt drive will not operate unless the hydraulic pump is running and the belts are tensioned. The tension roller will move to its fully extended position when the tension valve is placed in the tension position. Ensure no personnel or equipment is in the path of the tension roller as it extends.

- Place the tension control valve in the belt tension position and allow the tension cylinders to extend to their full stroke.
- 7. Energize the belt drive and allow the old belt to pull the new belt into the machine.
- 8. Roll up the old belt as it comes out of the machine.
- 9. Retract the tension cylinders and seam the ends of the new belt together with a new seam wire.
- 10. Repeat with the second belt.
- 11. Replace the broken belt sensor proximity switches and adjust to their original positions.

#### 10.17.6 Possible Causes for Belt Tracking Problems

Occasionally a problem will arise where one or both belts of a belt filter press will not track properly. When this happens look for these possible causes.

#### When both belts wander off track:

Uneven sludge distribution across the width of the machine will make the belts steer away from the heavy side because the higher sludge load between the belts makes the belt on the outside behave as though it were on a steering roller turned away from the heavy side. This occurs to both belts alternately as they go around the rollers. When the belt is on the inside against the roller it WP84-10 Rev. 2

does not see the uneven sludge thickness, but when it is on the outside it will be steered "down hill" away from the heavy side. Correct the sludge distribution at the inlet spreader. In extreme cases of off center sludge loading the steering system will not be able to compensate and the belt will go into the over travel limit switches. Also, serious cases will cause diagonal creasing and destruction of the belts. If the belt seam is not straight across the machine this is evidence that the sludge loading has not been correct in the recent past. The seam will lag behind on the heavier loaded side and, if run this way long enough, will not recover even if the sludge distribution is corrected.

A pressure roller bearing that has come loose from its mounting to the frame will allow the roller to get out of alignment and it will act like a steering roller and cause both belts to track toward one side. This may be detected by observing that the steering cylinders are staying off center or are hunting for their balance point. If the bearing housing has moved enough to cause this problem you should see the mark on the frame showing it has moved from its original place. Put the bearing back where it was and check all the bearing mounting bolts for tightness. Observe for correct tracking without hunting.

Check for bearings that have been moved in an attempt to "realign" the rollers. Sometimes this is done in the field by persons attempting to make a damaged or irregular belt track straight. When the belt wears or is later replaced, then tracking problems will begin. Put all the rollers back in their original places so they are parallel. Be sure to check that all the bearing bolts are tight.

#### When one belt wanders off track:

Uneven sludge distribution across the width of the machine will make the belts steer away from the heavy side because the higher sludge load between the belts makes the belt on the outside behave as though it were on a steering roller turned away from the heavy side. Uneven sludge distribution usually affects both belts, but in mild cases or if the belts have been stretched only one belt may be affected. Look for creases in the belts or belt seams that have been pulled in a diagonal. See the paragraph above.

An idler roller bearing that has come loose from its mounting to the frame will allow the roller to get out of alignment and it will act like a steering roller and cause one belt to track toward one side. This may be detected by observing that its steering cylinder is staying off center or is hunting for its balance point. If the bearing housing has moved enough to cause this problem you should see the mark on the frame showing it has moved from its original place. Put the bearing back where it was and check all the bearing mounting bolts for tightness. Observe for correct tracking without hunting.

Check for bearings that have been moved in an attempt to "realign" the rollers. Sometimes this is done in the field by persons attempting to make a damaged or irregular belt track straight. When the belt wears or is later replaced, then tracking problems will begin. Put all the rollers back in their original places so they are parallel. Be sure to check that all the bearing bolts are tight.

It is possible for the tension equalizing rack and pinion to get out of time. If the rack is clogged with dried sludge or there is any looseness in the assembly the pinion can jump a tooth and make the tension roller be out of line. Uneven sludge distribution can provide the force to cause this WP84-10 Rev. 2

to happen. Observe when you fully retract the tension cylinders if one side hits bottom first; or you can measure the distance between rollers or count the teeth. Clean the rack and reset the timing.

Intermittent steering problems, those that return after you have "fixed" the problem and watched the machine run fine for hours, can be the result of trash in the hydraulic lines. Take off the steering valves and flush the lines. Try swapping the steering valves between the upper and lower belts to see if the problem goes with the valve. If the filters in the fittings on the valve are clogged with dirt it may not be obvious and you may not be able to clean them. Replace the fittings or the entire valve.

A dirty or damaged steering valve will not respond to the movement of the belt and the steering cylinder may stay at one end of its travel for too long and then switch completely to the other end. Clean or replace the steering valve. Also, look for a broken spring on the paddle arm. If the arm is damaged or loose on its shaft the same effect may be observed.

The early steering cylinders had chrome plated steel rods that can rust where there are microscopic pores in the plating. After a long time in service the rod can become so rough that it will stick in the rod seal or bushing and the cylinder action will be erratic, not responding immediately to movement of the steering paddle. Look for leaking seals and rough spots on the cylinder rod. Replace the cylinder. The new steering cylinders have solid stainless steel rods that will not rust and there is no plating to flake off.

Wear or damage to the steering bearing pivot assemblies can cause irregular tracking action. Make sure the pivots are in good condition and there is no looseness.

Sometimes a new belt gets stretched on one side by uneven sludge loading. When the belt tension is applied the belt will be tight like a drum head on one side of the machine and slightly slack on the other. A stretched belt will not track straight. Sometimes the belt can be straightened by running it for a while at maximum belt tension with only the wash water on. Apply hot water if it is available and the straightening will happen faster, but don't over do it.

#### The basic steps in recovering from a belt tracking accident

- 1. turn off the power and disconnect the belt misalignment switches
- 2. turn on the power and start the hydraulic unit
- 3. retract the tension cylinders to loosen the belts.
- 4. turn off the power
- 5. manually pull the belts back to center
- 6. start the press and allow it to run without sludge until clean
- 7. observe the belt tracking
- 8. watch for proper operation of the belt steering
- 9. if belt tracks OK and steering is working, shut down the press
- 10. turn off the power and reconnect the misalignment switches
- 11. place the press back in service
- 12. watch for tracking problem to reappear
- 13. determine and correct the cause

## **BELT DATA SHEET**

1. Fiber: Polyester Monofilament

2. Type: 8065

3. Weave: Mod. Satin

4. Weight: 35.25 oz/sq.yd.

5. CFM: 437

6. Mesh Opening in Micros: 47

7. Tensile Strength (Warp): 1130

8. Tensile Strength of seam: 502.8 pli

9. Safety Factor of Belt: (22 @ 50pli)

10. Safety Factor of Seam: (10 @ 50pli)

11. Belt Edge Coating: Acetone Based Plastic Resin

(Heat Sealed)

## Belt Usage Log

Machine Size:	Machine S/N:
Date:	Date:
Belt Number:	Belt Number:
Belt Type:	Belt Type:
Why Replaced:	Why Replaced:
Date:	Date:
Belt Number:	Belt Number:
Belt Type:	Belt Type:
Why Replaced:	Why Replaced:
Date:	Date:
Belt Number:	Belt Number:
Belt Type:	Belt Type:
Why Replaced:	Why Replaced:

## Filter Belt Maintenance As Recommended By Belt Manufacturer

- 1) A Weekly maintenance and cleaning of belts are recommended. This can be done by using 16oz. Of dry detergent that can be purchased in any typical grocery store, and an addition of 16oz. of Clorox bleach to 5 gallons of water.
- 2) A wash down on daily basics of cleat wash water to remove any polymer build-up and debris within the belt.
- 3) A wash down with mild soap can either be applied directly on to the belts or fed into the spray wash system for a period of no less than 1-2 hours.

NOTE: A program of preventive maintenance would be of greater benefit to the end user rather that using a harsh caustic chemical that can bring damage to the belts as well as to the personnel cleaning the presses.

## 10.18 IN-LINE VENTURI MIXER & POLYMER INJECTION RING

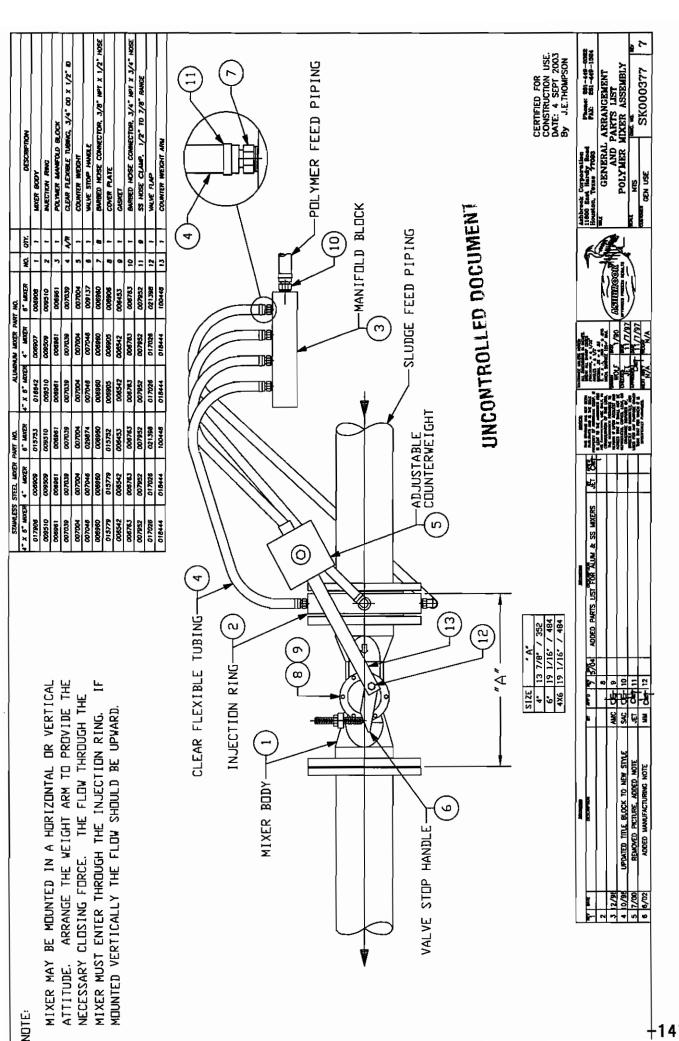
10.18.1 Drawing No. SK000377 Polymer Mixer.
In-Line Mixer with manifold and Injection Ring

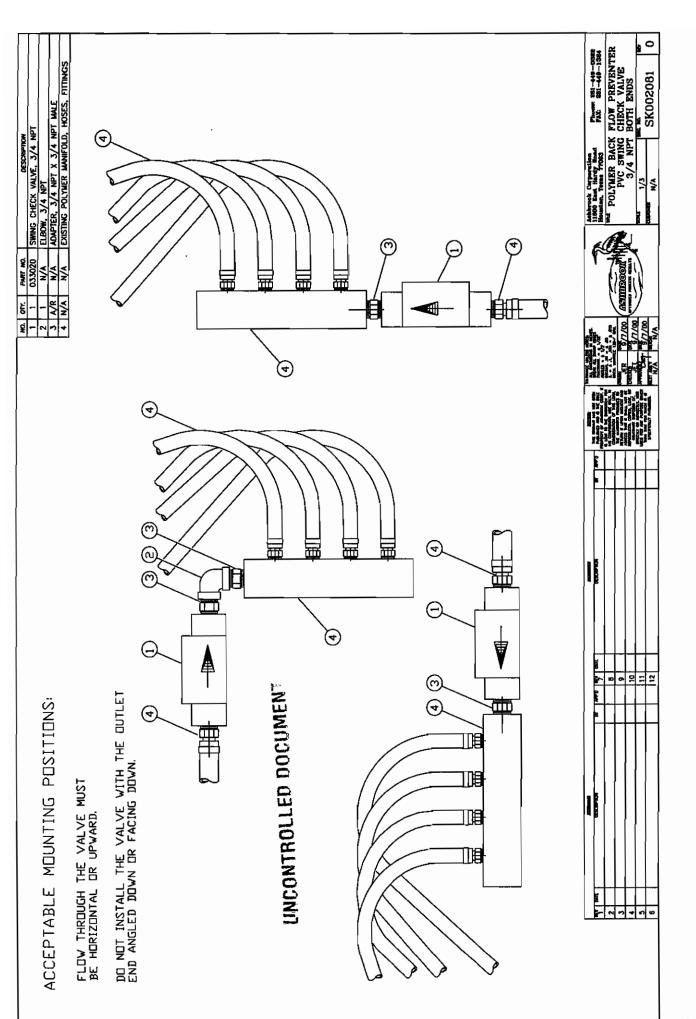
Drawing No. SK002081 Polymer Back Flow Preventer PVC Swing Check Valve to prevent sludge backing up into the polymer system.

## 10.18.2 Mixer Cleaning Procedures:

- a. Remove side plate.
- b. Clean internals.
- c. Replace side plate and tighten bolts.

WP97-10 Rev. 2







## ASHBROOK WINKLEPRESS®

## 11.0 WASHWATER SYSTEM

- 11.1 PRESSURE GAUGE SYSTEM
- 11.2 PRESSURE SWITCH SHEETS
- 11.3 BOOSTER PUMP DATA

## WASHWATER SPRAY SYSTEM DATA

### **SPAN INSTRUMENTS**

## SPAN PRESSURE GAUGE DATA

## 2.5 INDUSTRIAL DIAL RANGES

## **Specifications:**

Case Material Zytel nylon ("Dupont trade-name). ½" blow out plug

Temperature Compensation Internal breathing diaphragm, optional in 2.5". 100 psi

Bezel Material Zytel nylon (optional-316 stainless steel bezel available)

Socket Brass or 316 stainless steel

Bourdon Tube Phosphor bronze: Berylium copper: 316 stainless steel

Accuracy 3-2-3% brass internals. 1% stainless steel internals

Connections 4" NPT male in stem or center back mounts

Fill Fluid Glycerine (silicone available)

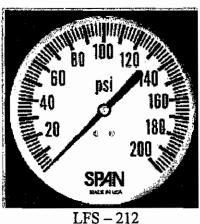
Lens Acrylic

Dial White with black markings

O'Rings Buna-N

Pressure Ranges Vacuum to 10,000 psi

Model Numbers LFS 212 (stainless steel)



INTERVALS 0-15 0-30 10 0-60 0-100 10 0-160 20 0-200 **2**0 25 0-300 0-400 50 0-600 50 0 - 1000100 0-1500 300 0-2000 200 0-3000 500 0-5000 500 0-6000 500 0-10,000 1000

RANGE

STAINLESS INTERNALS

**SMALLEST** 

INTERVAL

.5

1.0

2.0

2.0

2.0

5.0

5.0

10.0

20.0

20.0 25.0

50.0

50.0

100.0

100.0

**FIGURE** 

## WASHWATER SPRAY SYSTEM DATA

## **SPAN INSTRUMENTS**

## SPAN PRESSURE GAUGE DATA

## 'RODUCT INFORMATION

#### Features:

#### **Zyntel Nyion Case**

Tough corrosion resistant, impact resistant, Zytel\* Nylon case (\*Dupont trade name). Resilient and weather resistant.

#### Non-Yellowing Glycerine Fill

Standard fill is non-yellowing, crystal clear glycerine. Special fills available.

#### **Temperature Compensated Case**

No need to vent case to atmosphere by activating a vent screw.

3.5" and 4.5" industrial gauges, and 4.5" process gauges feature
"internal breathing diaphragms", to compensate the case for changes
in internal case pressure build up. Temperature fluctuations cause
the fill fluid to expand and contract. This causes internal pressure
inside the case to build up, as the fill expands and the Bourdon tube
senses this internal case pressure, unless the case is compensated for
these changes. SPAN's "breathing diaphragm" compensates for internal
case pressure build up to over 150°F, which allows the gauge to stay fully
accurate.

#### **Unrestricted Blow-Out Hole**

One half inch, unrestricted blow out plug in all industrial models, and a low out back in our process gauges give added safety protection.

#### No Air Bubble

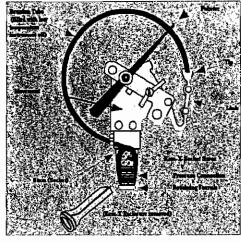
SPAN's internal "breathing diaphragm" eliminates the need for an air bubble in the mid-range of the gauge, which could distort reading the gauge from a distance.

#### Specials

Special dials, customer logos, stainless steel bezels, and special manufactured instrumentation available.

#### Variety of Connections

All models available in stem, center back, or panel mountings.

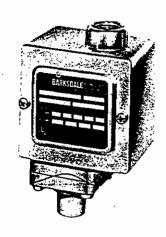


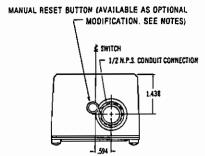
General Advautage of Liquid Filled Gauges:	a. Stops corrosion b. Solves pulsation and vibration wear on gauges. c. Weather tight-no condensation. d. Lengthens gauge life. e. Lubricates internals.
Liquid Filled Applications:	<ul> <li>High pressure washers.</li> <li>Steam cleaning equipment.</li> <li>Chemical plants &amp; refineries.</li> <li>Agriculture equipment.</li> <li>Car wash systems.</li> <li>Oil field equipment.</li> <li>Shipboard applications.</li> <li>Hydraulic equipment.</li> </ul>
Temperature Ranges:	General: Liquid filled gauges are generally rated to 150°F. At that point, internal case pressure build up due to expansion of the fill as temperature increases, causes loss of accuracy. Also, the lens and O Ring seals are limited to 175. Case: Zytel: High temperature stabilized. Fill Fluid: Glycerine – +150°F to +20°F. Silicone - +150°F to -40°F. Seals: Buna N - +150 °F to -40°F. Lens: Acrylic - +150°F to -40°F.
Guarantee:	SPAN INSTRUMENTS, INC warrants products free from defects in material and workmanship under normal use and service for one year from date of delivery. All equipment requiring repair or replacement under this warranty, shall be returned to us at our factory or at such other location, as we may determine, transportation prepaid. This warranty shall not apply to any equipment which has been tampered with or altered after leaving our control, or which has been subject to misuse, neglect, abuse, or improper use.
Warning:	Misuse of this product may cause explosion and personal injury. Read ANSI-B40.1 and apparatus installation operating instructions before using.  Glycerine can combine with strong oxidizing agents including (but not limited to) chlorine, nitric acid, and hydrogen peroxide, and result in an explosion, which can cause property damage and personal injury. Consult factory for proper filling medium in hazardous service.

# PRESSURE SWITCH PIN (LOW-WATER) 009272

**ECON-O-TROL Dia-Seal Piston Models** Water-Tight Housing (NEMA 4)

**PRESSURE SWITCHES EIH Single Setting VACUUM SWITCHES** E1H-H-VAC Single Setting

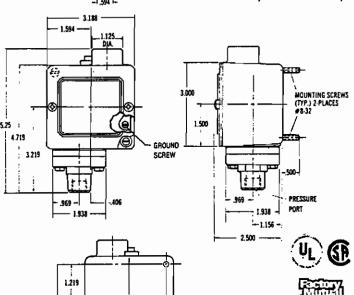




2,438

MOUNTING SCREWS

(TYP.) 2-PLACES



BARKSDALE, INC. • 3211 Fruitland Avenue, P.O. Box 58843 • Los Angeles, CA 90058 • (213) 589-6181

### **OPERATING CHARACTERISTICS • ORDERING DATA**

#### PRESSURE SWITCHES — All values given in P.S.I. (Gauge)

Proof		Adjustabl	le Range		Approx.* Actuation Value	Catalog Number	Catalog Number	
(Test)	Decre	asing Inc		Decreasing		asing	1/4" npt Internal	1/8" npt Interna
Press	Min.	Max.	Min.	Max.	(Differential)	(No Ext. Thread)	1/2" npt External	
1000	.5	14.2	.6	15.0	.1 to .8	E1H-H15	E1H-H15-P6†	
1000	3.0	82.0	3.5	90.0	.5 to 8.0	E1H-H90	E1H-H90-P6†	
1000	10.0	230.0	11.0	250.0	1.0 to 20.0	E1H-H250	E1H-H250-P6†	
1000	25.0	472.0	29.0	500.0	4.0 to 28.0	E1H-H500	E1H-H500-P6	
Approximate shipping weight lbs.						1.5	1.5	

<sup>\*</sup>Fixed at any pressure setting, varies as shown from lowest to highest setting.

#### VACUUM SWITCHES — All values given in inches of mercury (Gauge)

Proof	Proof	Ĺ	Adjustab	le Range		Approx.*	Catalog Number	
(Test)	(Test)	Decre	Decreasing		Decreasing Increasing		Actuation Value	1/2" npt Internal &
Vacuum	Press	Min.	Max.	Min.	Max.	(Differential)	1/2" npt Ext. Thread	
30	30 PSI	,5	29.0	2.2	30.0	.3 to 1.7	E1H-H-VAC-P6	
Approxi	Approximate shipping weight lbs.							

<sup>\*</sup>Actuation value depends on Actuation Point (Set Point), Maximum actuation value is at .5 inches HG Set Point. Minimum actuation value is at 30 inches HG Set Point.

Models listed have aluminum fittings and Buna "N" diaphragms. Aluminum fittings are not recommended for water service. Use Polysulfone fittings, suffix -PLS, or Nickel Plated fittings, suffix -F2.

#### **DETAIL DATA**

ELECTRICAL CHARACTERISTICS (Pressure and Vacuum Switches): All models incorporate Underwriters' Laboratories, Inc. listed single pole double throw snap-action switching elements. Electrical rating (continuous inductive) 10 amps 125 or 250 volts AC, 3 amps 480 volts AC. Automatically reset by snap-action of switch.

ELECTRICAL CONNECTION (Pressure and Vacuum Switches): Through 1/2" NPS Conduit Connection to screw terminals on switch. May be wired Normally Open or Normally Closed.

PRESSURE CONNECTION: 1/4" npt internal thread, standard. 1/4" npt internal and 1/2" npt external thread, -P6 option.

VACUUM CONNECTION: 1/4" npt internal and 1/2" npt external thread, standard.

ADJUSTMENT INSTRUCTIONS (Pressure): Turn self locking adjustment nut clockwise to raise and counterclockwise to lower the actuation point. All dials are calibrated for increasing settings.

ADJUSTMENT INSTRUCTIONS (Vacuum): Turn self locking adjustment nut counterclockwise to adjust the actuation point toward 30 inches HG. All dials are calibrated for increasing settings.

#### OPTIONAL MODIFICATIONS (Pressure Switches)

Diaphragms: These models can be supplied with Viton or Teflon diaphragms to special order. To specify add suffix -V or -T to switch number and consult plant for delivery.

Polysulfone 40% glass filled pressure fitting with 1/8" NPT internal connection and 1/2" NPT external connection. Proof pressure 400 P.S.I. Add suffix -PLS to tabled units with †. For higher pressures consult factory.

Nickel plated fitting for water service. Add suffix -F2.

Brass fitting, add suffix -BR (Not available on vacuum)

Manual Reset. Actuates automatically at set point on pressure increase. Must be reset manually after pressure decreases. To specify, change electrical letter to 'G' and add suffix -RD to catalog number. Example: EIH-G250-RD

All models shown are Underwriters' Laboratories listed in the Electrical Construction Materials Directory under Industrial Control Equipment, Float and Pressure Operated (NKPZ), File E42816, and Canadian Standards Association listed under Guide 380-W-1.16, Class 3231, File 22355.

Catalog numbers E1H-B15, B90, B250-P6-PLS-U and E1H-M15, M90, M250-P6-PLS-U are listed in the Factory Mutual Approved Guide under Waterflow Alarm Switches.



## ASHBROOK WINKLEPRESS®

## 12.0 ELECTRICAL COMPONENTS

## 12.1 TRIP CORD DATA

## SAFETY PULL SWITCH, RAMSEY MODEL SPS-2D-3-NP

The safety pull switch shall be CSA approved for Class II, Divisions 1 and 2, Groups E,F and applications. The safety pull switch enclosed in aluminum NEMAA-4X weatherproof enclosure. Force applied to the pull cable at any position shall cause the actuating arm to rotate 20 degrees to a trip locked position. Pull rating shall be 8-18 pounds. A spring-loaded dog holds a cam detent in this position until manually reset. The safety pull switch shall meet OSHA requirements for safety shutdown.

## SAFETY PULL SWITCH, RAMSEY MODEL SPS-2-3-FM

The safety pull switch shall be CSA approved for Class II Divisions 1 and 2, Groups E, F and G applications. The safety pull switch shall contain 2 SPDT, 10A, 480V switch enclosed in an aluminum NEMA-4X weatherproof enclosure. Force applied to the pull cable at any position shall cause the actuating arm to rotate 20 degrees to a triple-locked position. Pull rating shall be 8-18 pounds. A spring loaded dog holds a cam detent in this position until manually reset. The safety pull switch shall meet OSHA requirements for safety shutdown.

### 12.2 BELT BREAKAGE SWITCH

Each belt is fitted with a proximity switch to sense extreme travel of the tensioning arm. If one of the belts should break the tension cylinders will extend the tensioning arm to the limits of its travel where it will contact the belt breakage limit switch.

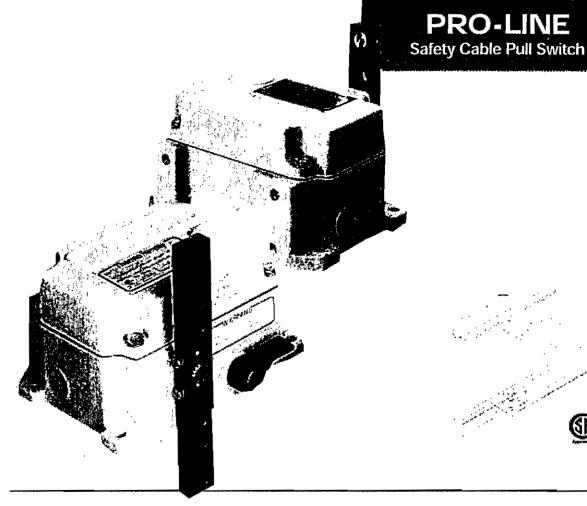
#### 12.3 BELT MISALIGNMENT SWITCH

There are two limit switches mounted inside the frame alongside the pressure rollers. If either belt wanders too close to the end of the pressure rollers it will trip the limit switch. Under no circumstance should you operate the press with these limit switches disabled. These switches are provided to avoid unnecessary damage to the belts in case the automatic belt tracking system cannot maintain the belts centered on the rollers.

WP84-12Rev.1

## **Emergency or Normal Shut-Off Control for Safer Operation**

## Ramsey





## SAFETY CABLE PULL SWITCH (S.P.S.)

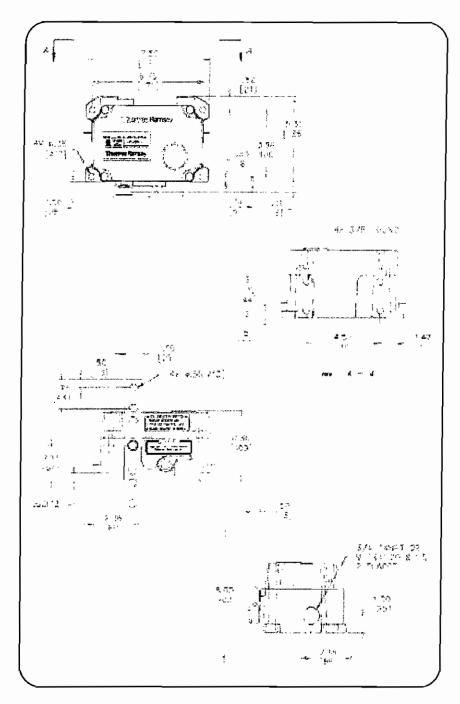
#### For Emergency or Normal Shut-Off

- Universal design for bi-directional activation allows one unit to be used for end or middle locations.
- · Universal mounting design allows for either top or side mounting of the switch to the conveyor stringers.
- · Rugged cast aluminum enclosure with standard NEMA-4 clear iridite finish or optional two-part baked urethane enamel finish for salty, alkaline, or acidic atmospheres. Also, electroless nickel finish optional for extremely corrosive environments.
- · Full cover plate permits easy access to terminals and switches without deactivating or disassembling switch.
- · Compact design for tight-fit areas.
- Highly visible black arm against silver or yellow background easily shows condition of the switch, indicating alarm or normal.
- · Complete accessories available including cable, standoff eyes and cable clamps.
- Stocked by local distributors for immediate delivery.
- Manual reset lever.
- CSA approved Class II models available, along with barriers for Class I areas.
- Optional red flags available for notification of alarm condition.

A pull cable is terminated at one end from a fixed mounting and attached at the switch end to one of the actuating arm holes. Force applied to the pull cable at any position causes the actuating arm to rotate 20° to a tripped-locked position. This will stay locked until manually reset by the reset lever.

At the same time as the switch is mechancally locked out, 2 microswitches activate SPDT circuits for alarming equipment circuits of the stop condition. Although the black arm in the alarm condition is quite visible, accessories such as auxiliary flags or lights can be supplied. Also available are specially designed mounting hardware, which can eliminate welding or drilling holes in the conveyor for mounting.

## **DIMENSIONS**



#### **SPECIFICATIONS**

- · 2 Switch rating SPDT 10A 480V
- NEMA-4 weatherproof enclosure
- Lock angle 20 degrees
- Pull rating 8 18 pounds
- Two or three conduit openings, threaded 3/4" - 14 NPT
- Recommended spacing between switches: 200 ft. with factory size cable and supports every 10 feet
- Meets OSHA requirements for safety shutdown
- CSA approved models for Class II Division 1 & 2, Group E,F, & G

### **APPLICATIONS**

#### Emergency or Normal Stop for:

- Conventional belt conveyors
- · Shuttle conveyors
- · Apron feeders & conveyors
- · Bucket elevators
- · Packaging lines
- Stockpile/reclaim systems, cranes, shovels and drag-lines
- · Ship loading/unloading systems
- · Horizontal feed systems

#### OPTIONS

- · Universal mounting plate
- · Secondary flag alarm
- Complete hook-up accessories including: cable, clamps, standoffs and lights
- · Optional finishes include:
  - Double baked urethane enamel
  - Electroless nickel
- · NEMA-4 and NEMA-9 Alarm Light
- European tension spring-loaded mounting hardware

#### Models Available

- Standard NEMA-4 SPS-2D Dual Switch
- Class II CSA Approved SPS-2D-3 Dual Switch SPS-2D-3-NP Dual Switch Nickel Plated (NEMA-4X)

## Thermo Ramsey

501 90th Avenue N.W. Minneapolis, MN 55433 (763) 783-2500 FAX: (763) 783-2525 www.thermoramsey.com



Australia Canada Germany Italy

Mexico South Africa Spain

The Netherlands United Kingdom



## TABLE OF CONTENTS

- 1.0 Safety Pull Switch
- 2.0 Inspection and Installation
- 3.0 Theory of Operation
- 4.0 Set-up and Adjustment
- 5.0 Troubleshooting
- 6.0 Maintenance, Spares, and Repairs

## Safety Pull Switch

## 1.1 Introduction

` . **:**:

. .

The Safety Pull Switch actuates when a force is applied to a pull cable at any position causing the actuator arm to rotate 20° to a "tripped locked" position. The switch stays in locked position until manually reset.

## 1.2 Specifications

- (1) Switch rating SPDT, 15 amp, 480 volts
- (2) Terminal board rating: 1000 volts
- (3) NEMA 4 weatherproof enclosure
- (4) Lock angle: 20 degrees
- (5) Pull rating: 12 to 25 lbs.
- (6) Three conduit opening, threaded 3/4" -14 NPT
- (7) Recommended spacing between switches: 150 ft support cable

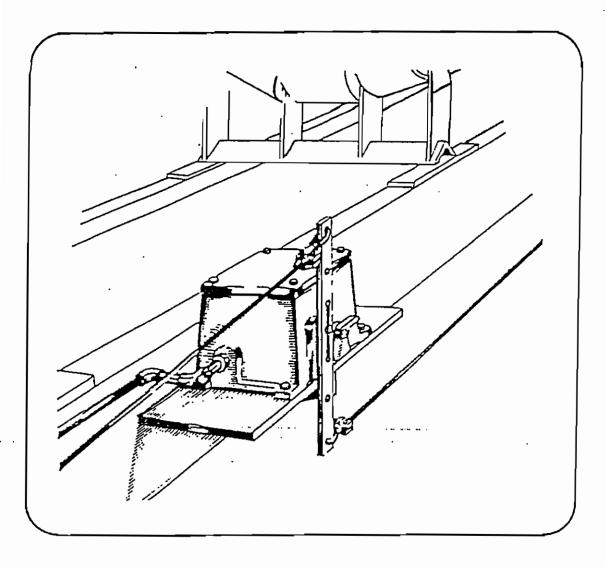


Figure 1-1 Safety Pull Switch

## Inspection and Installation

## 2.1 Inspection

Inspect the package for external damage before opening, as often times the carrier can be held responsible for shipping damages. After unpacking, inspect the unit for damaged parts, etc.

## 2.2 Installation

Refer to Figure 2-1 for installation methods.

NOTE: Cable should have sufficient play to allow switch to operate in two directions.

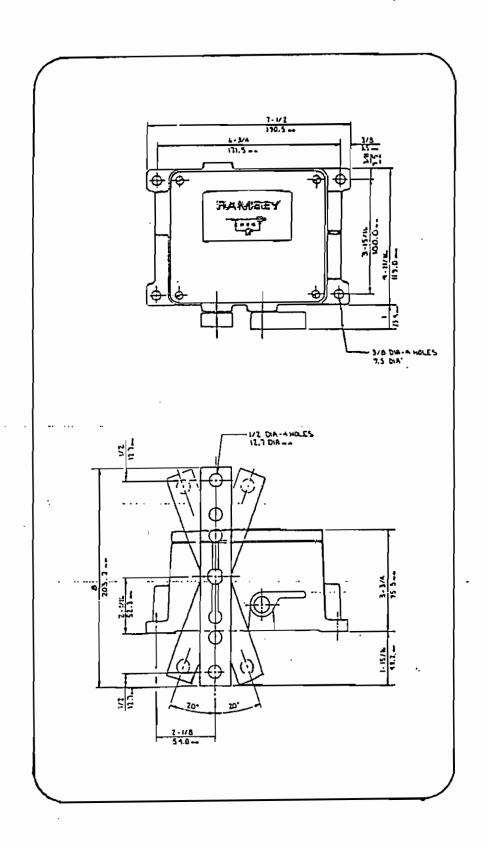


Figure 2-1 Mounting

## 2.3 Installation - Electrical

- (1) Each switch is supplied with three (3) 3/4" -14 NPT openings for conduit connections.
- (2) One Switch Figure 2-2 shows the terminal connections used in wiring a one switch unit. One switch units are used for belt shutdown.
- (3) Two Switch Figure 2-3 shows the terminal connections used in wiring a two switch unit. Two switch units are used for belt shutdown and alarm.

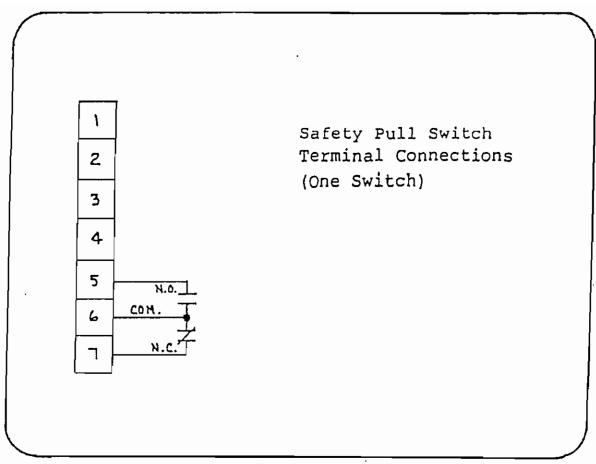


Figure 2-2

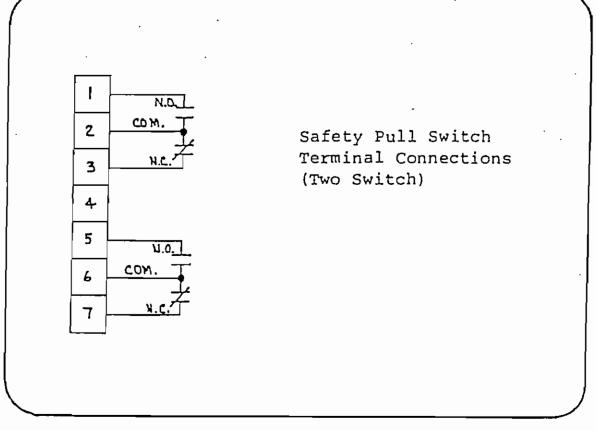


Figure 2-3

## Theory of Operation

## 3.1 General

Refer to Figure 2-1 while reading the following description.

## 3.2 Operation

The Safety Pull Switch must be mounted alongside the conveyor stringer. A pull cable is firmly fixed at one end and attached to the actuator arm of the Safety Pull Switch on the other end. This cable must have some play in it to ensure the switch will operate properly when cables are extended in opposite direction from the switch actuator arm.

When a force is applied in any position along the cable, the actuator will rotate 20°, then "tripped-locked" into position. A spring-loaded dog holds lever in detent position until actuating arm is manually reset.

At the time the arm is tripped, a microswitch is actuated which provides a SPDT circuit to interrupt the drive, thus stopping the conveyor. On units with two (2) microswitches, the conveyor would stop and an alarm would be actuated.

To reset Safety Pull Switch, the reset lever must be depressed, thus placing the actuator arm in to operating position.

## Set-Up and Adjustment

## 4.1 Set-Up

- (1) The recommended spacing between switches should not exceed 150 feet.
- (2) Cable lengths, if tied off at one end, should not exceed 75 feet.
  - (3) Eye bolts to support the cable should be spaced at 8 feet apart.
  - (4) Safety Pull Switch is to be mounted alongside conveyor stringer.
  - (5) Electrical hook-up should be completed as shown in Chapter 2.

## 4.2 Adjustment

All necessary adjustments are made at the factory. The unit does not require field adjustment.

## Troubleshooting

### 5.1 General

The Safety Pull Switch has been designed to operate under industrial environment with no mechanical maintenance.

## 5.2 Troubleshooting Procedure

- (1) Check actuator lever to make sure it is in the normal position.
- (2) Check to see if terminal wires are connected properly and terminal screws are tight.
- (3) Check to see if microswitch cams are not actuating microswitch arm. If so, reset cams.
- (4) If the above checks out all right, the problem is not with Safety Pull Switch.

## Maintenance, Spares, and Repairs

## 6.1 General

Except for the parts replacements mentioned below, Ramsey recommends that repairs not be attempted on this unit. Unauthorized repairs during the warranty period will void the warranty.

## 6.2 Recommended Spares

(1) Microswitch: Ramsey Part No. 3680

## **BELT BREAKAGE SWITCH / Lake of Cake Switch**

S Barrel

## **Barrel, Plastic with Potted-In Cable**Partial Threading

**Turk Inductive** 



2-Wire AC (SCR Output)



20-250 VAC

Normally Closed (N.C.), Normally Open (N.O.)



## **Sensor Selection**

And to Shapping Care Cordsets  View/Pent Q-Pak Specification Page Q-Pak Show All Similar Products	Footnotes	Rated Operating Distance	Barrel Diameter (mm)	of LEDs	Embeddable	Mormally Open	Mormally Closed	CSA Certification	Switching Frequency Hz	Number	Connection
Part Number	0	5	80	: <b>%</b>	: <u>ह</u>	Z ·	E C	ປ	ŝ	2	8 _
Bi 5-S18-AZ3X		5	18	1		•			20	T4350400	potted cable
Bi 5-S18-AZ3X/S100	*	5	18	1	•	•			20	M1373400	potted cable
Bi10-S30-AZ3X		10	30	1	•	•		•	20	T4355400	potted cable
Bi10-530-AZ3X/S100	*	10	30	1	•	•			20	M1371900	potted cable
Ni 8-S18-AZ3X	FR 1 10	8	18	1		•		•	20	T4350500	potted cable
Ni 8-S18-AZ3X/S100	*	8	18	1		•			20	M1371800	potted cable
Ni15-S30-AZ3X		15	30	1		•	:	•	20	T4355500	potted cable
Ni15-S30-AZ3X/S100	*	15	30	1	. :	•	'		20	M1375800	potted cable
Bi 5-S18-RZ3X		5	18	1	•		•	•	20 .	T4350600	potted cable
Bi 5-S18-RZ3X/S100	*	5	18	' 1 ,	•	:	•		20	M1376000	potted cable
Bi10-530-RZ3X		10	30	1	•		•	•	20	T4355600	potted cable
Bi10-S30-RZ3X/S100	*	10	30	1	•		•			M1371300	potted cable
Ni 8-S18-RZ3X	THE RESERVE OF SECTION		18		g Fa <b>dd</b> ifferede fo	THE THE PERSON AND PERSON	•	•		T4350700	potted cable
Ni15-S30-RZ3X			30			vener-re phe die				T4355700	

\* These sensors will operate up to 100°C (212°F).

#### Material

Barrel: PA 12-GF30 Plastic

End Cap: PUR Plastic

Cable/Conductor

Cable: PVC Jacket; 2 and 7 Meter standard length

PVC Jacket; 2 Meter standard for S100 style

Copper Conductor: 21 AWG

(PVC insulated)

Specifications

Line Frequency 40-60 Hz

Differential Travel (Hysteresis) 3-15% (5% typical)

Voltage Drop Across Conducting Sensor <=7.0 V at 500 mA (100 mA for S100 style)

Continuous Load Current <=500 mA (100 mA for S100 style)

Leakage (Off-State) Current <=1.7 mA
Minimum Load Current >=5.0 mA

Inrush Current <=8.0 A (<=10 ms, 5% Duty Cycle)

Time Delay Before Availability <=25 ms

Power-On Effect Per IEC 947-5-2

Transient Protection 5 kV, 10 ms, 10 kOhms

Operating Temperature -25°C to +70°C (-13°F to +158°F)

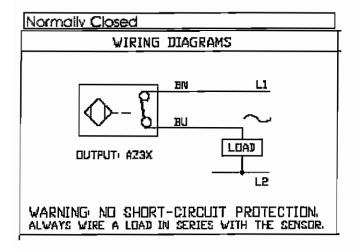
Enclosure Meets NEMA 1,3,4,4X,6,13 and IEC IP 67

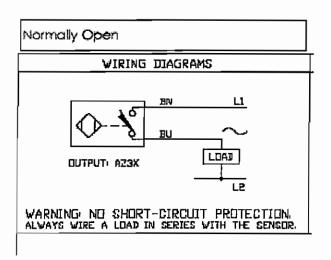
Shock 30 g, 11 ms

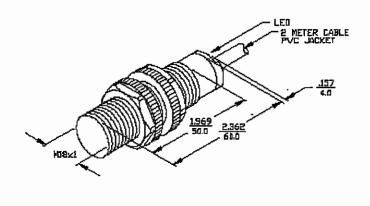
Vibration 55 Hz, 1 mm Amplitude in all 3 Planes
Repeatability <=2% of Rated Operating Distance

LED On Output Energized

## Wiring Diagrams







Boletin de Directives instrucciones d'utilisation



60083-760-01A Raleigh, NC, USA 8/97

#### Replaces / Reemplaza / Remplace 60083-760-01 4/93

## Miniature Limit Switches Interruptores de límite miniatura Interrupteurs de position miniaturisés

Class	Type
Clase	Tipo
Classe	Type
9007	MS/MI

#### **DESCRIPTION**

Type MS/ML miniature switches provide environmental sealing for very small enclosed switches. Factory prewiring with industrial grade cable (type SJTOW-A) eliminates the need to remove the cover to wire the switch. Cables connect by either the bottom or side entrance. An epoxy compound provides excellent sealing for encapsulation of the electrical cable connections and switch housing. Plunger sealing keeps liquids from entering the switch cavity. Housings are rugged zinc (die cast) construction.

### **DESCRIPCION**

Los interruptores miniatura tipo MS/ML proporcionan un cierre hermético ambiental a los interruptores pequeños en gabinete. El precableado de fábrica (con cable industrial tipo SJTOW-A) elimina la necesidad de retirar el frente para conectar el interruptor. La conexión de los cables se realiza por la entrada inferior o lateral. La encapsulación de epoxia proporciona un excelente cierre hermético a las conexiones eléctricas y a la caja del interruptor. El cierre hermético del pulsador evita la penetración de líquidos en la cavidad del interruptor. Las cajas son robustas construidas de troquelado de zinc.

#### **DESCRIPTION**

Les interrupteurs miniaturisés de type MS/ML fournissent l'étanchéité de l'environnement pour les très petits interrupteurs sous coffret. Le pré-câblage à l'usine utilisant un câble de qualité industrielle (type SJTOW-A) élimine le besoin d'enlever le couvercle pour câbler l'interrupteur. Les câbles se raccordent par l'ouverture du fond ou latérale. Un époxyde fournit une excellente étanchéité pour l'enrobage des connexions électriques de câble et du boîtier de l'interrupteur. L'étanchéité du poussoir empêche les liquides de pénétrer dans la cavité de l'interrupteur. Les boîtiers sont en zinc renforcé (moulés en coquille).

Table / Tabla / Tableau 1 Electrical Ratings / SPDT Form C (MS Type) / Especificaciones eléctricas/1P2T forma C (tipo MS) / Valeurs nominales électriques/UPBD forme C (type MS)

Circuit/Circuito/Circuit	Electrical Ratings/Especificaciones eléctricas/Valeurs nominales électriques						
Circulo Circulto Circult	Silver Cor	Gold Contacts/Contactos					
1 N.O. / 1 N. C. // 1 NA / 1 NC // 1 NO / 1 NF	Volts	Make/Cierre/Fermeture	Break/Apertura/ Ouverture	dorados/Contacts en or			
	120 AC /- / CA	60 A	6 A	100 mA; 125 VAC/100 mA;			
Black/Negro/ White/Blanco/	240 AC / ~ / CA	30 A	3 A	125 V~/100 mA; 125 VCA			
Green/ Red/Rojo/	10 A Continuous/	30 mA; 28 VDC/30 mA; 28 V /30 mA; 28 VCC					
Verde/ Rouge	DC Contact Rating 5 A (res); 28 V						

Table / Tabla / Tableau 2 Electrical Ratings / SPDT-DB Form Z (ML Type) / Especificaciones eléctricas/1P2T- doble apertura forma Z (tipo ML) / Valeurs nominales électriques/UPBD-double coupure, forme Z (type ML)

Circuit/Circuito/Circuit	Electrical Ratings/Es	Electrical Ratings/Especificaciones eléctricas/Valeurs nominales électriques					
Circuiv Circuito/Circuit	Silver Contacts/Contactos plateados/Contacts en argent						
1 N.O. / 1 N. C. // 1 NA / 1 NC // 1 NO / 1 NF	Volts	Make/Cierre/Fermeture	Break/Apertura/Ouverture				
10 A 125/150 Vac/~/CA	120 AC /- / CA	60 A	6 A				
	240 AC / ~ / CA	30 A	3 A				
Red/Rojo/ Rouge White/Blanco/Blanc Green/Verde/Vert	10 A Continuous / 10 A contin	nuos / 10 A continus					
Black/Negro/ Orange/ Anaranjado/Orange	DC Contact Rating: 5 A (Res) Valeur nominale du contact C	); 28 VDC/Capacidad de los conta C : 5 A (Rés); 28 VCC	ctos de:5 A (res); 28 V /				

NOTE: Devices with Micro Connector (option 54 and 55) have 3 A continuous current rating; those with Mini Connector (option 12) have 10 A continuous current rating. Enclosure ratings are NEMA 1, 2, 3, 4, 6, 6P, 12, and 13 except for: option 21, a low-force operator, which is NEMA 1 only; and MS05, an omnidirectional operator, which is NEMA 1, 2, 12, and 13.

NOTA: Los dispositivos con microconectores (opciones 54 y 55) tienen una capacidad de corriente continua de 3 A; los miniconectores (opción 12) tienen una capacidad de corriente continua de 10 A. Los interruptores vienen en gabinetes NEMA 1, 2, 3, 4, 6, 6P, 12 y 13; excepto la opción 21 (un operador de baja fuerza) que viene en un gabinete NEMA 1 solamente; y el interruptor MS05 (un operador omnidireccional) que viene en gabinetes NEMA 1, 2, 12 y 13.

REMARQUE: Les dispositifs á micro connecteur (options 54 et 55) ont un courant continu nominal de 3 A; ceux avec mini connecteur (option 12) ont un courant continu nominal de 10 Å. Les valeurs nominales du coffret sont NEMA 1, 2, 3, 4, 6, 6P, 12 et 13 sauf pour: l'option 21, un opérateur à force faible qui est seulement NEMA 1; et MSO5, un opérateur omnidirectionnel qui est NEMA 1, 2, 12 et 13.



SQUARE D

#### APPLICATION GUIDE

#### **Polarity**

Opposite polarities should not be connected to the contact of one limit switch unless the limit switch is specifically designed for such service.

#### **Power Sources**

Do not connect power from different sources to the contacts of one limit switch unless the switch is specifically designed for such service.

#### **GUIA DE APLICACION**

#### Polaridad

Las polaridades opuestas no deben conectarse al contacto de un interruptor de límite a menos que éste esté específicamente diseñado para este propósito.

#### Fuentes de alimentación

No utilice diferente fuentes de alimentación para alimentar los contactos de un interruptor de límite a menos que el interruptor esté específicamente diseñado para este propósito.

#### **GUIDE D'APPLICATION**

#### Polarité

Les polarités opposées ne doivent pas être connectées au contact d'un interrupteur de position sauf si ce dernier est spécialement conçu pour cette application.

#### Sources d'alimentation

Ne pas connecter des alimentations de sources différentes aux contacts d'un interrupteur de position sauf si l'interrupteur est spécialement conçu pour cette application.

## DANGER / PELIGRO / DANGER

#### **HAZARDOUS VOLTAGE**

- Disconnect power before performing any work on the device.
- · Ground switch properly.

Failure to follow this instruction will result in death or serious injury.

#### **TENSION PELIGROSA**

- Desenergice el equipo antes de realizar cualquier trabajo a éste.
- · Aterrice el interruptor correctamente.

El incumplimiento de estas precauciones podrá causar la muerte o lesiones serias.

#### **TENSION DANGEUREUSE**

- Coupez l'alimentation à l'appareil avant d'y travailler.
- L'interrupteur doit étre adéquatement mis à la terre.

Si ces précautions ne sont pas respectées, cela entraînera la mort ou des blessures graves.

#### **PLUNGER ACTUATORS**

For limit switches with plunger actuators, the actuating force should be applied in line with the plunger axis.

#### **ACCIONADORES PULSADORES**

La fuerza de accionamiento en los interruptores de límite con accionadores pulsadores deberá aplicarse en línea con el eje del pulsador.

#### **ACTIONNEURS DU POUSSOIR**

Pour les interrupteurs de position équipés d'actionneurs du poussoir, la force d'actionnement doit être appliquée le long de l'axe du poussoir.

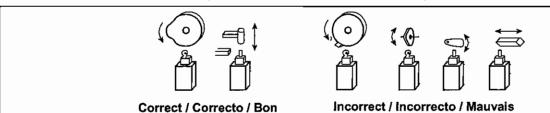


Figure / Figura / Figure 1 Plunger Actuators / Accionadores pulsadores / Actionneurs du poussoir

#### **Dwelling Requirements**

When cam motions are too fast or rise on the cam is too small, the limit switch will not function long enough to operate relays, valves, and other necessary components. Make sure the cams are designed so that the limit switch will operate properly.

#### Requisitos de paro

Cuando los movimientos de la leva son demasiado rápidos o la elevación de la leva es muy baja, el interruptor de límite no funcionará lo necesario para hacer funcionar los relevadores, las válvulas y otros componentes necesarios.

Asegúrese de que las levas estén diseñadas para que el interruptor de límite funcione correctamente.

#### Exigences de repos

Lorsque les mouvements de came sont trop rapides ou lorsque l'élévation de la came est trop petite, l'interrupteur de position ne fonctionne pas assez longtemps pour actionner les relais, les soupapes et autres composantes nécessaires. S'assurer que les cames sont conçues de façon à ce que l'interrupteur de position fonctionne convenablement.

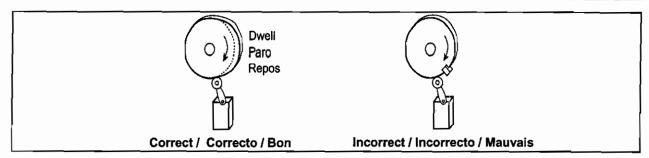


Figure / Figura / Figure 2 Dwelling Requirements / Requisitos de paro / Exigences de repos

#### **Overtravel Limitations**

Design operating mechanisms for limit switches so that no operating or emergency conditions will make the limit switch operate beyond its overtravel limit position. Do not use a limit switch as a mechanical stop.

#### Restricciones de sobrerrecorrido

El diseño de los mecanismos de funcionamiento para los interruptores de límite debe ser tal que las condiciones de paro o emergencia hagan funcionar el interruptor más allá de su posición de límite de sobrerrecorrido. No utilice un interruptor de límite como un tope mecánico.

#### Limites de course

Il faut concevoir les mécanismes de fonctionnement des interrupteurs de position de sorte qu'aucune condition de fonctionnement ou d'urgence ne force l'interrupteur de position à fonctionner au-delà de sa position limite de course. Ne pas utiliser un interrupteur de position comme arrêt mécanique.

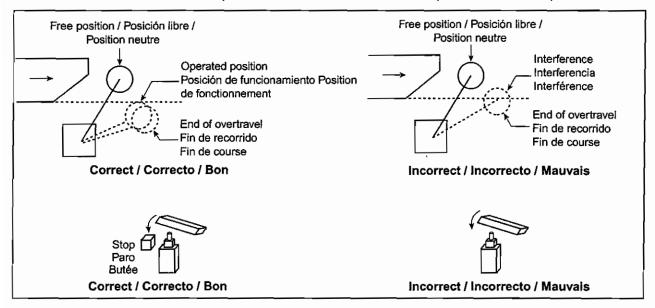


Figure / Figura / Figure 3 Overtravel Limitations / Restricciones de sobrerrecorrido / Limites de course

#### **Control Fusing**

These units comply with IEC 947.5.1, SC 8.3.4 when protected with a Bussman CC KTK-R-10 (10 A) fuse.

#### **Rotary Levers**

Make sure the rotary lever attachment screw is torqued to 27 lb-in/min.

#### Fusibles de control

Estas unidades cumplen con la norma IEC 947.5.1, SC 8.3.4 cuando están protegidos con un fusible CC KTK-R-10 Bussman de 10 A.

#### Palancas giratorias

Asegúrese de que el tornillo del aditamento de la palanca giratoria esté apretado a 3,05 N·m (27 lbs-pulg) como mínimo.

#### Fusibles de contrôle

Ces unités satisfont à la norme IEC 947.5.1, SC 8.3.4 lorsqu'elles sont protégées par un fusible Bussman CC KTK-R-10 (10 A).

#### Leviers rotatifs

S'assurer que la vis d'attache du levier rotatif est serrée à un couple de 3,05 N·m (27 lb-po) au minimum.

## Square D www.SquareD.com FOR CURRENT INFORMATION

## **General Specifications and Selection**

Class 9007—Type MS/ML Miniature

## **Belt Misalignment**

The heavy duty completely encapsulated miniature MS limit switch is intended for difficult applications such as machine tools, earth moving equipment, general transportation, etc. (The switch has 40 mm mtg hole centers.)



General Specifications				
-40°F to +221°F (-40°C to +105°C) The minimum temperatures listed are based of the absence of freezing moisture or water				
Enclosure rating	NEMA Type 1,2,4,6,6P,12,13, IP 67			
Vibration resistance	10G (75–1200 Hz)			
Shock resistance	35G			

Contact Characteristics					
Rated thermal current	10 A (standard)				
Rated insulation voltage	300 Vac and dc (standard)				
Gold contact switching ratings	.1A, 24 Vdc; .24 VA				
Cable	#18 AWG SJTO				

	Electrical Ratings/SPDT Form C (MS Type)							
MS Circuit - Form C	sı	Gold Contacts						
1 N.O1 N.C.	Volts	Make	Break					
	120 ac	60 A	6 A	100 mA @				
BLK OF TOTO WHT.	240 ac	30 A	. 3A	125 Vac 30 mA				
GRN OF RED	10.0 Ar	28 VDC						
=	DC Contact F							

ML Circuit - Form Z	Electrical Ratings/SPDT-DB Form Z (ML Type)					
	Silver Contacts					
1 N.O1 N.C.	Volts Make Break					
	120 ac	60 A	6 A			
	240 ac	30 A	3 A			
RED OF TO OF DRG E	10.0 Amperes, Continuous					
BLK. OLO OF ORG.	DC Contact Rating: 5 A (Res). 28 Vdc					

	1		1	<u> </u>	1	1	
Description / Functiona Diagram	MS	ML	Operating Force/Torque	Contact Form	Contact Type	Catalog Number ▲	List Prio
op plunger						-	
	.070" max.	.080° max.	8080 oz	SPDT Form C	Silver	MS01S0100	\$ 57.
	Bk-Pid	fla-W Bk-Rd	80 oz	SPDT Form C	Gold	MS01G0100	63.
	0 (GO1*)-4 .19* max. min.	0 3.03° jei .19° mex. min.	80 oz	SPDT Form Z	Silver	ML01S0100	79.
arallel roller plunger							
	.070" max.	,080" max	80 oz	SPDT Form C	Silver	MS02S0100	66.
	Bk-W Bk-Rd	Bh-W Bh-Md	60 oz	SPOT Form C	Gold	MS02G0100	73.
	0 1004" -s .19" max. min.	0   .03" → .19" #962. Min.	80 oz	SPDT Form Z	Silver	ML02S0100	88.
ross roller plunger							
ďЪ	.070° max.	.xara *060. →≪ DH-Hd	80 oz	SPDT Form C	Silver	MS03S0100	66.
dh —	Bk-Pid	BL-W BL-Pd	80 oz	SPDT Form C	Gold	MS03G0100	73
	0 10047 19"	0 1:02, Pr 12.	80 oz	SPDT Form Z	Silver	ML03S0100	88
stary lever, CW and CCV	<u></u>						
$\bigcirc$	35* Bk-Rd	40°	48 in oz	SPDT Form C	Silver	MS04S0100	83
(00)	Br. Rd Br. W Sr. Rd	Bh-M Sh-Ro Bk-W	48 in oz	SPDT Form C	Gold	MS04G0100	90.
	1 5° l⇔ 70°	20°  -1 70°	48 in oz	SPDT Form Z	Silver	ML04S0100	106
nnidirectional - wire whi	sker (NEMA 1, 2, 12, 1	3 only)					
	Sk-Rd		15 in oz	SPDT Form C	Silver	MS05S0100	83.
<u> </u>	Bk-W   5'  = 15'		15 in oz	SPDT Form C	Gold	MS05G0100	90.
ushing mounted - top pla	unger						
Д	.070* max.	,090° max.	80 oz	SPDT Form C	Silver	MS06S0100	80.
$\Rightarrow$	Bi-W bi-Ad	Bk-Rd	80 oz	SPDT Form C	Gold	MS06G0100	87.
	0 (304")→ .19" max, min.	0  .03" )→ .19" max. min.	80 oz	SPDT Form Z	Silver	ML06S0100	102.
shing mounted - paralle	el roller plunger	_					
<u> </u>	.070° max.	,080° anax.	B0 oz	SPDT Form C	Silver	MS07S0100	90.
具	Bk-Fki Bk-Fki	Bit-No	80 oz	SPDT Form C	Gold	MS07G0100	96.
	Bk-W 1004"j-e .10" 0 1004"j-e .10" cntor. min.	0   .03°   → .19° mex. min.	80 oz	SPDT Form Z	Silver	ML07\$0100	112.
shing mounted - cross						•	
V	.070° max.	,080° max.	80 oz	SPOT Form C	Silver	MS08S0100	90.
<u></u>	Bk-W Bk-Ad Bk-W	Ba-Pd Ba-Pd	80 oz	SPOT Form C	Gold	MS08G0100	96.
	0 (0047-si .19" max. min.	0 (.03°)= .19° mio. min.	80 oz	SPDT Form Z	Silver	ML08S0100	112.
justable top plunger				•			
	Bk-Rd Bk-Rd	,080" max,	80 oz	SPDT Form C	Silver	MS09S0100	80.
$\Box$	Eh-Hd ■	Sk-W Bk-Rd	80 oz	SPDT Form C	Gold	MS09G0100	87.
	0 µ0047-4 .19°	0  .03°}≠ .19°	80 oz	SPDT Form Z	Silver	ML09S0100	102.6
See available options on page	19-32. Add to the end of cat	alog number. Up to three o	ptions may be added,	if applicable.			•













Discount T Schedule

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19-31

**Lever Arms** 

▲ See available options below. Add to the end of catalog number. Up to three options may be added, if applicable.
 ■ See below for conductor length selection.

Shown with side entrance cable, option 06

#### For Conductor Length and General Options Selection: 9007MS01S A\_B\_

A\_ Conductor Length 4

	Designator	Price Adder
No cable ◆	00	NC
3 feet—standard	01	NC
6 feet	02	\$ 4.20
9 feet	03	9.50
12 feet	04	13.70
18 feet	05	23.20
33 feet	13	63.00

Use with options 54, 55, 82

	Designator	Price
#16 AWG SJTO cable	02	\$ 4.20
Side entrance #18 AWG SJTO cable	06	7.40
Gray #18 AWG SJTO cable	10	NC
#18 AWG individual conductors	11 .	NC
Male 4 pin mini connector with 3 ft. cable	12	40.10
Low force (NEMA 1 only)18 oz.	21	3.20
High Pre-travel—adds .030	30	13.00
Male 4 pin micro connector in housing (DC type)	54	35.90
Male 5 pln micro connector (MS and ML, DC type)	55	35.90
Tapped holes in top of plunger housing (MS and ML)	81	N/C
Male 4 pin micro connector in housing (AC type)	82	35.90
Black #18 AWG SJTO cable	83	NC

There are over 100 styles of levers to accommodate most of the Industrial applications. They are made of aluminum bar stock hardened to 68000 psi tensile strength to combine strength with light weight. The roller levers are available with nylon rollers as standard and are also available with steel rollers or ball bearing roller (selected models only). Corrosion resistant models are also available.

	Style 7 Levers—.75" (19 mm) diameter, nylon or steel roller (900/ prenx is not required on levers catalog numbers)								umpers)
.75 19.0		Length		Number nm) Wide		Number nm) Wide	Catalog Number 3/4" (19 mm) Wide	Catalog Number 1" (25 mm) Wide	List Price
T	inch	(mm)	Nylon	Steel	Nylon	Steel	Nylon	Nylon	Price
	.875	(22.23)	7A2N	7A2	7B2N	7B2	7F2N	7J2N	\$ 9.50
	1.375	(34.93)	7A3N		7B3N	***	7F3N	7J3N	9.50
	1.5	(38.10)	7A1N	7A1	7B1N		7F1N	7J1N	9.50
<u></u>	1.75	(44.45)	7A7N		787N	•••	<b>7</b> F7N	7J7N	9.50
	2.00	(50.8)	7A4N	•••	784N	***	7F4N	7J4N	15.80
137	.875	(22.23)	7XA2N	7XA2	7XB2N	7XB2	7XF2N	7XJ2N	\$ 9.50
tyle 7A	1.375	(34.93)	7XA3N		7XB3N	***	7XF3N	7XJ3N	9.50
	1.5	(38.10)	7XA1N	7XA1	7XB1N		7XF1N	7XJ1N	9.50
	1.75	(44.45)	7XA7N		7XB7N		7XF7N	7XJ7N	9.50
n er.,75	2.00	(50.8)	7XA4N		7XB4N		7XF4N	7JX4N	15.60

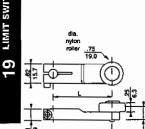
Specialty Arms and Options (9007 prefix is not required on levers catalog numbers)

Description	Catalog Number	Price Adder
Style 7D adjustable length 13/8 to 33/875" diameter, 1/4" wide, metal roller	70	\$15.80
Style 7DN adjustable length 13/8" to 33/8"75" diameter, 1/4" wide, nylon roller	7DN	\$15.80
Style 7S spring nylon, 6" rod, .3" diameter	7S	15.80
Style 7N nylon rod, 5" long, .3" diameter	7N	15.80
Corrosion resistant (option available with nylon rollers only)	S*	3.20

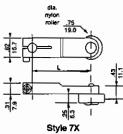
\* Add S to end of catalog number.

Lever Tightening torque: for mounting lever on the shaft: minimum 17 in lb.

For additional information, reference Catalog #9007CT9701R8/98 or D-FAX™ #1562.



St



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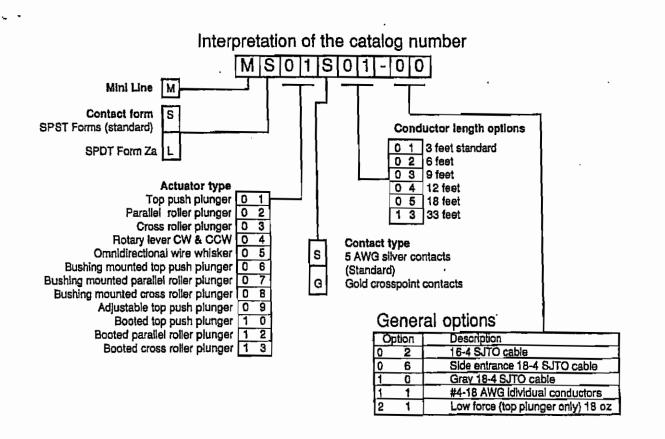


LIMIT SWITCHES

19-32

## **Belt Misalignment**

Switch			Omnidirectional
Type Description	MS Miniature		
Housing	Zinc die cast		
Contact type	Epoxy encapsulated SPST Form C or SPDT snap action		
Current rating	5A and 10A		
Housing	NEMA 1,3,4,6,	ł.	5.4
Repeatability	6P,12,13	f	1 11
Temperature range: standard		l	1 //
Temperature range: extended	-20°F to 200°F	al a	.63
Mechanical life	5 million	जनामुहासूत्रा । जन्म	.63
Plug-in	• <u> </u>		
Rotary lever-spring return	Yes		.63 Dia.
Rotary lever - maintained			
Rotary lever - 2 step	<u> </u>		1 1
Top plunger	Yes	Section Figure 7	┸╈┸╌┸╈╌┸
Top roller plunger	Yes	$(\mathcal{J})$	<del>-1(3)-1-(3)1-</del>
Side plunger			14 1 41
Side roller plunger			· \[-+\]
Omnidirectional	Yes	HSCISO F-MIN	[
Special features	Prewired 3 SJTO cable	<u> </u>	11 1 11
·	Bushing mounted option		
	Machine tools, washing equipment	- 100	
Applications :	Vehicles	St. P.	M-05





# ASHBROOK WINKLEPRESS® 13.0 LUBRICATION INFORMATION

## 13.1 LUBRICATION SCHEDULE

DAILY	None
WEEKLY	Check hydraulic tank level and condition of oil.
SEMI-ANNUALLY	Lubricate press roller bearings. Lubricate hydraulic pump motor bearings. Change oil in hydraulic tank, wash and replace filter screen.
ANNUALLY	Change oil in belt drive gear box.

13.2 Winklepress Lubrication Cross Reference

Frequency	Annually Drain & Refill	6 months Purge & refill	6 months or when necessary	6 months
Phillips	W/A	N/A	Magnus 150	N/A
Mobil	Mobilgear 630	Mobilith SHC 460	DTE 13M	Mobilith SHC 460
Chevron	Non-Leaded Gear Compound 220	Ultra Duty Grease #2	AW Oil 32	Ultra-Duty Grease #2
Shell	Omala Oil 220	N/A	Tellus 32	N/A
Exxon	N/A	N/A	Nuto 32	N/A
Техасо	Meropa 220	N/A	Rando Oil HO 32	N/A
Point of Application	Belt Drive Reducer	Press Roller Support Bearings	Hydraulic System Reservoir	Hydraulic Pump Motor

Revised July 2000



# ASHBROOK WINKLEPRESS® 14.0 SPARE PARTS INFORMATION

14.1 SUPPLIED SPARE PARTS LIST

14.2 SPARE PARTS ORDERING INFORMATION

For your convenience, spare parts may be ordered directly from Ashbrook.

If you need parts or have questions, please do not hesitate to call Ashbrook at 281-449-0322 or 800-547-7273.

14.3 SPARE PARTS PRICE LIST

On the following page are listed parts that you may want to purchase and keep on hand to have available for the maintenance of your Winklepress. The table gives the recommended quantities to keep on hand. If you feel you need other parts on hand or have questions regarding parts, please contact the Ashbrook Spare Parts Sales Office at 800-547-7273.

Belts can usually be supplied in 24 to 48 hours in cases of emergency.

#### AMERICAN WINKLEPRESS SZ 3 SPARE PARTS LIST W/DODGE BEARINGS

DESCRIPTION	PART #	QUANTITY REQUIRED	AVAILABILITY
UPPER BELT, 2.2M X 20.300M	030657	1	2 WEEKS
LOWER BELT, 2.2M X 15.670M	030658	1	2 WEEKS
RUBBER SEAL	004488	120'	ASH STOCK
SCRAPER BLADE	008146	2	ASH STOCK
CHICANE BLADE	009406	2	ASH STOCK
TENSION VALVE	012667	1.	ASH STOCK
STEERING VALVE	016408	2	1 WEEK
STEERING PADDLE ASSEMBLY	012986	2	1 WEEK
CERAMIC WEAR PAD	008565	2	ASH STOCK
POLY GRID STRIP	008718	6000"	ASH STOCK
VERTICAL SEAL ASSY	008145	1	1 WEEK
HYDRAULIC FILTER, 10 MICRON	032264	1	1 WEEK
90MM SEAL	040576	2	1 WEEK
90MM SNAP RING	008971	2	1 WEEK
90MM SPACER RING	008970	2	1 WEEK
ROLLER BEARING, 90MM	421268	2	1 WEEK
90MM STAB RING	040563	1	1 WEEK
90MM SPLASH GUARD, MALE	009233	1	ASH STOCK
90MM SPLASH GUARD, FEMALE	009234	1	ASH STOCK
60MM SEAL	040555	4	1 WEEK
60MM SNAP RING	008978	2	1 WEEK
60MM SPACER RING	008977	2	1 WEEK
ROLLER BEARING, 60MM	421263	2	1 WEEK
60MM STAB RING	040562	1	1 WEEK
60MM SPLASH GUARD, MALE	009231	1	ASH STOCK

#### AMERICAN WINKLEPRESS SZ 3 SPARE PARTS LIST W/DODGE BEARINGS

DESCRIPTION	PART #	QUANTITY REQUIRED	AVAILABILITY
60MM SPLASH GUARD, FEMALE	009232	1	ASH STOCK
BEARING, NU2212, EXPANSION	029206	2	1 WEEK
BEARING, NUP2212, NON-EXP.	422161	2	1 WEEK
BUTTON HEAD GREASE FITTING	010591	2	ASH STOCK
BUTTON HEAD GREASE GUN ADAPTER	009439	2	ASH STOCK
STEERING CYLINDER, FRP	026520	1	ASH STOCK
STEERING CYLINDER REPAIR KIT	026697	1	ASH STOCK
FRP CYLINDER			
TENSIONING CYLINDER, FRP	027452	1	ASH STOCK
TENSION CYLINDER REPAIR KIT	028202	1	ASH STOCK
FRP CYLINDER			
PRESSURE GAUGE	010846	1	1 WEEK
UPPER PLATE FOR FIXED VERTICAL WEDGE	011170	1	1 WEEK
LOWER PLATE FOR FIXED VERTICAL WEDGE	011862	1	1 WEEK
UPPER PLATE FOR HINGED VERTICAL WEDGE	011168	1	1 WEEK
LOWER PLATE FOR HINGED VERTICAL WEDGE	011169	1'	1 WEEK

PARTS LISTED ARE MINIMUM RECOMMENDED.IF YOU FEEL YOU NEED OTHER PARTS ON HAND OR HAVE QUESTIONS REGARDING PARTS, PLEASE CONTACT THIS OFFICE AT (800) 547-7273.
\*BELTS CAN USUALLY BE SUPPLIED IN 24-48 HOURS IN CASES OF EMERGENCY

06/02



# ASHBROOK WINKLEPRESS®

#### 15.0 REFERENCE

#### 15.1 TROUBLESHOOTING CHARTS

Also see Section 8.10 Process Diagnostic Chart.

#### HYDRAULIC SYSTEM TROUBLE SHOOTING GUIDE

<u>PROBLEM</u>	PROBABLE CAUSE	REMEDY
Hydraulic power unit fails to energize when control pushbutton is depressed.	1. Control panel feeder circuit in "off" or "tripped position.	1. Set breaker to "on" position.
	2. Motor starter overload protectors in tripped position	2. Depress overload reset button on motor starter.
Belt steering erratically, requiring constant automatic correction.	Improper roller alignment, valve alignment, valve sensitivity or belt defects.	Carry out check and adjustment procedures which are appropriate.

#### HYDRAULIC SYSTEM TROUBLE SHOOTING GUIDE

PROBLEM	PROBABLE CAUSE	REMEDY
Hydraulic unit operational but fails to build pressure.	1. Incorrect direction.	1. Insure that rotation is correct. If not have a qualified electrician revise motor wiring at motor starter.
	2. Pressure regulator, located on hydraulic pump, is not properly adjusted.	2. Correct adjustment.
	3. Pressure regulator clogged by foreign material causing fluid bypass back to reservoir.	3. Disassemble & clean valve. Check for worn or broken parts. If particles are found in valve, drain and clean reservoir, refill as recommended in lubrication schedule.
	4. Belt guidance valve bypassing fluid directly back to power unit reservoir.	4. Remove and clean belt guidance valve of any foreign material. If cleaning does not improve operation, contact a qualified hydraulic repair center or contact Ashbrook Corporation.
	5. Hydraulic pump worn or damaged.	5. Have pump serviced by a qualified hydraulic repair center. Contact Ashbrook if a replacement pump or part is required.

## DRIVE SYSTEM TROUBLE SHOOTING GUIDE

<b>PROBLEM</b>	PROBABLE CAUSE	<u>REMEDY</u>
Main drive fails to start and drive the belt when energized.	1. Control panel interlocks prohibit belt drive energizing until appropriate ancillary equipment is operational.	1. See sequence of operations and control diagrams for design interlocks. Energize appropriate equipment.
	2. Belt drive speed potentiometer set at zero.	2. Increase pot setting to desired speed.
	3. VFD (A.C. electronic drive controller) tripping chassis mounted overload protector or feeder voltage fuses burnt out.	3. Reset overload and check fuses for continuity, renew or reset as required. Check for dried sludge or other obstructions on the belt which would put unusual starting load on belt drive.
	4. If condition #3 is found to exist.	4. Turn off control panel main breaker. Release belt tension. Remove cover from reducer. Rotate motor/reducer by hand. If movement is not possible, remove gear guard and check for missing or broken teeth on pinion or bull gears. Replace gears as required.
	5. If check out fails to show problem and incoming voltage to VFD is proper. The VFD has failed.	5. Take VFD controller to repair center for reconditioning or replacement. Contact Ashbrook for service.

# **Process Trouble Shooting**

Problem	Probable Cause	Remedy
Sludge does not Flocculate	Polymer is not flowing	Verify polymer system is on.
		Verify polymer is flowing through plastic hoses at mixer.
_	Insufficient amount of polymer	Increase polymer dosage
	Wrong polymer type	Contact Ashbrook or polymer representative
	Insufficient polymer mixing	Increase polymer mixing energy
		Increase retention time in piping
Sludge does not dewater in gravity section	Belt is blinded	Clean belts
	Poor flocculation	Increase polymer
-		Increase mixing energy
-	Wrong polymer type	Contact Ashbrook or polymer representative
	Loading rate too high	Decrease sludge feed rate
Capture is poor	Seals are worn on restrainers	Replace seals
	Insufficient polymer	Increase polymer dosage
Low Cake Solids	Insufficient polymer	Increase polymer dosage
	Too much polymer	Decrease polymer dosage
	Wrong polymer type	Contact Ashbrook or polymer representative
	Low belt tension	Increase hydraulic pressure on belts
	Loading rate is too high	Decrease sludge feed rate.
	Belt speed is too fast	Decrease belt speed.
Cake adheres to belt	Belt tension is too high	Decrease belt tension
	Polymer dosage is too high	Decrease polymer dosage
	Insufficient mixing	Increase mixing energy
Sludge build up in pans	Upset process	Clean pans and optimize process

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## Belt Wash Water System Trouble Shooting guide

# Problem Probable Cause Remedy

Water Pump Does Not Run	Pump Motor Not Running	Verify Switch is On
-	Tuning	Verify Power is On
		Motor is Burned Out or Needs Repaired
Low pump pressure	By Pass Valve at Press	Close Handwheel Valve at Wash Box
Dow pump pressure	is Open	Close Halle wheel y arve at Wash Box
	Impeller is Worn	Replace Impeller
	Suction pressure too low	Correct suction pressure problem
_	Pressure Switch Fault	Restart System and verify pressure is above 50 psi
		Verify pressure switch is functioning by bypassing switch and restarting system
Low Pressure at Wash Box	Line is Blocked	Check piping and remove obstruction
-	By Pass Valve at Press is Open	Close Handwheel Valve at Wash Box
	Nozzle is Missing	Replace Nozzle in Wash Tube
_		
No Water at Wash Box	Valve is Closed	Open Valves
Water bypassing	Valve is open	Close handwheel valve
shower	, mile to open	CASS AMERICAN AND A PROPERTY OF THE PROPERTY O
	Seals on washtube are worn	Replace seals

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## **Belt Tracking Trouble Shooting guide**

# Problem Probable Cause Remedy

Belt Will Not Track	Poor distribution of sludge	Correct distribution on gravity section
	Wedge section opening is not even	Adjust top and bottom of wedge so that the opening is the same on both sides of the machine
	Sludge is built up on rollers	Clean rollers
	Steering Paddle not following belt	Spring on valve is worn or broken, replace spring
		Valve is sticking or frozen, repair or replace valve
		Paddle is out of adjustment, Adjust paddle.
	Belt is stretched out of square due to poor distribution	Run the machine without sludge for two hours at 700 psi pressure to correct uneven stretch. Correct distribution problem. If belts will not restretch to square, replace belts.
	Belt is cut out of square	Remove the belt from the machine. Rotate it 180 degrees and reinstall. If the belt is bad, it will go off on the opposite side. If it steers off the same side, the belt is not at fault.
	Roller has been knocked out of alignment	Check all rollers for parallel. Run a 100 foot flat tape along the belt path on both sides near the end of the roller. Each side should be the same (1/2" tolerance). If not, call Ashbrook
	Hydraulic pressure is low	Increase pressure
	Cylinder is stuck	Manually move steering paddle to see if cylinder responds. If not, repair/replace cylinder.

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# Winklepress Trouble Shooting

<u>Problem</u>

Probable Cause

Remedy

Belt Press Does Not Run	Sludge Pump Not Operating	Check Sludge Pump
	Polymer System Not Operating	Check Polymer System
	Belt Drive Not Operating	See Drive System Trouble Shooting Guide
	Hydraulic Unit Not Operating	See Hydraulic System Trouble Shooting Guide
	Water Pump Not Operating	See Belt Wash Water System Trouble Shooting Guide
	Control System Problem	See Control System Trouble Shooting Guide
Belt tension slacks when sludge is applied	Hydraulic cylinder is by passing oil internally	Repair or replace cylinder
Scraper blade not cleaning belt	Blade is out of adjustment or requires replacement	Adjust or replace blades
	Build up of fibrous material, such as hair, at the knife edge of the blade	Open blade and clean
Scraper blade wears quickly	Blade tension too tight	Reduce blade tension. Optimize process
	Belt speed too fast	for good belt release Reduce belt speed
Roller sticking	Bearing is worn	Replace bearing
Bearing losing excessive grease	Bearing seals are blown	Replace seals
Machine runs in a jerky motion at roller bearings	Gear train is damaged	Inspect gear reducer and replace as required.

# Winklepress Trouble Shooting

Problem/Alarm	Probable Cause	Remedy
Emergency Stop	Press Trip Cord	Reset Trip Cord
	Press E-Stop Pushbutton	Pull-Out Emergency Stop Operator At Junction Box
	Panel E-Stop Pushbutton	Pull-Out Emergency Stop Operator At Control Panel
	ESR Failure	Relay out of socket; No voltage(120vac); Bad Relay
Belt Drive Fail	BD-VFD Failure	Reset BD-VFD
Low Water Pressure	Low Water Pressure	Washwater Pump Not Running
		Bad Pressure Switch Contact/ Setting
Washwater Pump Fail	WP Overload Failure	Reset Washwater Pump Overload at MCC-SP
Hydraulic Pressure Fault	Low Hydraulic Pressure	Hydraulic Pump Not Running
	High Hydraulic Pressure	Bad Pressure Switch Contract
Hydraulic Pump Fail	HP Overload Failure	Reset Hydraulic Pump Overload at MCC-SP
Belt Mis-Aligned	Belt Over-Tracked	Re-Align Belt
Belt Broken	Belt Broke	Replace Belt
Polymer System Fail	Polymer Pump Failure	Reset failure at PP-SCR
	Polymix Tank Low Water Seal Failure	Replace Seal
	BFP Poly No Flow	Polymer Pump Not Running
	Low-Low Polymer Mix Tank	Add Poly To Mix Tank
Sludge-System Fail	BFP No Sludge Flow	Sludge Pump Not Running
· )	Sludge Pumo High Pressure	Blockage In Sludge Line
	Sludge Pump Fail	Reset Failure At SP-VFD
	Sludge Seal Water Failure	Replace Seal
	Belt Blinding	Sludge Pump Not Running
No Cake	Lake of Polymer/Sludge	Sludge Pump Not Running
		Polymer Pump Not Running



#### **15.2 EQUIPMENT IDENTIFICATION**

The plate pictured below is attached to the side of the frame on each filter press or gravity belt thickener. Prior to calling our service department for information, or when placing a parts or service order, please have the data from this plate available. This will help us to serve you better.

#### Ashbrook Simon Hartley 11600 East Hardy Houston, TX 77093

MPS No.	 	 	
Serial No.		 	
	<u> </u>		
Part No.			
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#### 15.3 CUSTOMER SERVICE DEPARTMENT INFORMATION

Our Customer Service department is comprised of four traveling technicians, two traveling pilot operators, the process manager, the customer service coordinator and customer service manager. The Customer Service department is headed by Vice-President of Operations, Mr. Peter Deaville. Operating hours are Monday through Friday from 8:00a.m. to 5:00p.m. (Central Time).

When calling, please use the direct numbers listed below. If you should get a recorded message, please do not hang up. State your name, Company name, phone number and the nature of you call and we will respond to you as soon as possible. If your needs are urgent, press "0" to return to the operator, who can page the requested party.

Customer Service Manager	Pat Everett	281-985-4465
Customer Service Coordinator	Danny Grant	281-985-4429
Spare Parts		800-547-7273
Vice-President, Operations	Pete Deaville	281-985-4443

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